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WIND TUNNEL MEASUREMENTS OF THE
MAGNUS INDUCED SURFACE PRESSURES ON
A SPINNING ARTILLERY PROJECTILE
MODEL IN THE TRANSONIC SPEED REGIME

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by Miles C. Miller
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RESEARCH DIRECTORATE

September 1986

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PREFACE

The work described in this report was authorized under Project No. 1L162618AH80, Launch and Flight Technology, Exploratory Development. This funding supported the design, fabrication, testing, and analysis aspects of the effort. This work was started in October 1979 and completed in September 1984.

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All funding for the design, fabrication, testing and analysis associated with this study was provided by the U.S. Army Ballistics Research Laboratory. The funding and support provided by Dr. Charles H. Murphy, Chief of the Launch and Flight Dynamics Division, were essential to its completion.

The fabrication of the wind tunnel model and sting components was accomplished by the Experimental Fabrication Branch, Research, Development and Engineering Support Directorate, Chemical Research, Development and Engineering Center (formerly the Chemical Systems Laboratory). In particular, the exceptional skills of Coy Barker, David Blake, Kenneth Younger, Scotty Johnson, and Llewellyn Thompson provided the high quality test items required.

A key element in the success of this study was the o-ring utilized in the sliding seal. The cooperative efforts of Ike Royster and Dutch Haddock of the Parker Hannifin Corporation in providing advice and samples facilitated the evaluation and selection of the required o-ring configuration and material.

Access to the NASA Ames, 14-foot transonic wind tunnel was gained through the test justification support provided by Harold R. Vaughn and Albert E. Hodapp of the Aeroballistic Division, Sandia National Laboratories and Carman Spinelli, XM785 Project Manager at the U.S. Army Armament Research and Development Center.

Important guidance for the test procedure and interpretation of the resulting data was obtained from Dr. William Oberkampf of the Aeroballistic Division, Sandia National Laboratories.

Individuals from the Aerodynamics Research and Concepts Assistance Branch also contributed to this effort. Owen C. Smith, Jr., in addition to his previous efforts in developing the sliding seal design, participated in several of the functional check-outs of the model and instrumentation systems prior to the wind tunnel test. Daniel J. Weber developed the computer program necessary to analyze the relatively large volume of complex data reduction associated with force and moment coefficient pressure integration.

Finally, the authors express their appreciation to Abraham Flatau for his encouragement and support, which allowed the sliding seal experimental technique to be sequentially evolved from the initial concept in 1975 to the current application.

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WIND TUNNEL MEASUREMENTS OF THE MAGNUS INDUCED SURFACE PRESSURES ON A SPINNING ARTILLERY PROJECTILE MODEL IN THE TRANSONIC SPEED REGIME

1. INTRODUCTION

A spinning projectile in flight produces aerodynamic surface pressures that have led to the so-called Magnus effect. This external aerodynamic phenomenon due to the combination of projectile spin and angle of attack produces forces and associated moments that have resulted in flight instabilities for several military projectiles.¹⁻³ Although the Magnus force is only a 10th to a 100th of the normal force, it can have a large detrimental influence on range and accuracy. Figure 1 contains flight test data illustrating the yaw growth experienced by an artillery projectile experiencing a Magnus instability. A concerted effort has been underway to experimentally investigate the fundamental Magnus phenomena and to develop theoretical models and analytical techniques to describe the effect.^{4,5}

This report presents wind-tunnel test measurements of the aerodynamic surface pressures on a full scale spinning model of the M549/XM785 artillery projectile in the transonic speed regime. The model, a secant ogive, cylinder, boattail configuration with an 8-inch diameter and a 5.5 caliber length, was evaluated both with and without a rotating band. The model was tested in the NASA-Ames 14 Foot Transonic Wind Tunnel. Circumferential pressure distributions were obtained at several longitudinal locations on the model, with emphasis on the cylindrical and boattail sections. The model was tested at angles of attack of 0, 4, and 10 degrees and spin rates of 0 and 4,900 rpm. All testing was done at a Mach number of 0.94, which corresponds to the critical Mach number for this projectile configuration.

The model configuration, scale, and test conditions were selected to complement a series of wind-tunnel tests conducted by the Ballistics Research Laboratory (BRL) that involved an extensive wind-tunnel investigation of a similar projectile configuration and scale at the NASA-Langley 8-Foot Transonic Wind Tunnel.^{6,7} During these tests, the aerodynamic forces and moments as well as velocity profiles of the boundary layer were obtained on both a spinning and non-spinning model. The aerodynamic surface pressures were also measured, but only for the non-spinning condition.

The tests were conducted to extend the data base for this projectile configuration and represent the first time that the aerodynamic surface pressures have been experimentally determined on any spinning projectile. Several other test objectives were also achieved as shown in Figure 2. The results allow a detailed insight into the Magnus phenomena as well as providing experimental data to support the evolution and validation of theoretical and numerical analyses. In addition, the test demonstrated the use of a new experimental method to obtain surface pressure data.

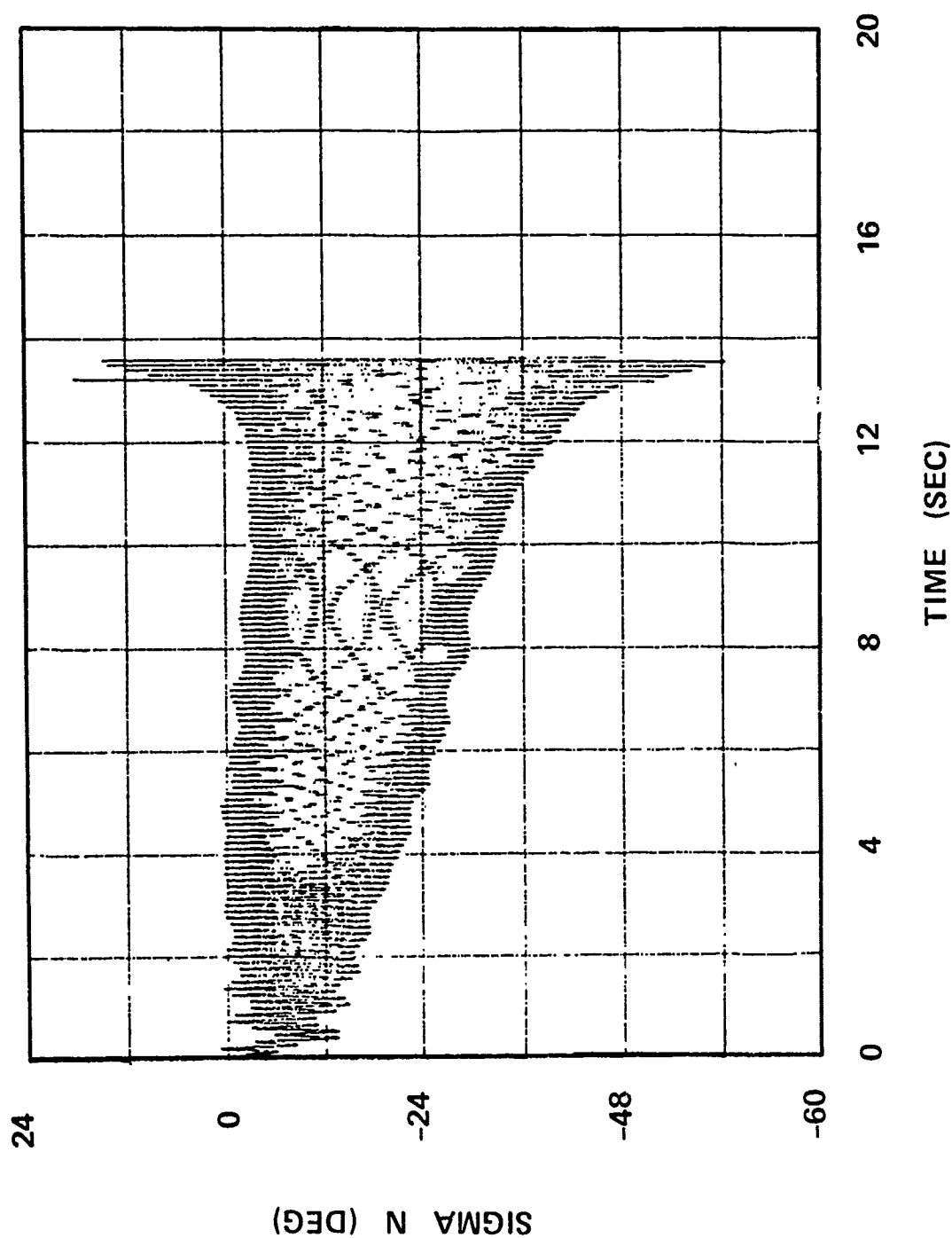


Figure 1. Time History of Projectile Yawing Motion
Resulting from Magnus Instability

- DETERMINE MAGNUS CHARACTERISTICS OF PROJECTILE AT CRITICAL (TRANSONIC) MACH NUMBER
 - EFFECT OF SPIN
 - EFFECT OF ANGLE OF ATTACK
 - ATTACHED FLOW ($\alpha = 4^\circ$)
 - SEPARATED FLOW ($\alpha = 10^\circ$)
 - EFFECT OF ROTATING BAND
- COMPLEMENT PREVIOUS TEST DATA
 - FORCE AND MOMENT
 - NON-SPINNING SURFACE PRESSURE
 - BOUNDARY LAYER
- INTERPRET GENERAL MAGNUS PHENOMENA
- DEMONSTRATE NEW TESTING TECHNIQUE
- PROVIDE DATA TO SUPPORT AND VERIFY THEORETICAL COMPUTATIONS

Figure 2. Objectives of the Wind Tunnel Tests

Mach number 0.94 represents the critical Mach number for this projectile (i.e., the condition where the projectile possesses the maximum destabilizing aerodynamic effects). Figure 3 depicts the flow field that exists over the projectile at this transonic condition. The shadowgraph shows that two separate shock waves occur: one just downstream of the ogive/cylinder junction and the other just downstream of the cylinder/boattail junction. This combination of subsonic and supersonic flow produce a complex surface pressure distribution as shown.

In addition to the basic angle of attack of 0 degree, the test included angles of attack of 4 and 10 degrees because they produce an attached flow and separated flow, respectively, over the boattail region of the model. The aerodynamic characteristics undergo a significant change between these two angles of attack, and the resulting pressure data would be of great interest. The spin rate of 4,900 rpm represents a tip speed ratio of .17 corresponding to a Mach 0.94 muzzle velocity condition. Finally, the influence of the rotating band on the Magnus surface pressures in the transonic speed region is of particular concern. This situation is currently being addressed by using computational fluid dynamic methods, and little experimental data exists to support or verify these theoretical analyses.^{8,9}

2. BACKGROUND

During the past several years, the Aerodynamics Research and Concepts Assistance Branch has systematically evolved a new and unique method to experimentally measure the aerodynamic pressures acting over the external surface of the spinning wind tunnel model. The method is based on an unconventional model design and instrumentation arrangement. The model is composed of two parts. A non-spinning inner portion of the wind tunnel model, containing the instrumentation, detects the surface pressure through a series of vent holes in the spinning outer portion of the model, the pressure being retained for measurement by means of a sliding seal arrangement.¹⁰ This method avoids the problems and limitations of conventional test techniques^{11,12} and allows surface pressures to be measured on spinning bodies at any attitude and flow regime. In addition, the body can include indentations or protuberances.

The validity and performance capability of the testing method has been demonstrated in stages, beginning with a simple spinning right-circular cylinder in cross flow that verified the basic concept.¹³ A second major series of tests involved the measurement of the surface pressures on a spinning Magnus autorotor,¹⁴ which extended the testing method to bodies having irregular surface features and an unsteady, periodic flow field. Other studies investigated improved instrumentation elements, in particular, the critical sliding seal units. This latter work evolved a magnetic fluid seal¹⁵ (to reduce friction effects), a miniature sized seal, and a remotely selectable pneumatic seal, all intended to increase the versatility and accuracy of the testing method. These efforts were funded by the BRL, CRDEC, and Sandia National Laboratories, respectively. Portions of the material presented in this report have been disseminated through presentations at conferences¹⁶ and articles in technical journals.¹⁷ A concise summary of the evolution of the experimental technique and the results obtained has also been published.¹⁸

TRANSONIC FLOW FIELD

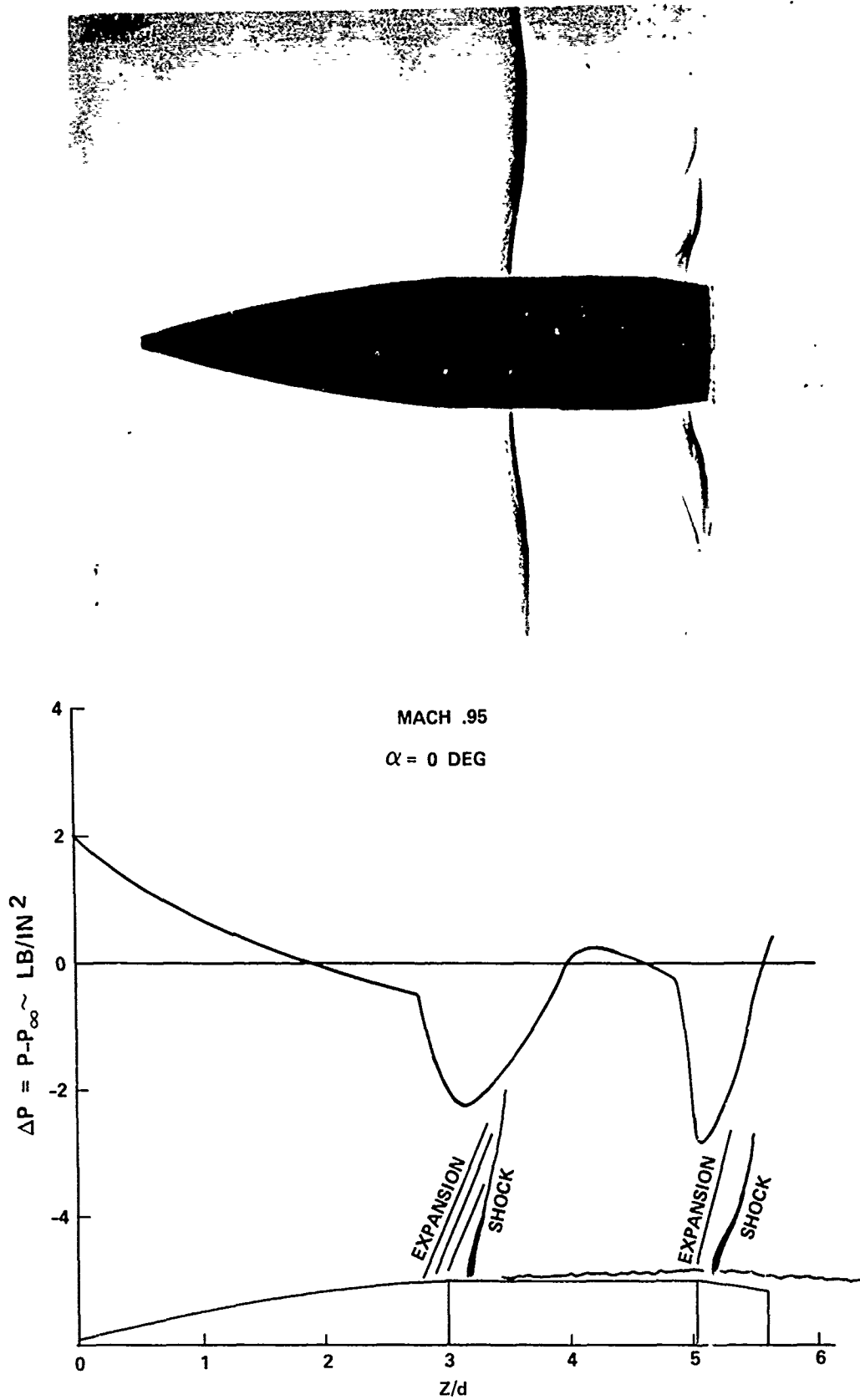


Figure 3. Transonic Flow Field and Surface Pressure Distribution

3. MODEL DESCRIPTION

The external model configuration and model sting arrangement are shown in Figures 4 and 5, respectively. The model was composed of a 3 caliber secant ogive, a 2 caliber cylindrical section, and a 7-degree, 0.5-caliber boattail. The projectile represents a 130-percent scale model of the M549/XM785 155-mm artillery projectile; however, it closely resembles the baseline projectile shape being analyzed by the BRL. The model also included the flat nose and wrench grooves of a standard fuze. The model's external shaping and scale were also identical to the model used in the Langley tests. The aft end of the model sting was attached directly to the wind tunnel roll head assembly which, in turn, was attached to the tunnel angle-of-attack sector sting.

A schematic drawing of the model's internal arrangement is shown in Figure 6. Detailed engineering drawings of the model components are included for your convenience in the last appendix in this report (Appendix D). The model consisted of an aluminum core containing the spin motor, pressure taps, and scanivalve mechanism. The model core was stationary (i.e., non-spinning) with respect to the model sting. The steel shell, representing the outer contour of the projectile was attached to the core by means of front and rear bearings and connected to the spin motor through an axial drive shaft at the nose. A set of four vent holes at 90-degree circumferential intervals were located through the shell at each of 20 longitudinal stations along the model. These vent holes which were 0.0625 inch in diameter coincided with the 20 pressure taps contained in the outer surface of the core section. Only two taps are shown in Figure 6 for clarity.

Two scanivalves, located in the core, were used as switching devices to allow the remote selection and engagement of the pressure tap seal units. The scanivalves were simultaneously driven by a common index/drive unit, also located in the model core. One scanivalve directed pneumatic air to a particular pressure tap seal unit to force it outward against the inner surface of the spinning shell. Concurrently, the other scanivalve directed the surface pressure being measured at that tap out through the sting to the pressure transducer and associated recording equipment located outside the tunnel. Figures 7 and 8 contain photographs of the model core with the shell removed to illustrate the scanivalve installation and the pressure tap locations, respectively.

The gap between the face of the pressure tap seal unit and the inner surface of the shell was sealed by means of a circular o-ring located on the outer face of the seal unit. The cavity created by engaging the seal unit with the shell was open to the pressure acting on the outside surface of the shell when the vent hole was aligned with the seal unit, as illustrated in Figure 9. Once the vent hole in the spinning shell rotated past this aligned position, the o-ring caused the cavity to retain the pressure. After a sufficient number of shell revolutions, the cavity eventually assumed a constant pressure equal to the pressure acting on the surface of the spinning shell at that particular circumferential location. Details of the pressure tap seal units are contained in Figure 10, and a photograph of them is shown in Figure 11. Figure 12 depicts the seal units installed in the boattail section of the core. The outer surface of each seal unit was contoured to match the radius of the inner shell surface at that location. The Parker-Hannifan No. 2-204-N827-80 o-rings, 0.5 inch diameter, were composed of lubricant-impregnated carboxylated nitrile rubber and were retained in the circular groove of the seal block by high viscosity silicone

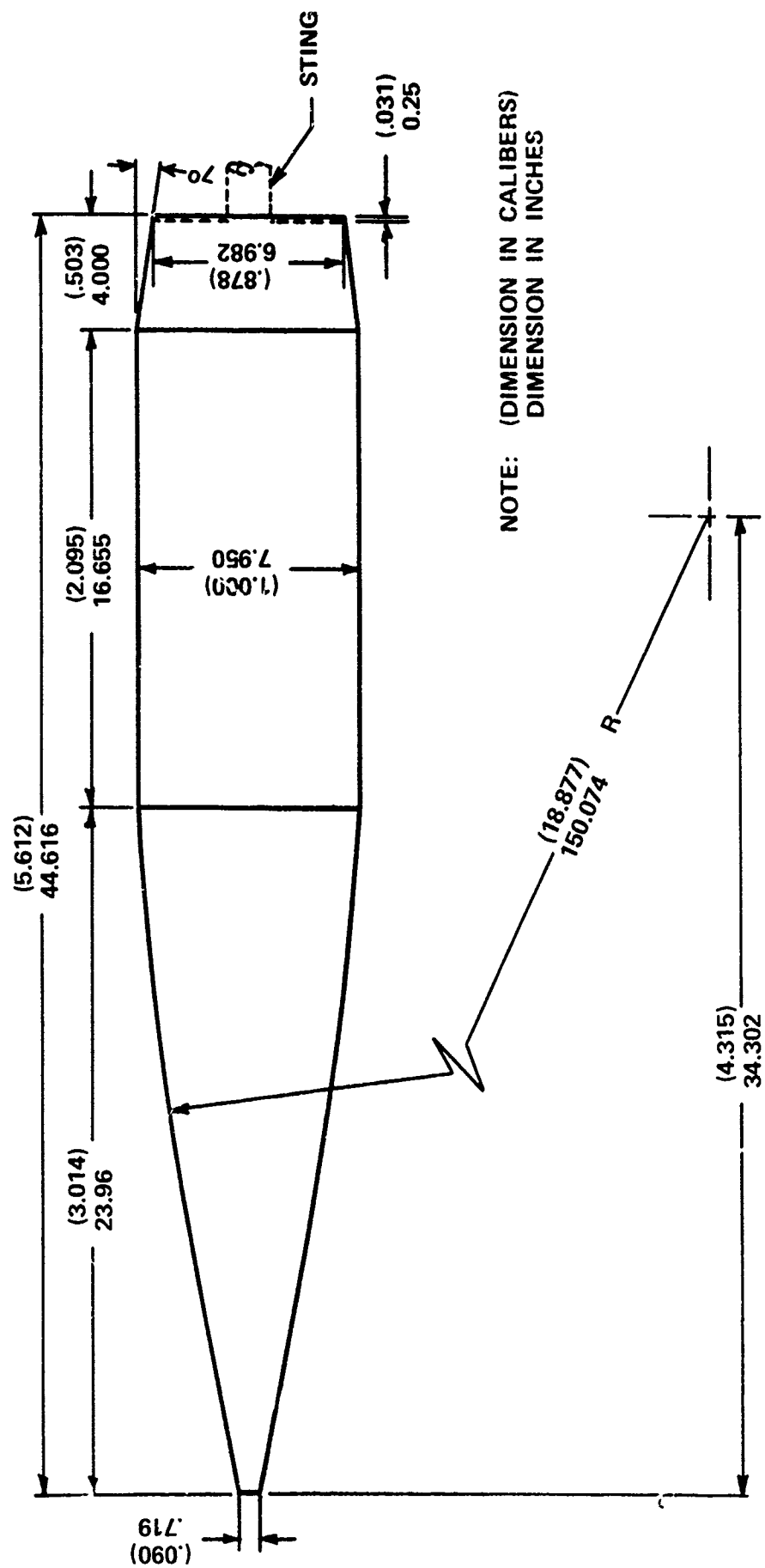


Figure 4. External Configuration of the Wind Tunnel Model

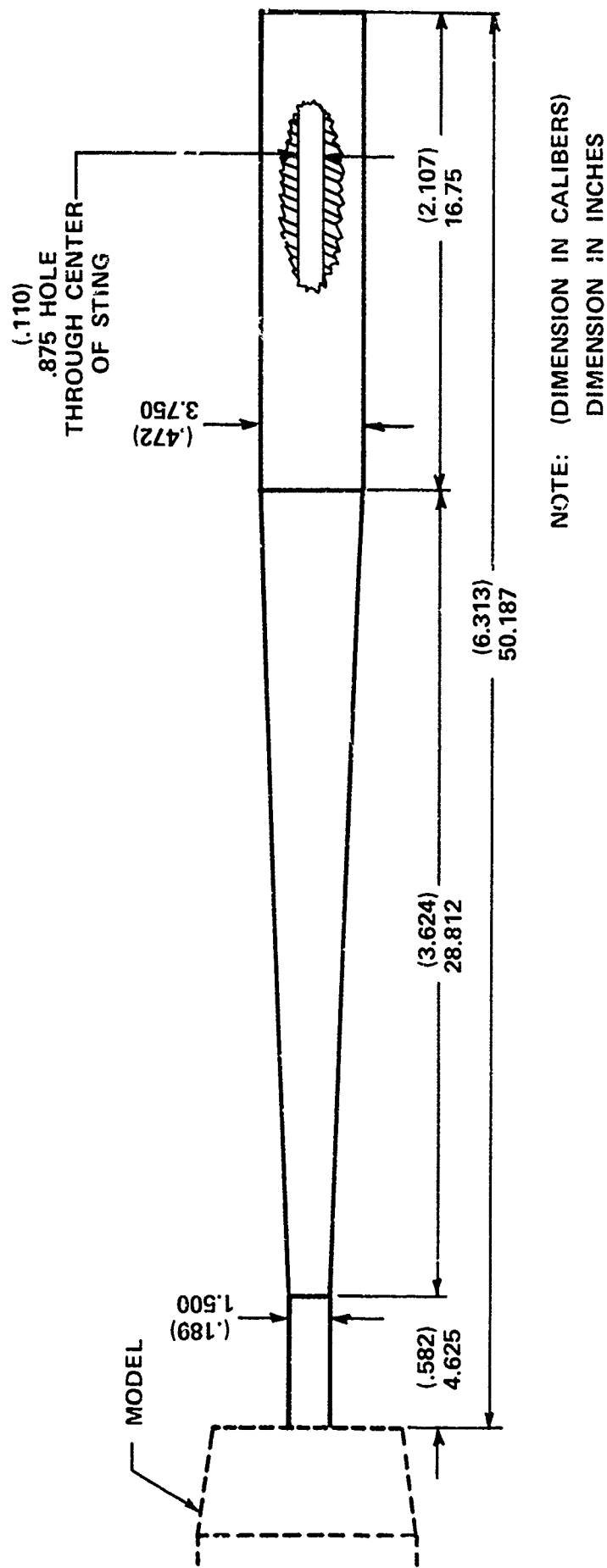


Figure 5. Sting Arrangement for the Wind Tunnel Model

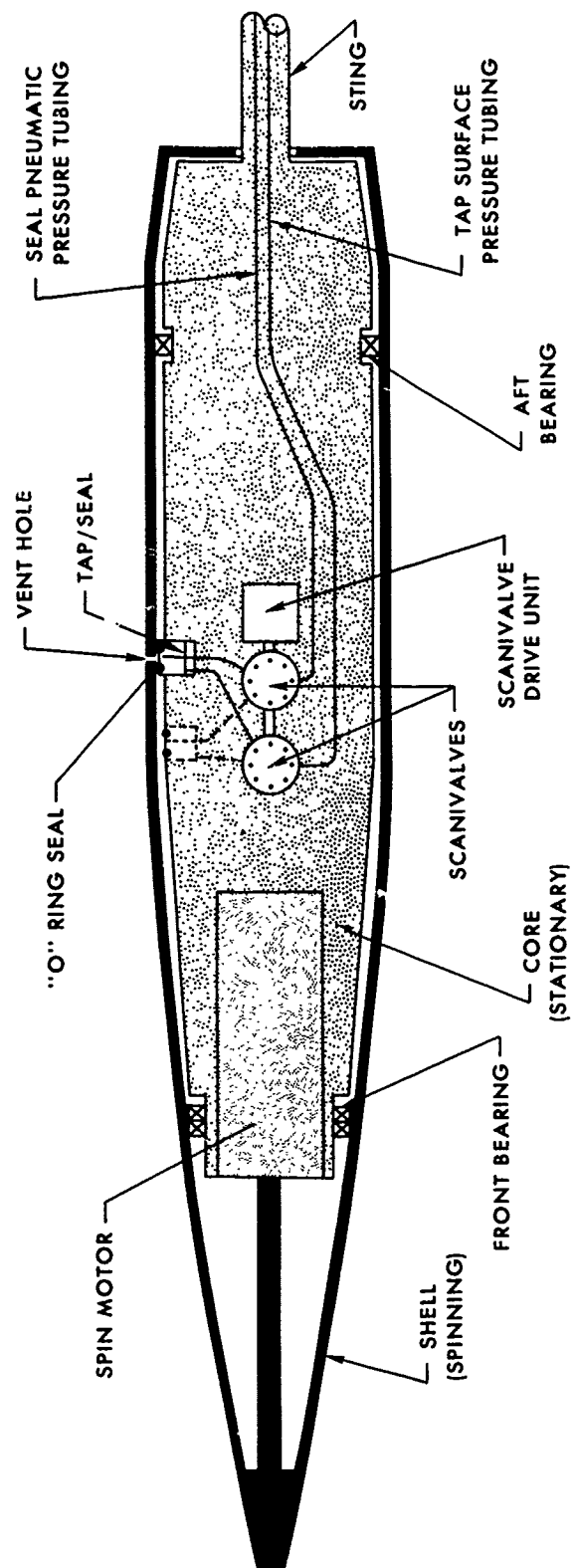


Figure 6. Internal Configuration of the Wind Tunnel Model



Figure 7. Photograph of the Model Core Showing
Scanivalve Installation

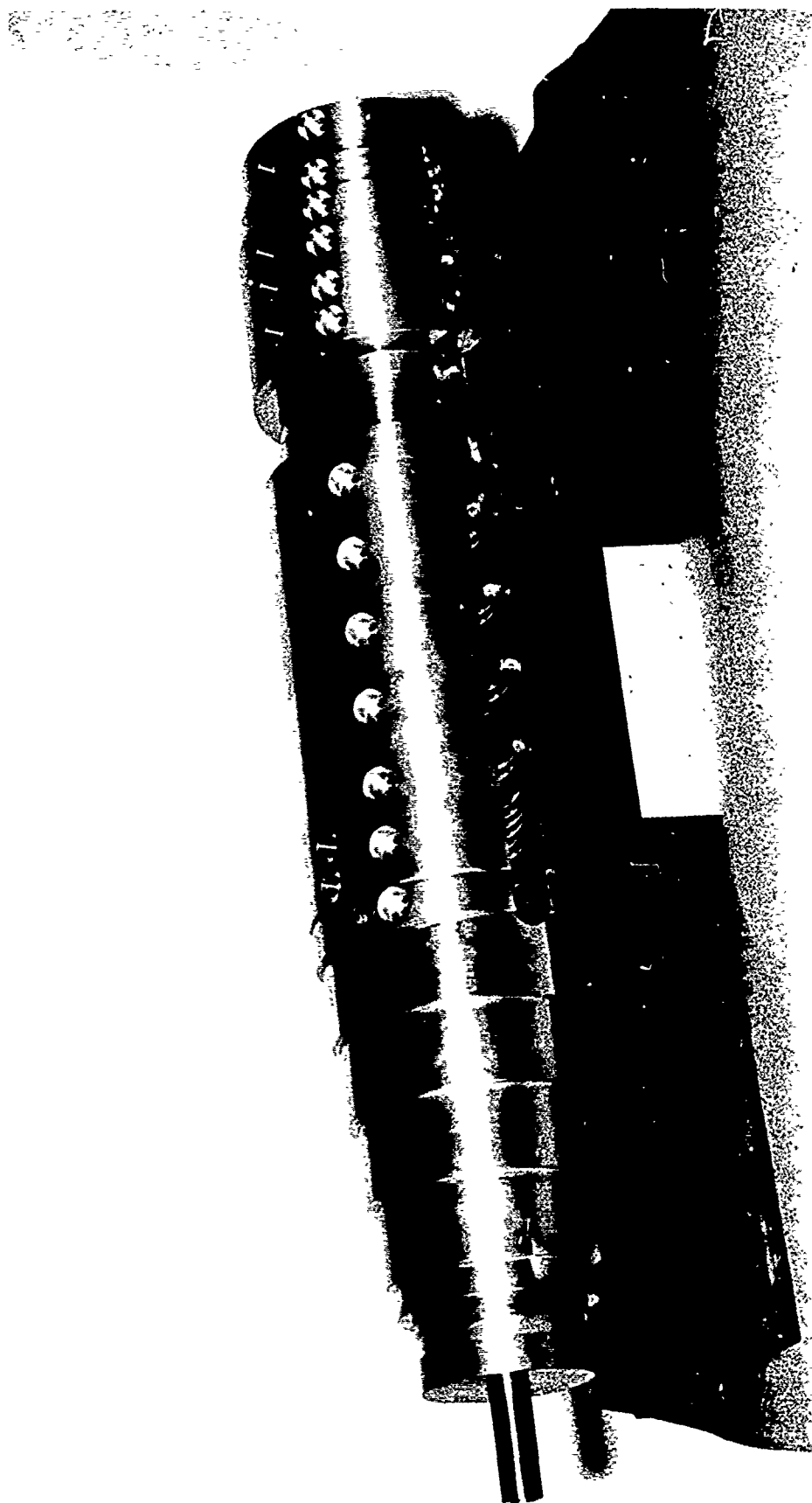


Figure 8. Photograph of the Model Core Showing
Pressure Tap Locations

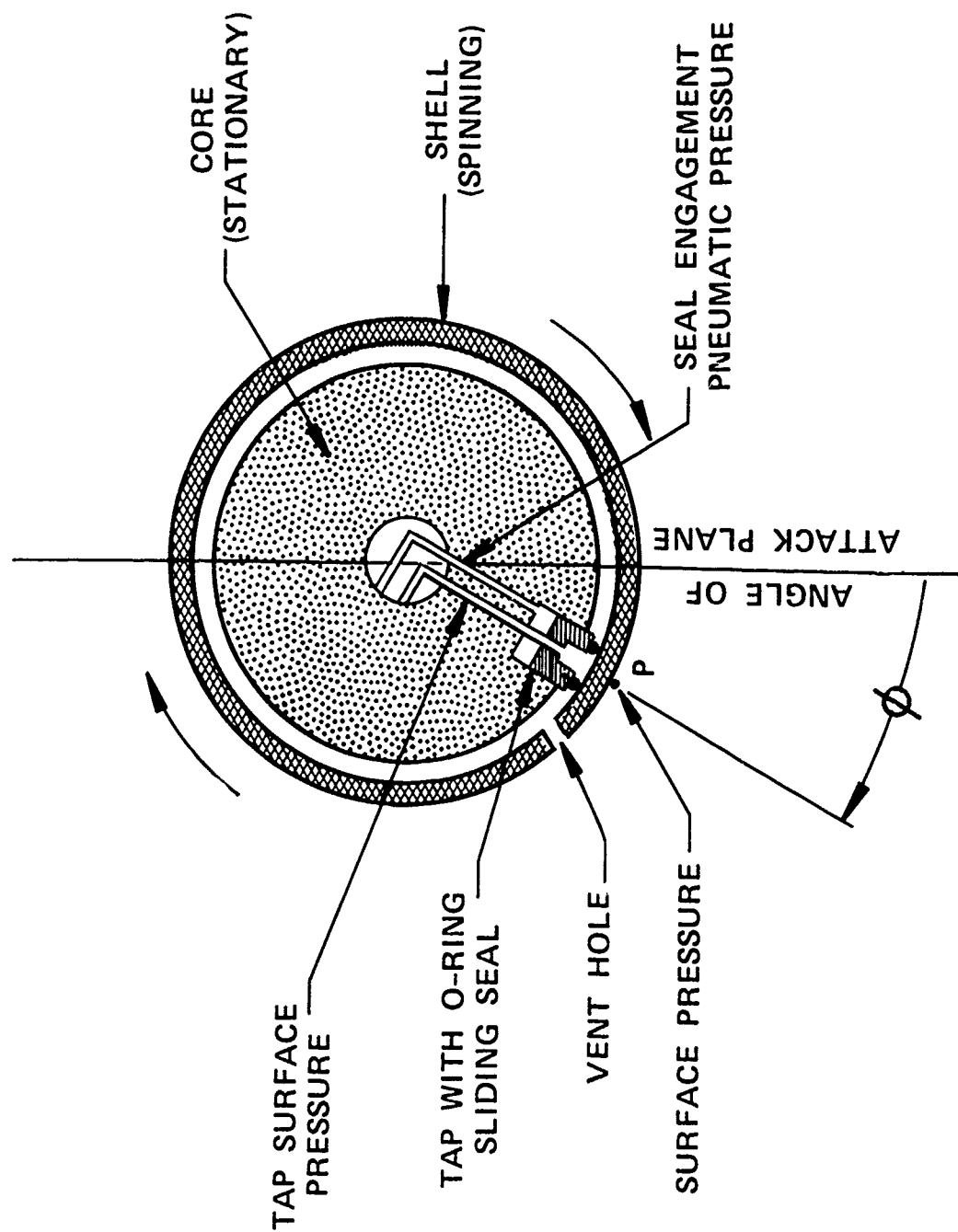
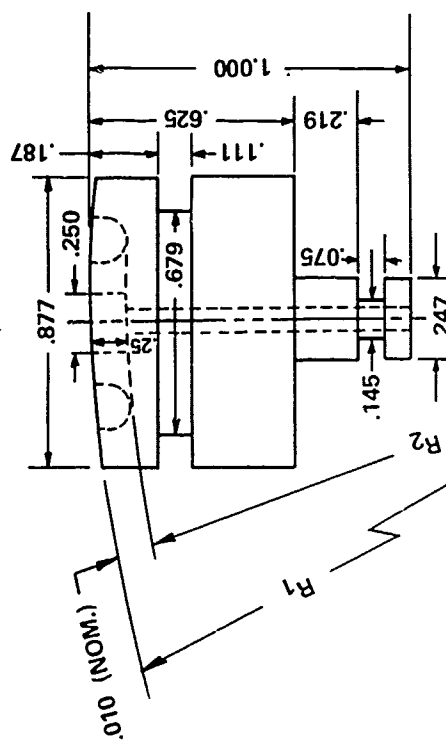
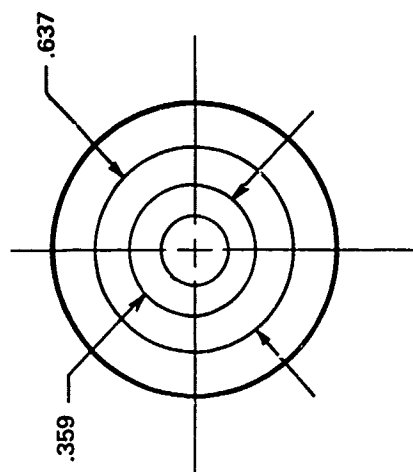


Figure 9. Surface Pressure Measurement Technique



NOTE: DIMENSIONS IN INCHES

R_1 AND R_2 DEPENDENT ON MODEL
TAP LOCATION; CURVATURE TO
MATCH SHELL I.D. WHILE ACCOMMO-
DATING DISPLACEMENT DUE TO
O RING THICKNESS.

Figure 10. Details of the Pressure Tap Seal Unit

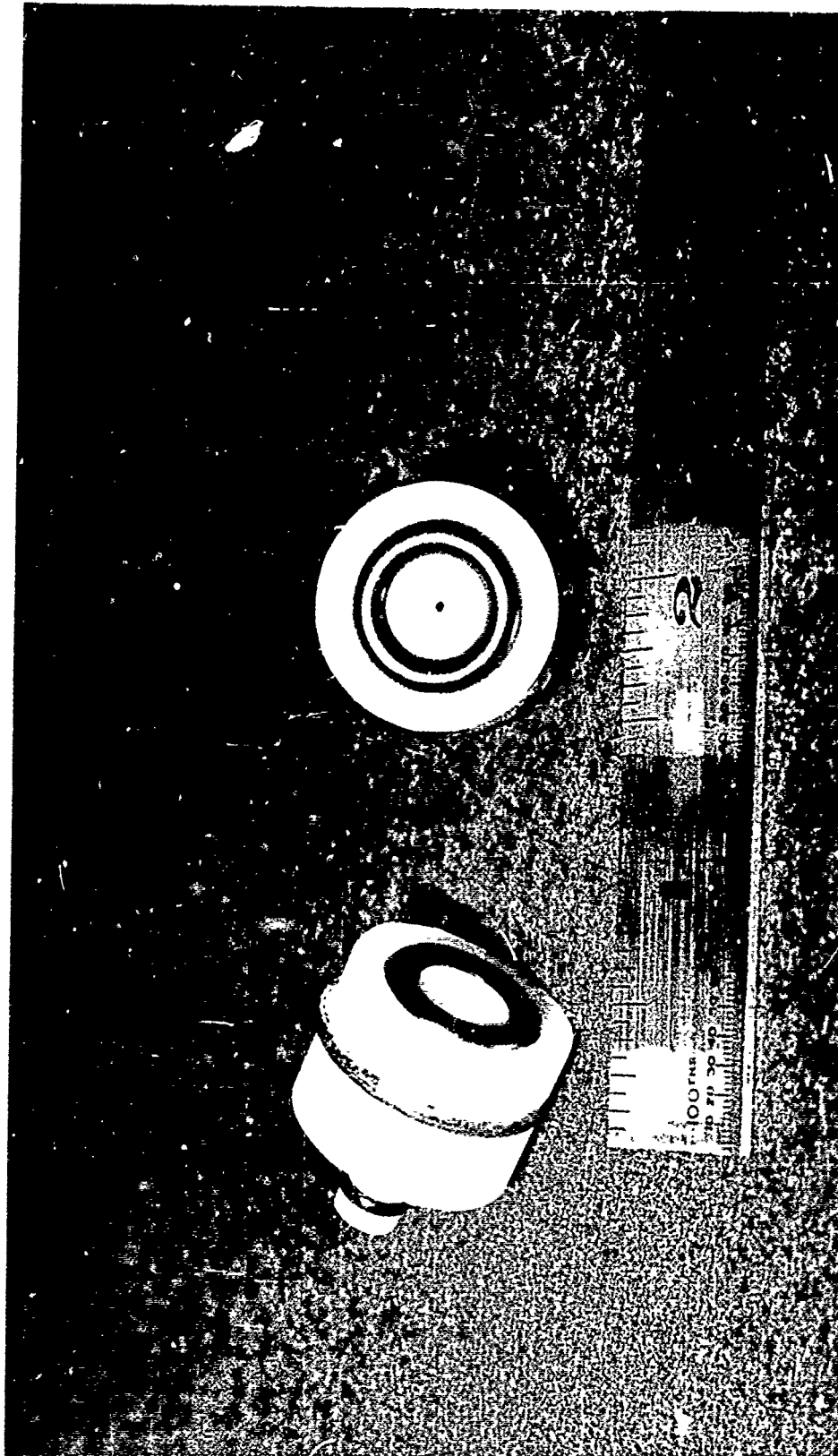


Figure 11. Photograph of Pressure Tap Seal Units

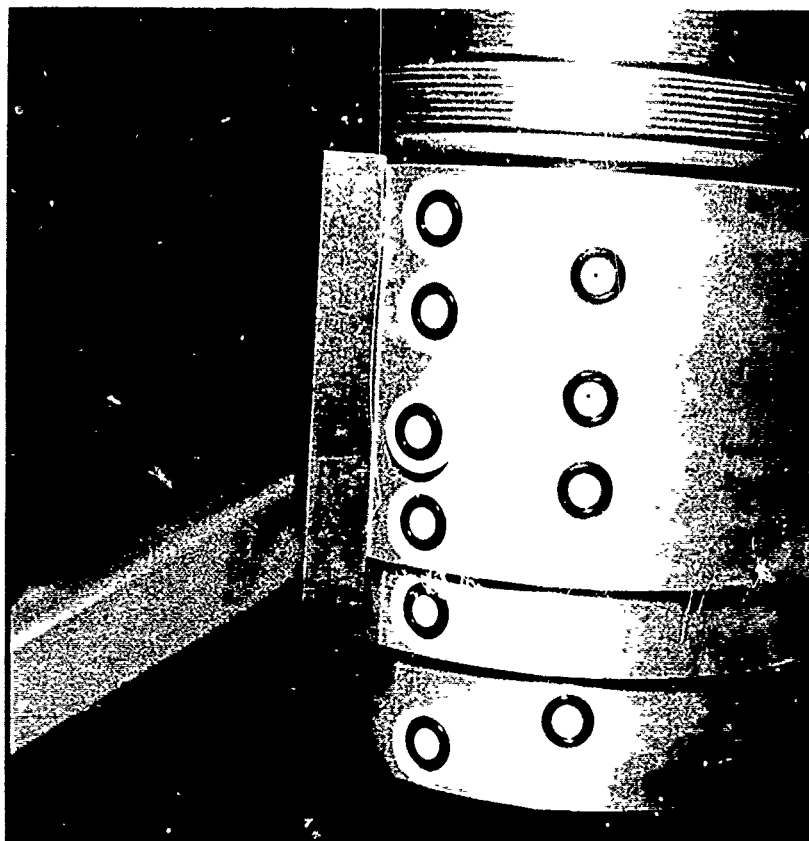


Figure 12. Photograph of Model Boattail
Section of Core Showing Installed
Pressure Tap Seal Units

oil. Pressure measurements at various points on the surface of the spinning body were obtained by positioning the core and the attached tap to different roll attitudes relative to the angle-of-attack plane. This was accomplished by means of a remotely settable roll head located between the model sting and the tunnel angle-of-attack sector sting. The roll head allowed the model core to be sequentially set to various roll orientations.

The steel shell was made up of two basic parts. The forward part included the ogive and most of the cylindrical section. The aft part included the boattail and the portion of the cylindrical section in the area of the rotating band. The model could be tested with or without the rotating band by simply changing the aft part of the shell. Figure 13 shows the aft shell section that included the rotating band. The rotating band, which represented a post-fired condition, was machined directly into the aft shell section. Vent holes were also located on the rotating band lands and grooves, allowing measurements at these positions. The model included an enclosed base similar to the actual projectile.

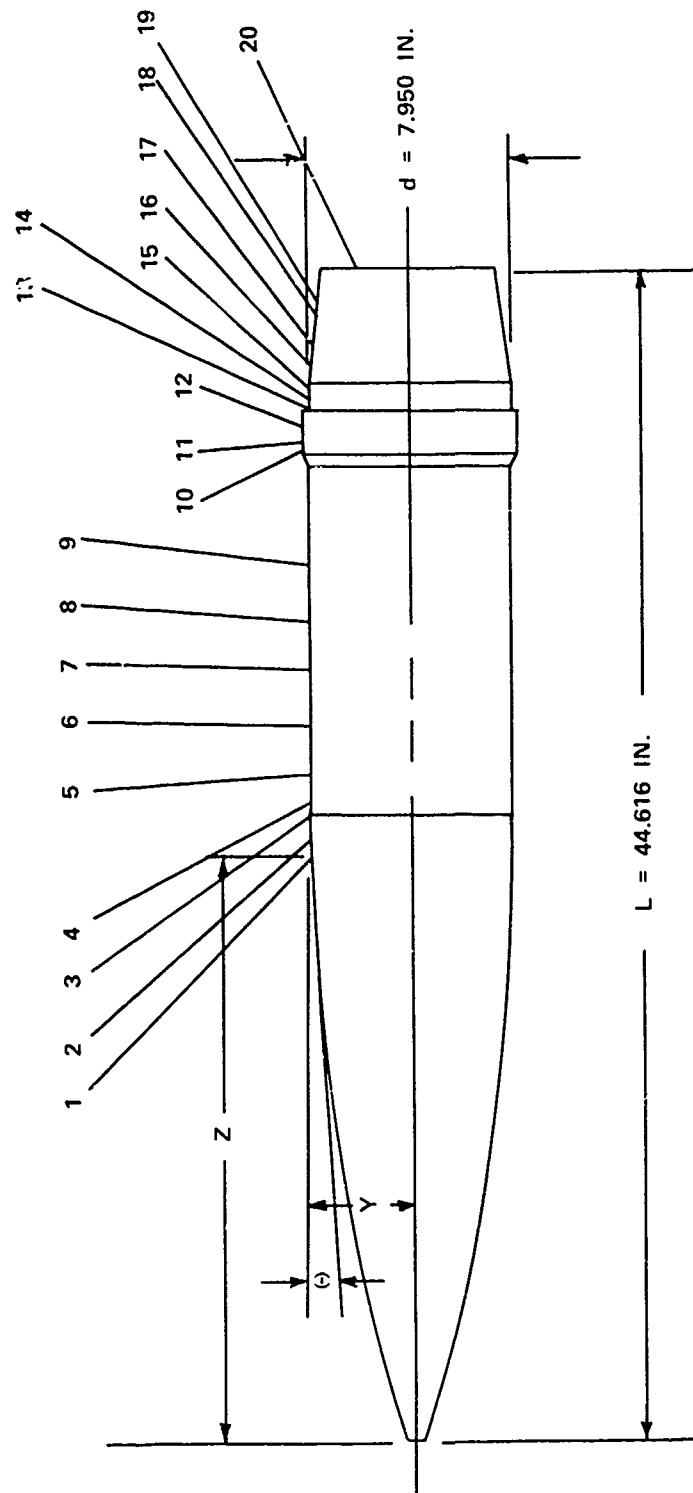
The longitudinal locations of the pressure taps for the 20 vent holes are defined in Figure 14. The tap locations were selected to match those used in the non-spinning surface pressure model used in the Langley tests. Some taps were offset 30 degrees to the main line of taps to allow closer longitudinal spacing than could be achieved with the seal units in a single line. The taps were concentrated over the cylindrical and boattail portion of the model because the Magnus effect primarily occurs in this area. Also, the flow over the ogive and the resultant small Magnus effect can be analyzed quite accurately by current theoretical means. One tap was located to measure the surface pressure on the base of the model at a radial location .09 calibers in from the edge of the boattail. Detailed drawings of the model and sting components are included in Appendix D.

All operation and instrumentation wiring and tubing were routed from the model to a special console located outside the tunnel test section through a hole .875 inch in diameter located down the length of the model sting. This hole contained the operating wires, thermocouple wires, and the cooling water tubing for the motor, the scanivalve operating wires, the engagement pneumatic pressure tubing and signal pressure tubing for the taps, and the thermocouple wires for the model bearings. The instrumentation and operating interfaces are detailed in Figure 15. The water-cooled, variable frequency/variable voltage electric motor was rated at 5 hp for the nominal 5,000 rpm model spin rate. This condition was easily achieved with 150 V/150 cps obtained from the tunnel generator system. The motor operated at about 10 amps and the motor temperature never exceeded 100 °F even after sustained operation of up to 8 hours. Model spin was smooth and, once established, never varied more than 50 rpm from the nominal 4,900 rpm. Engagement of a pressure tab seal unit reduced the spin rate about 100 rpm. Model bearing temperatures never exceeded 100 °F even under sustained spinning for several hours with the tunnel operating at a stagnation temperature of 130 °F. The model had no perceivable pitch or yaw motion during the test and possessed no vibration under all conditions of spin and angles of attack. During this test, the model was spun at 5,000 rpm for a total of 55 hours. Even after these 16,500,000 revolutions, the model bearings appeared to be as good as new. A photograph of the model installed in the wind tunnel test section is shown in Figure 16. The model core weighed 100 pounds, the model shell, 65 pounds, and the model sting, 85 pounds.



Figure 13. Photograph of Boattail Section of Model Shell

TAP NO.	TAP LOCATION				TAP LOCATION NOTES	TAP CIRCUMFERENTIAL LOCATION WRT MAIN TAPS (DEG)
	Z (IN.)	Z/L	Z/d	Y (IN.)		
1	22.449	.503	2.824	3.875	OGIVE	0
2	23.450	.526	2.950	3.969	OGIVE/CYLINDER JUNCTION	30
3	23.961	.537	3.014	3.975	CYLINDER	0
4	24.461	.548	3.077	3.975		30
5	25.461	.571	3.203	3.975		0
6	27.461	.615	3.454	3.975	ROTATING BAND	
7	29.461	.660	3.706	3.975		0
8	31.461	.705	3.957	3.975		
9	33.461	.750	4.209	3.975		0
10	37.821	.848	4.757	3.975		30
11	38.321	.859	4.820	3.975	CYLINDER	0
12	38.821	.870	4.883	3.975	CYLINDER/BOATTAIL JUNCTION	30
13	39.616	.888	4.983	3.975	BOATTAIL	0
14	40.116	.899	5.046	3.975		30
15	40.616	.910	5.109	3.975		0
16	41.151	.922	5.176	3.938		0
17	42.159	.945	5.303	3.813		30
18	43.236	.969	5.438	3.688		0
19	43.725	.980	5.500	3.625		30
20	44.616	.994	5.578	2.750	BASE	90



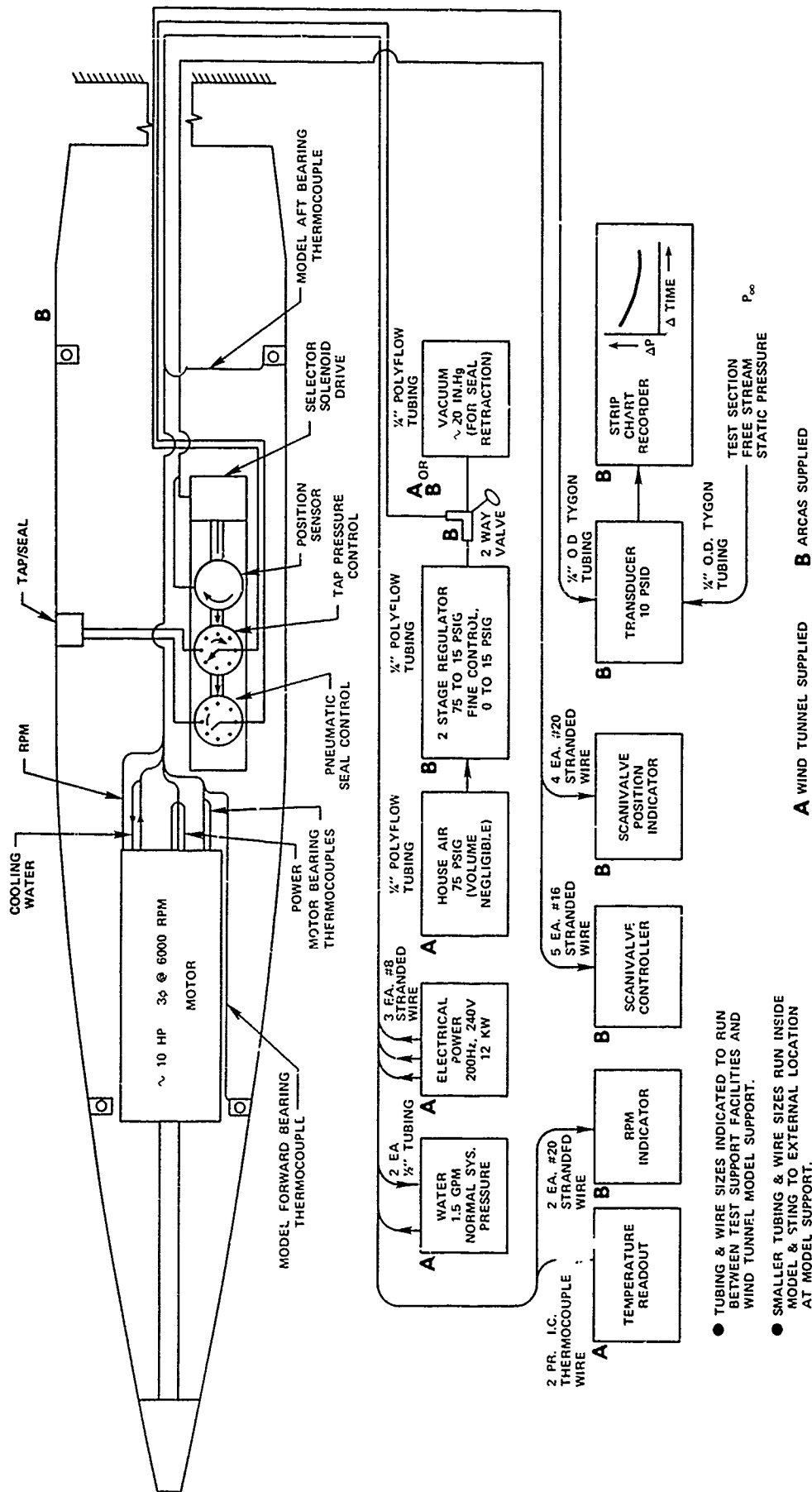


Figure 15. Details of Model Operation and Instrumentation Interfacing

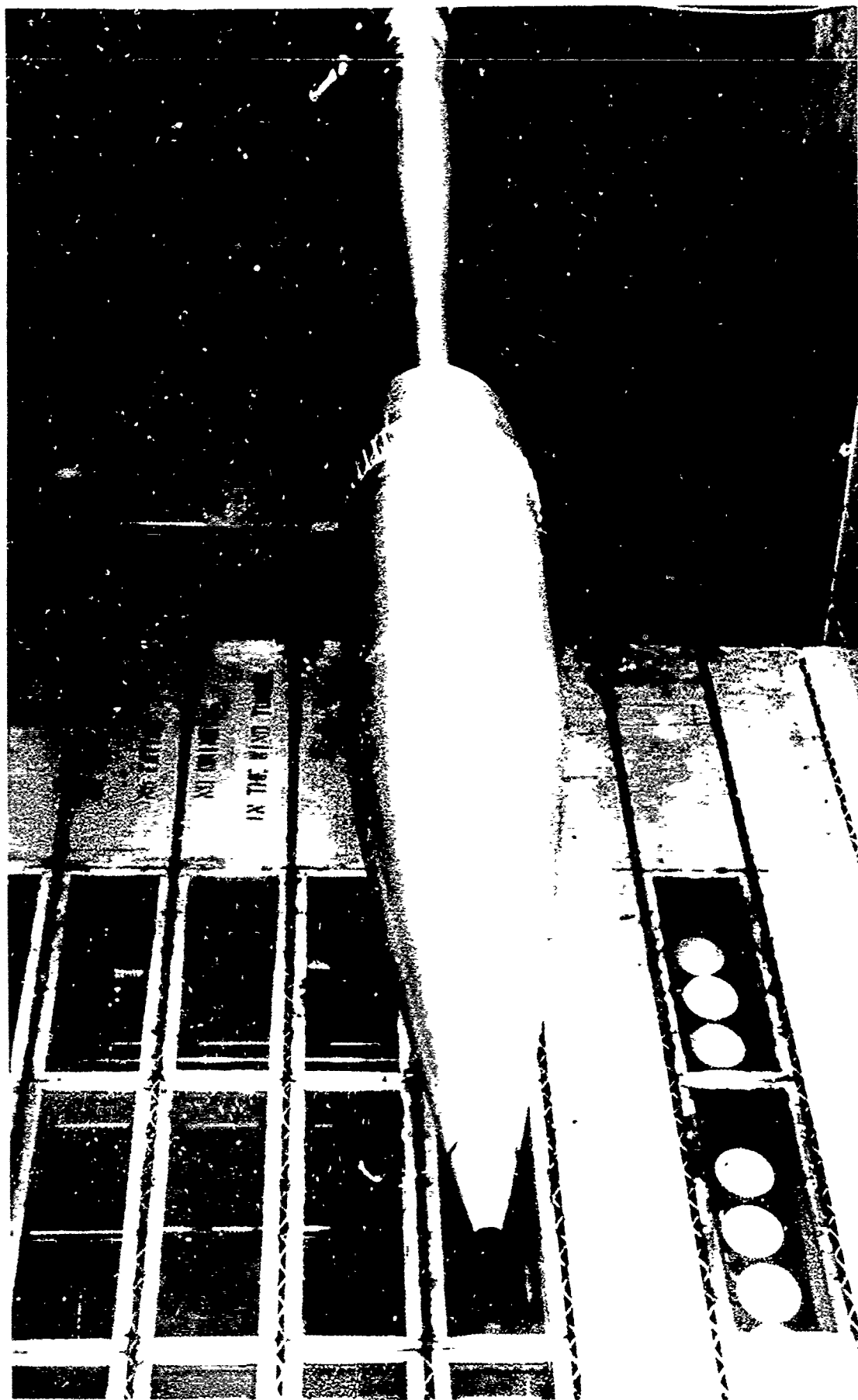


Figure 16. Photograph of Model Installed in 14-Foot Transonic Wind Tunnel



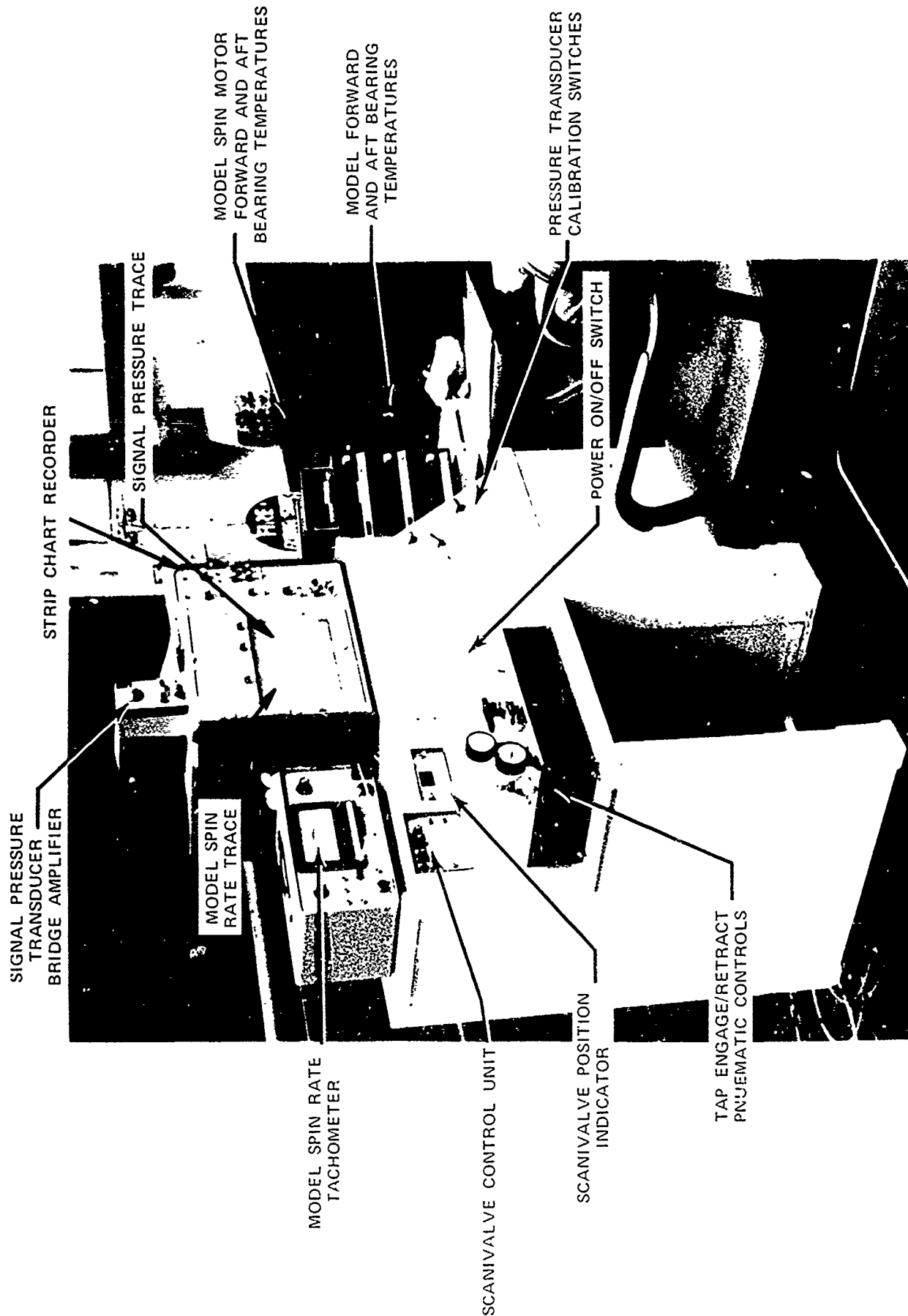
Figure 16. Continued

The special console, shown in Figure 17, was located in the tunnel control room and contained the single differential pressure transducer used to measure the surface pressure of the model with respect to the test section's free stream static pressure. The strip chart recorder continuously displayed the output of the pressure transducer as a function of time, thereby allowing the quality of the data to be assessed as testing proceeded. The console included the capability to remotely zero and calibrate the transducer while the tunnel was operating. Pressure tap selection, engagement, and disengagement were accomplished by controls located in the console. The model rotational speed and critical model bearing temperatures were also monitored with instrumentation located on the control console. Changes in the angle of attack, roll head movement, and model spin motor operations were controlled by wind tunnel personnel. Calibration of the roll angle of the model core was done by machining an indexed flat surface on the model sting. This surface was aligned with the primary row of model pressure taps as the zero degree reference. A clinometer placed on the flat allowed model roll alignment to within 1 minute of arc.

4. TEST PROCEDURE

The wind tunnel test program is summarized in Figure 18. All testing was done at a Mach number of 0.94. The model was tested at angles of attack of 0, 4, and 10 degrees for model spin rates of 0 and 4,900 rpm. Because of the constant circumferential pressure distribution for the runs at 0 degree angle of attack, pressures were measured at 45-degree increments of roll, resulting in eight readings per longitudinal location. For the runs at 4 and 10 degrees angle of attack, pressures were measured every 10 degrees of roll, resulting in 36 readings per longitudinal location. Due to time constraints, data for the model with the rotating band were only taken at 0 and 10 degree angles of attack. Also, only the 12 rear most taps were used for the rotating band case because the presence of the band did not affect the forward pressures.

The test procedure was to establish the tunnel air flow at the test Mach number for a given model configuration and angle-of-attack condition. The model was spun up to the desired test spin rate. A single pressure tap seal unit was then remotely engaged by means of the scanivalve selector, which directed high-pressure air to the tap location. A pneumatic pressure of about 5 psi was sufficient to force the designated tap o-ring out against the inner surface of the model shell to provide the sliding seal function. The engaged pressure tap was then able to detect the surface pressure at that location. When the pressure was visually determined to be constant from the strip chart recorder, the wind tunnel data acquisition system recorded the value, reduced it to coefficient form, and printed it out along with the tunnel conditions at that time. The model core was then rotated to the next circumferential position by means of the remotely controlled roll head and the procedure repeated until a complete circumferential circuit was completed. Figure 19 presents a portion of the strip chart record. About 60 to 90 seconds were required for the measured pressure to reach its constant equilibrium value. This pressure was directed through the second scanivalve and down the model support sting via plastic tubing to the pressure transducer located in the data recording console. At the completion of a circumferential circuit, the tap was disengaged and the next tap engaged. Engagement and disengagement of seals could be accomplished remotely while the model was spinning and the tunnel operating.



WIND TUNNEL TEST PROGRAM NASA AMES 14-FT TRANSONIC TUNNEL TEST NO. 463, 8 FEB 83 - 6 MAR 83

SERIES NUMBER	ROTATING BAND	MACH NO.	ANGLE OF ATTACK (DEG)	PRESSURE READINGS			CIRCUMFERENTIAL INCREMENTALS	RUN NUMBER
				LONGITUDINAL LOCATIONS	CIRCUMFERENTIAL LOCATIONS			
1	OFF	.94	0	20	8		45°	7-11, 12-25
2			↓		↓		↓	73-92
3			4		36		10°	30-49
4			↓		↓		↓	98-112
5			10				↓	113-122, 127-135
6			↓		↓		↓	50-69
7	ON		0	10	8		10°	144-154
8			↓		↓		↓	181-192
9			10		36		10°	157-168
10			↓		↓		↓	169-180

*NOTE: 1) SPIN RATE CORRESPONDS TO $pd/2V$ OF .162 FOR 7.95 INCH DIAMETER MODEL.
2) NOMINAL TEST SECTION CONDITIONS: $T_o = 130^{\circ}F$, $R_d = 4 \times 10^6/FT$, $q = 743 \text{ LB/FT}^2$,
 $P_{\infty} = 8.35 \text{ LB/IN}^2$

Figure 18. Wind Tunnel Test Program

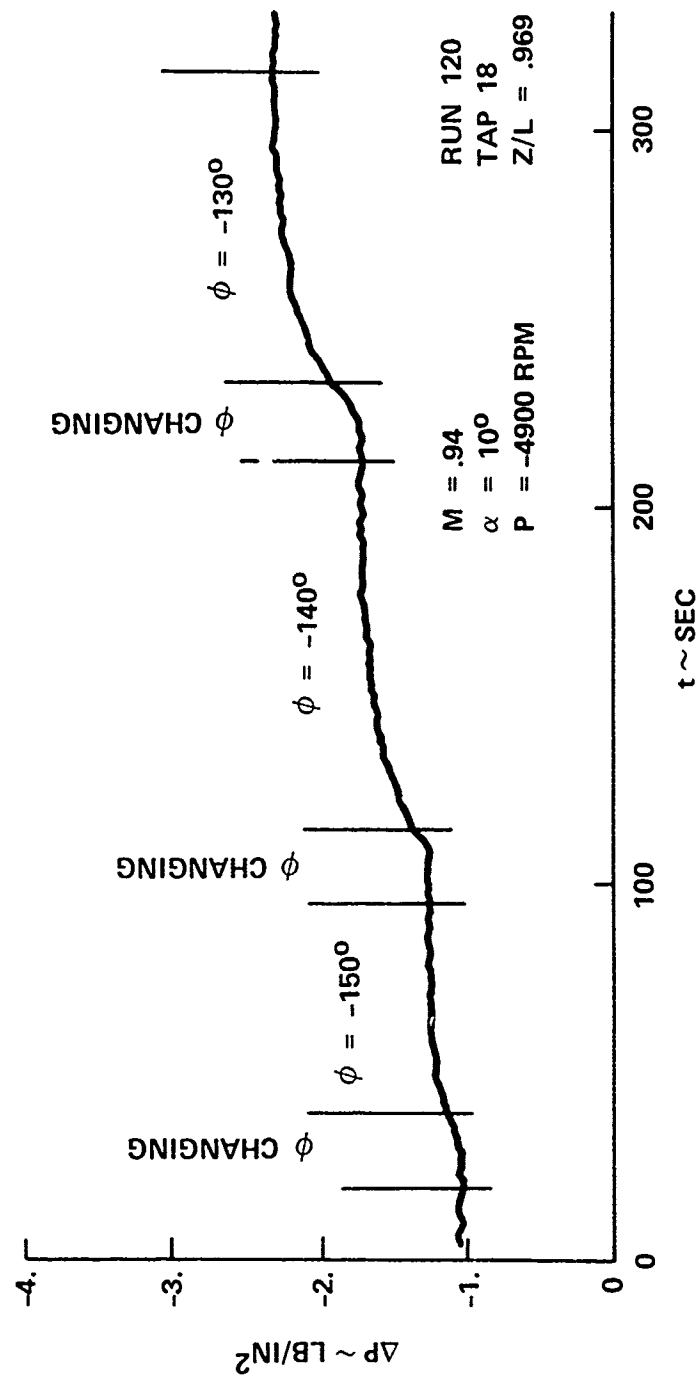


Figure 19. Typical Surface Pressure Measurements

The relatively long time required for the pressure to become constant was due to the 150-foot length of tubing between the model and the transducer. This resulted in seal engagement times of about 40 minutes to complete a circumferential survey at a particular longitudinal location. Over 12 hours were needed to test a single model configuration. Locating the transducer in the control room had several advantages, such as ease of calibration, absence of temperature effects, and the provision of pressure pulse damping volume. With the test method validated, in future use of this technique, the transducer could be located in the model or in the sector sting with a marked reduction in tube length, pressure lag time, and consequent data acquisition time.

After each spinning test, the shell was removed and the o-rings changed. In most cases, the o-rings showed little or no wear. In fact, one seal was engaged for over 75 minutes without experiencing any detectable wear. However, certain tap locations did produce severe o-ring wear, as noted in Table 1. For the non-spinning tests, the model shell was simply locked to the core by a set screw with the vent holes aligned with their respective taps. This allowed the shell and core to be rotated together by the roll head. Certain operational difficulties were encountered during the initial portion of the test. When fully retracted, the seal blocks would cover the pneumatic port, reducing the effective base area over which the engaging air pressure could act. Also, in the retracted position, the clearance between the seal block and the inside diameter of the shell was great enough to occasionally allow an o-ring to escape from its groove in the seal block. Both problems were effectively eliminated by placing a wire ring with a 0.30-inch diameter beneath the seal block. This prevented the base of the seal block from covering the pneumatic pressure port and reduced the clearance between the shell and seal so that the o-ring could not be dislodged from its groove in the seal block. It was found that 600,000 CS silicone fluid could be used to help retain the o-rings in their grooves. Following an o-ring change, each seal was sequentially engaged and the shell manually rotated back and forth to mate the contour of the seal with the internal contour of the shell to ensure seal engagement and alignment with the inside surface of the shell. The seals were then retracted prior to starting of the test run.

5. ANALYSIS OF RESULTS

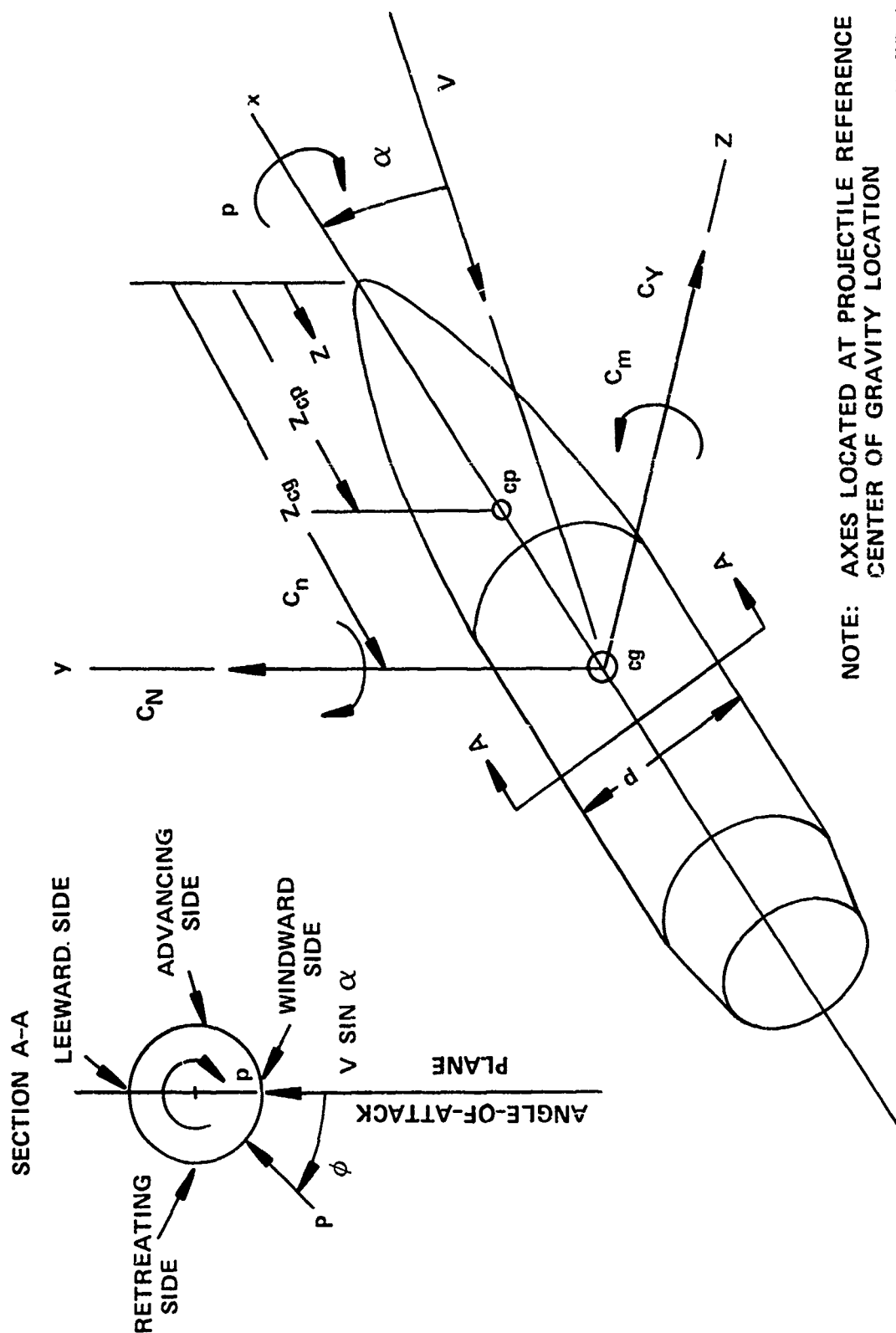
5.1 General.

The surface pressure data were reduced to coefficient form as defined in Figure 20. All of the wind tunnel data are tabulated in Appendix A, which lists the pressure coefficient measured at each circumferential and longitudinal location for a particular test run. The data are also provided in plotted form in Appendix B. The differential pressures measured and the associated pressure coefficients are plotted as a function of circumferential angle for each longitudinal tap location. Each set of data is presented for a specific model configuration for both the spinning and non-spinning cases. These data are available for use in evolving or validating theoretical or computational fluid dynamic analyses of the Magnus effect.

The following sections include examples of specific effects and observed phenomena obtained during this test.

Table 1. Summary of O-Ring Wear During Test

RUN	TAP NO.	ROTATING BAND	α (DEG)	COMMENTS
81	9	OFF	0	GREASE BLACKENED AROUND SOME SEALS, NO NOTICEABLE WEAR ON ANY O RINGS, DATA APPEARED OK
92	20		4	O RING HAD SOME SURFACE SCRATCHES
93	1		4	O RING BADLY WORN, DATA ERRATIC
102	10		10	O RING WORN
127	1		10	O RING WORN, O RING MATERIAL TRANSFERRED TO SHELL
144	14	ON		O RING WORN, O RING MATERIAL TRANSFERRED TO SHELL
145	15			O RING WORN, O RING MATERIAL TRANSFERRED TO SHELL
146	16			O RING WORN, O RING MATERIAL TRANSFERRED TO SHELL
152	10			O RING BAD
153	11			O RING WORN
164	16		0	O RING WORN
165	17			O RING WORN
166	18			SEALBLOCK STEM BROKEN, ALLOWING PNEUMATIC AND TEST PRESSURES TO COMMUNICATE



NOTE: AXES LOCATED AT PROJECTILE REFERENCE
CENTER OF GRAVITY LOCATION

x - AXIS LIES ALONG PROJECTILE CENTER LINE

y - AXIS IS NORMAL TO x - AXIS AND LIES IN
ANGLE-OF-ATTACK PLANE

z - AXIS IS NORMAL TO ANGLE-OF-ATTACK PLANE

Figure 20. Definition of Terms

5.2 Surface Pressure Distribution.

Figure 21 shows the pressure measured along the projectile for an angle of attack of 0 degrees for both the spinning and non-spinning cases. Note that spin produces slightly reduced pressures at most locations. These data illustrate the ability of the testing method to accurately measure even these small pressure effects. During the test, pressure differences of .025 psi could be determined. The non-spinning data in Figure 21 show excellent agreement with the previous NASA-Langley test data.

Figure 22 contains circumferential surface pressure data at a point on the boattail under spinning conditions. The model was spun in a counter-clockwise direction (pilot's view) in order to provide a tightening effect on the right-hand threaded shell components. This negative spin resulted in a positive Magnus force as defined in Figure 16. Data are shown for two separate tests and illustrate the excellent repeatability obtained, even for the severe pressure variations present.

Figure 23 shows similar pressure data measured on another boattail location for the model spinning in opposite directions. These data illustrate that no asymmetric bias was present with the model or instrumentation. The Magnus effect is clearly illustrated in Figure 24, which shows the difference in the circumferential pressure distribution due to spin. A net negative pressure difference is produced on the retreating side of the projectile and a positive pressure difference on the advancing side, resulting in an additive effect to the Magnus force. These data indicate that spin produces both a circumferential shift as well as a distortion of the non-spinning pressure distribution.

The effect of angle of attack on the circumferential surface pressure distribution at a point on the boattail under spinning conditions is shown in Figure 25. Note that the pressure asymmetry that produces the Magnus force is most pronounced at the largest angle of attack. The resultant local force in the angle-of-attack plane denoted by C_{N_i} (computed by integrating the circumferential pressure distribution) does not change with angle of attack for this location. However, the resultant force normal to the angle-of-attack plane C_{y_i} (i.e., the Magnus force) increases nonlinearly with angle of attack. These data also illustrate the presence of a negative pressure "hump" on the advancing side of the leeward point of the projectile ($\phi = 140$ degrees). This effect is present at all longitudinal locations for the spinning projectile at an angle of attack of 10 degrees, as illustrated in Figure 26, but does not occur at an angle of attack of 4 degrees. This hump may be due to the presence of an attached vortex on the leeward side of the projectile at the larger angle of attack.

5.3 Force and Moment Distribution.

The circumferential pressure distributions were integrated to determine the resultant normal force (in the angle-of-attack plane) and side force (normal to the angle-of-attack plane) at each longitudinal tap location. These local forces are presented in coefficient form as C_{N_i} and C_{y_i} , respectively as defined in

Figure 20. These coefficients indicate the detailed influence of the Magnus effect at various longitudinal positions on the projectile.

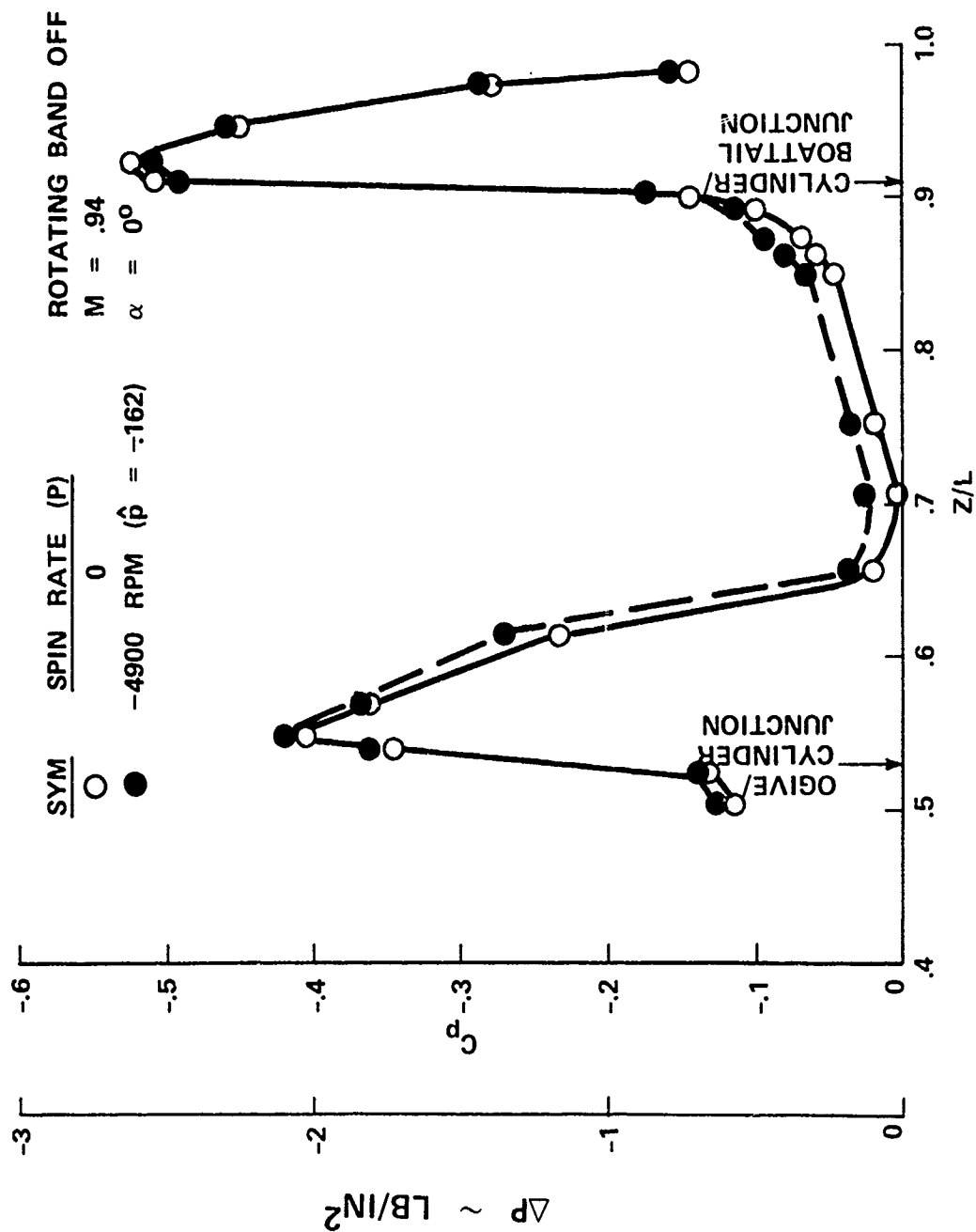


Figure 21. Effect of Spin on Longitudinal Surface Pressure Distribution for $\alpha = 0$ Degrees

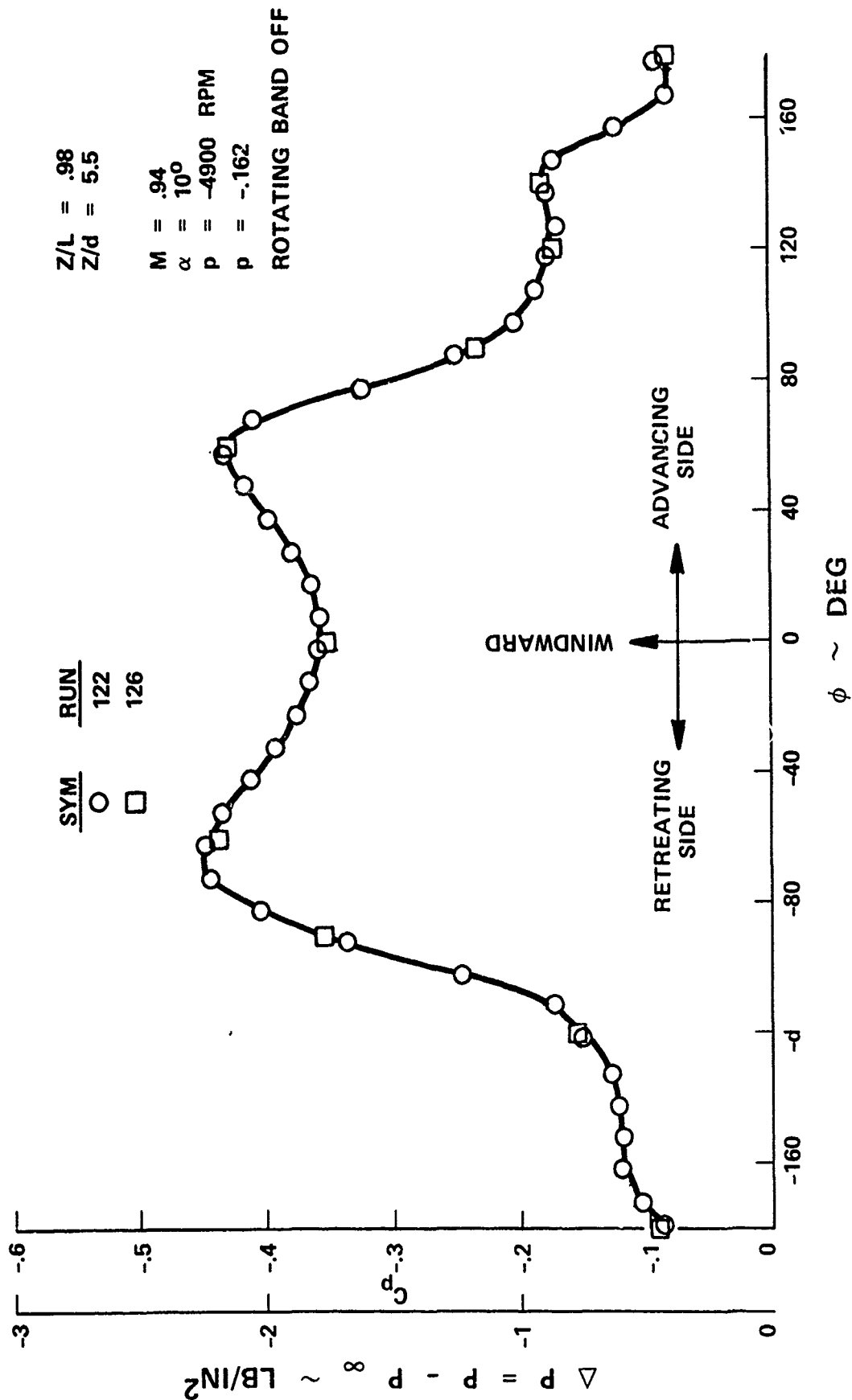


Figure 22. Circumferential Pressure Distribution on Boattail -
Demonstration of Repeatability

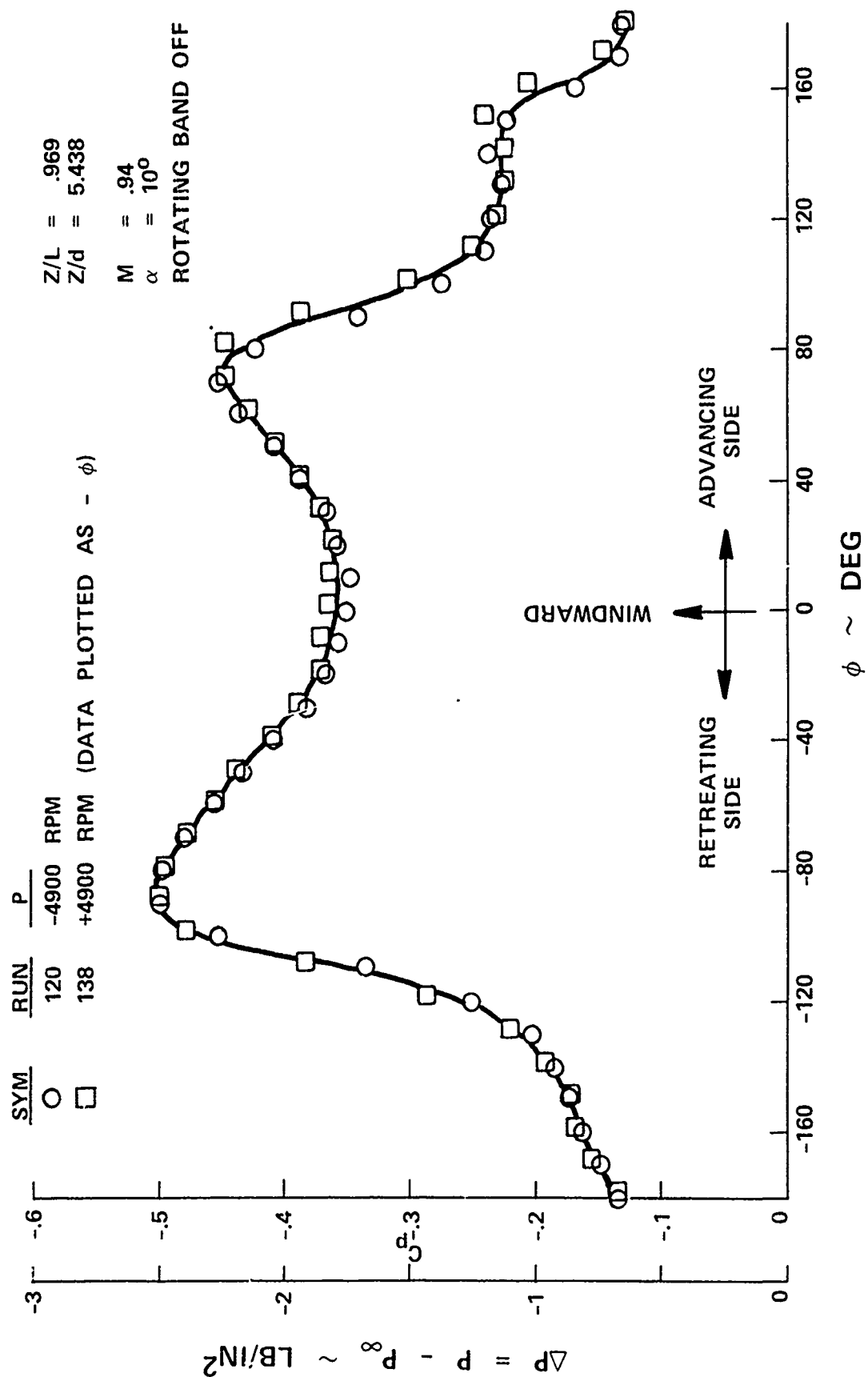


Figure 23. Circumferential Pressure Distribution on Boattail -

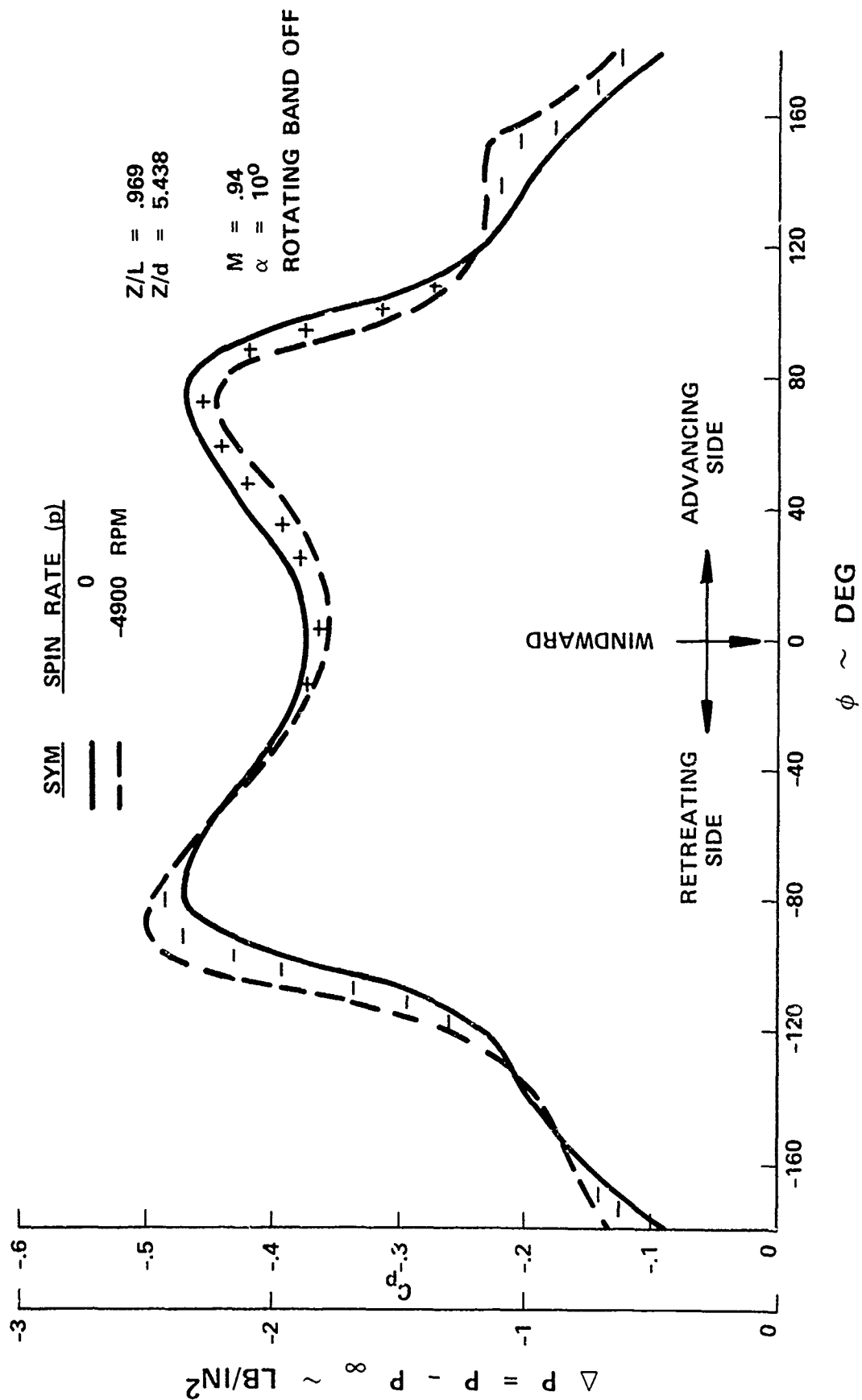
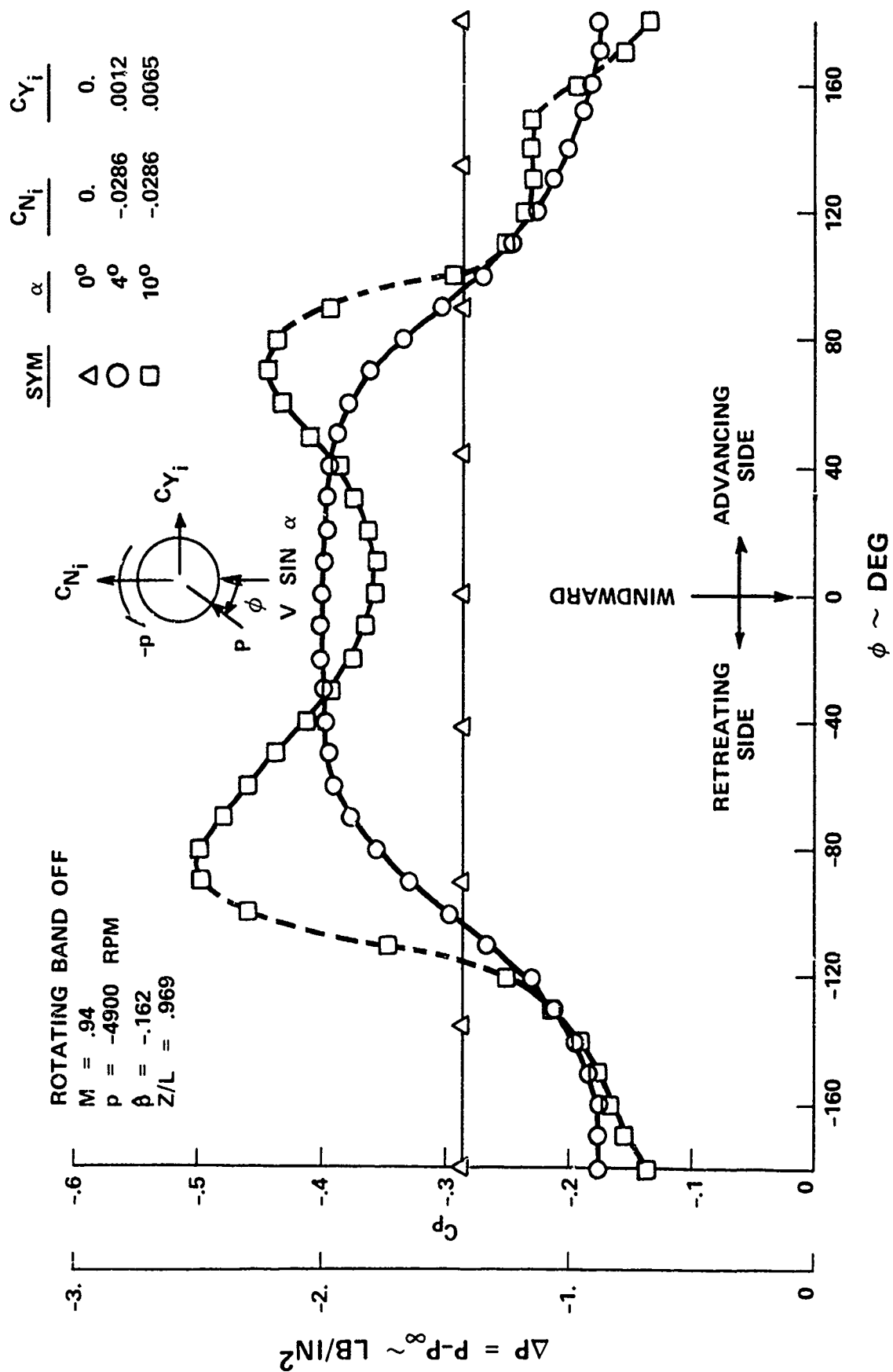


Figure 24. Effect of Spin on Boattail Circumferential Pressure



ROTATING BAND OFF

MACH. = .94

$\alpha = 10^\circ$

$p = -4900$ RPM

- = CENTER OF HUMP
- ◊ = LIMITS OF EFFECT

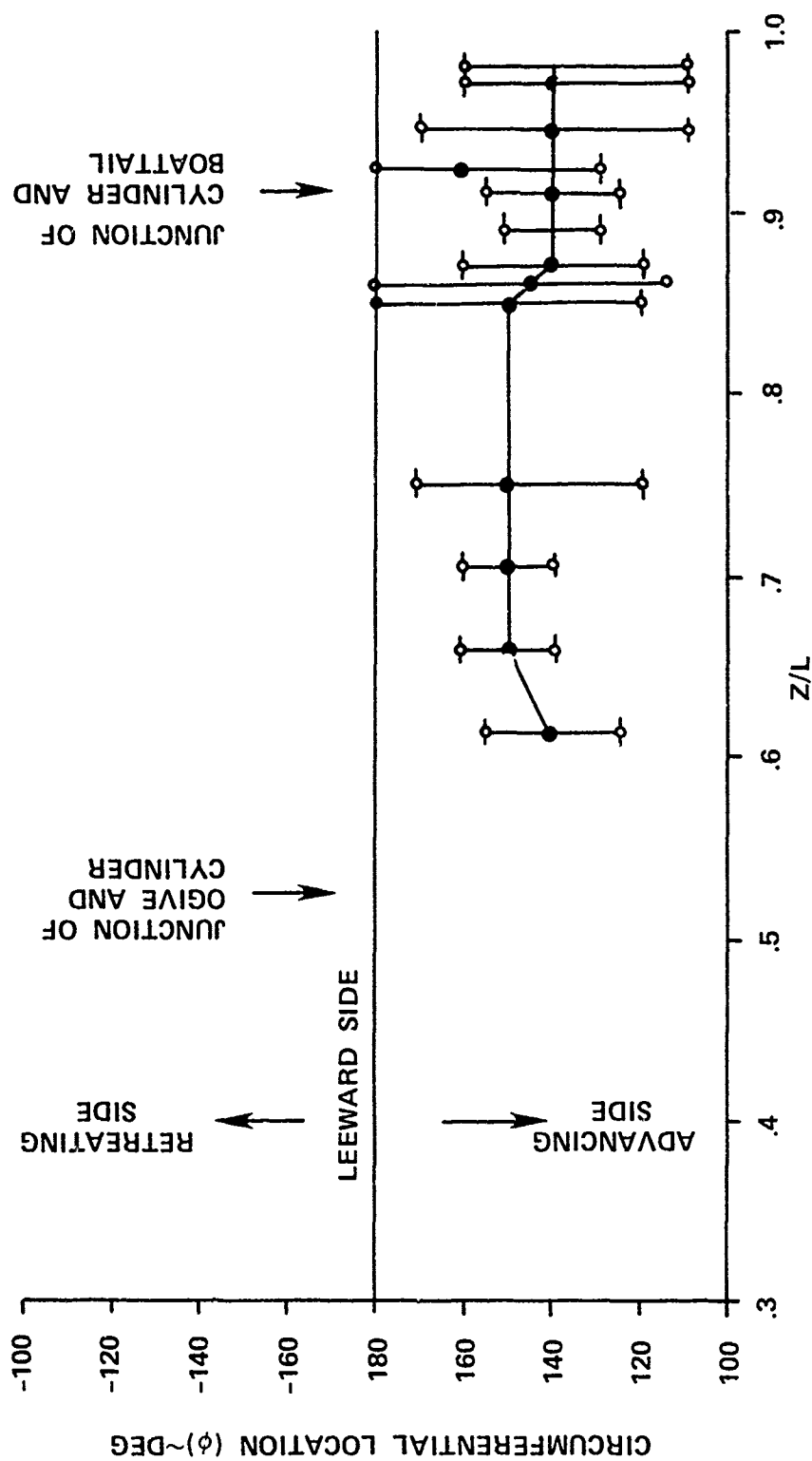


Figure 26. Circumferential Location of Negative Pressure Hump as a Function of Longitudinal Location ($\alpha = 10$ Degrees)

The resulting normal and side force distributions are shown in Figures 27 through 29 for angles of attack of 0, 4, and 10 degrees, respectively. As expected, the Magnus-induced side force is significantly less than the normal force. Figure 30 shows the side force at an enlarged scale, indicating that the largest Magnus effect occurs over the boattail.

Although a net positive Magnus force results for both the 4 and 10 degree angles of attack, there are longitudinal regions on the projectile where the local Magnus force acts in a negative sense. For the 10-degree case, this situation only occurs in the vicinity of the shock waves; whereas for the 4-degree case, it is also present on the cylindrical section and at the aft portion of the boattail. Note that the greatest Magnus side force occurs on the cylindrical portion of the projectile for the 4-degree case and on the boattail for the 10-degree case. A particularly large Magnus side force is present on the boattail at a 10-degree angle of attack. This large Magnus force, in combination with the large moment arm between the boattail and projectile center of gravity, results in a significant Magnus yawing moment.

By integrating the local force coefficients in a longitudinal sense, the normal force and side (i.e., Magnus) force coefficients can be determined for each component (i.e., ogive, cylinder, and boattail), as well as for the total projectile. In a similar fashion, pitching moments and yawing (i.e., Magnus) moments can also be computed, as well as their respective centers of pressure. The moment terms are referred to a reference point representing the nominal center of gravity of the actual projectile located .625 calibers from the nose.

These terms are summarized in Appendix C and include the coefficient derivatives for force and moment with respect to angle of attack and nondimensional spin rates. The detailed derivations of the local normal and Magnus side force and their centers of pressure are also contained in Appendix C. The use of these derivatives both facilitate interpretation of the data and allow comparison with results from other studies. The relative contributions of the various projectile components to the Magnus force and moment terms depicted in Figure 30 are summarized in Table 2. These quantitative values further demonstrate the importance of the boattail in producing the Magnus effect.

The influence of spin on the normal force distribution for angles of attack of 0, 4, and 10 degrees is indicated in Figures 31 through 33. At both angles of attack, the presence of spin decreases the negative normal force acting on the forward portion of the cylindrical section of the projectile and decreases the positive normal force acting over the aft portion of the cylindrical section, which should result in a larger positive force and pitching moment for the spinning case.

The effect of angle of attack on the normal force and moment terms are contained in Table 3 for the non-spinning case and in Table 4 for the spinning case. Tables 5 and 6 show the effect of spin on the normal force and moment terms for angles of attack of 4 and 10 degrees, respectively.

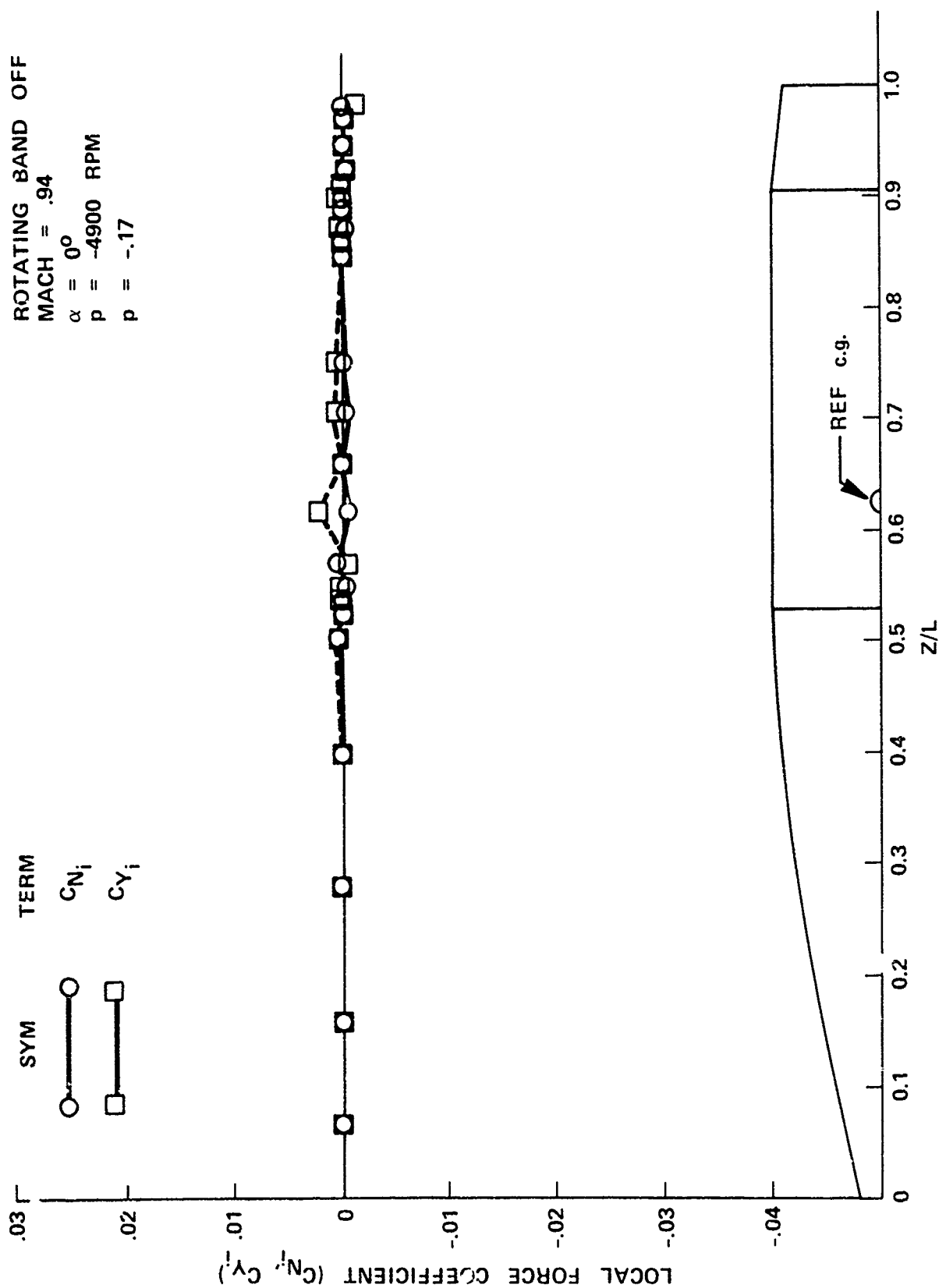


Figure 27. Normal and Side Force Longitudinal Distribution on Spinning Model
($\alpha = 0$ Degrees)

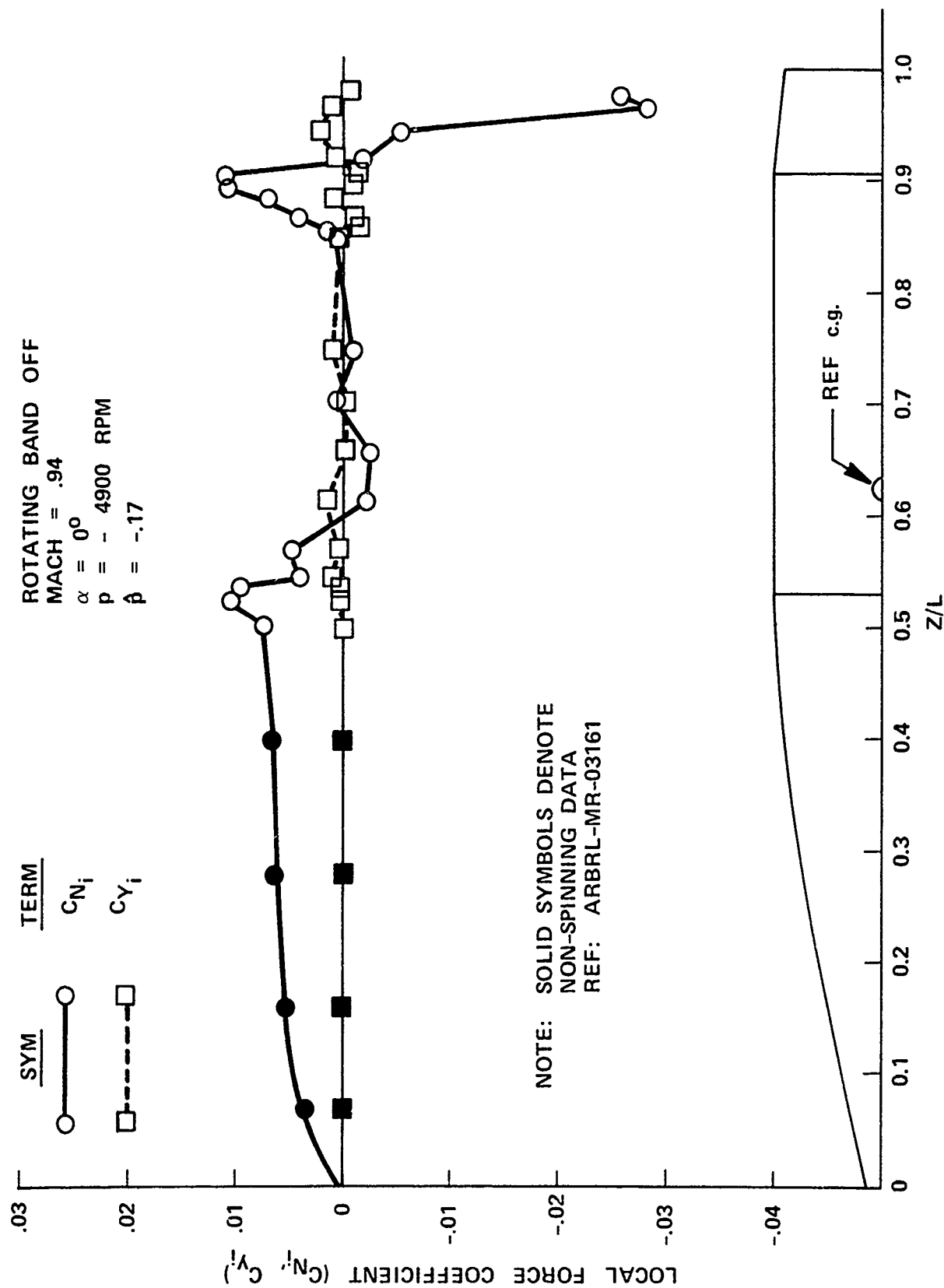


Figure 28. Normal and Side Force Longitudinal Distribution on Spinning Model
($\alpha = 4$ Degrees)

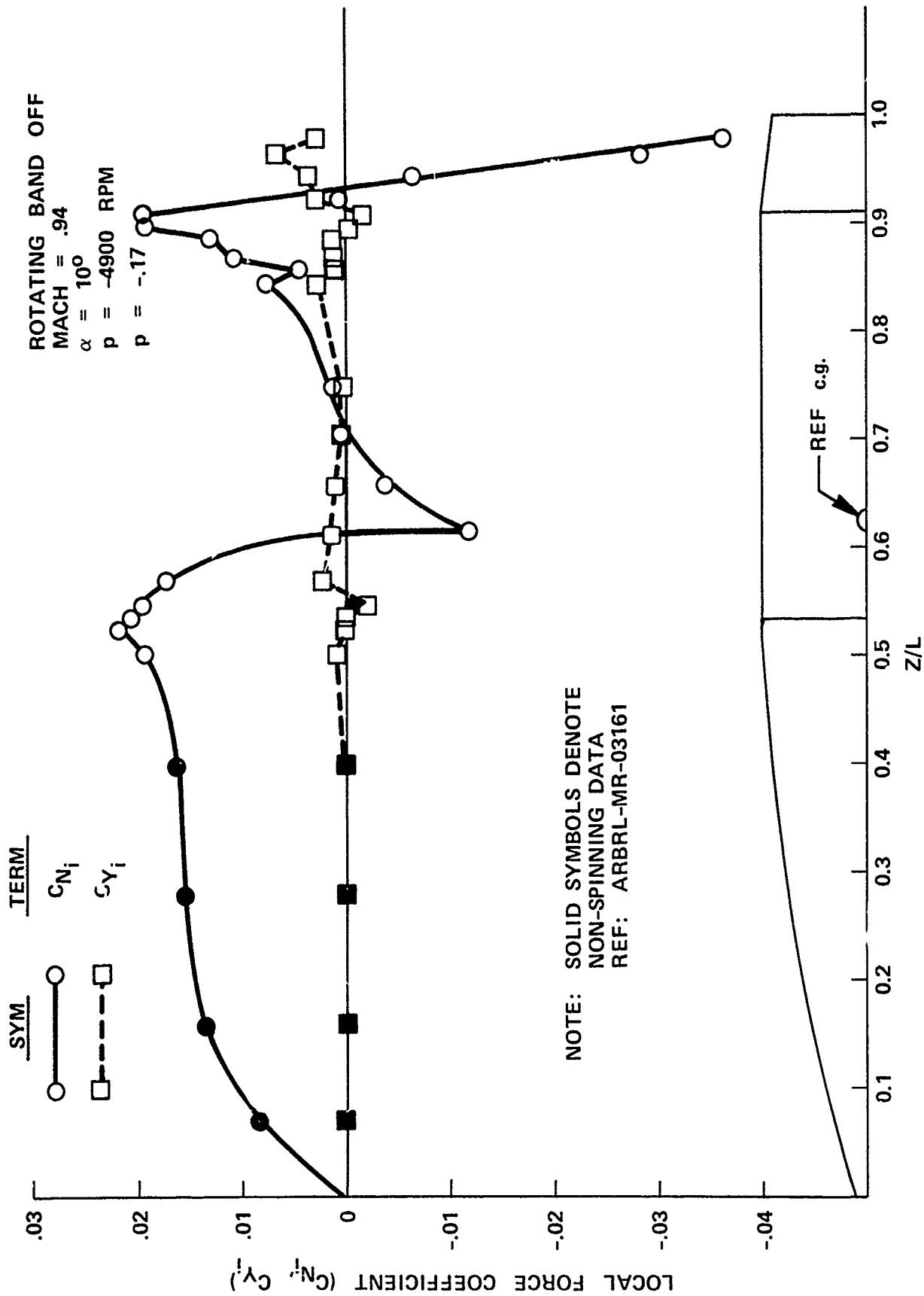


Figure 29. Normal and Side Force Longitudinal Distribution on Spinning Model ($\alpha = 10$ Degrees)

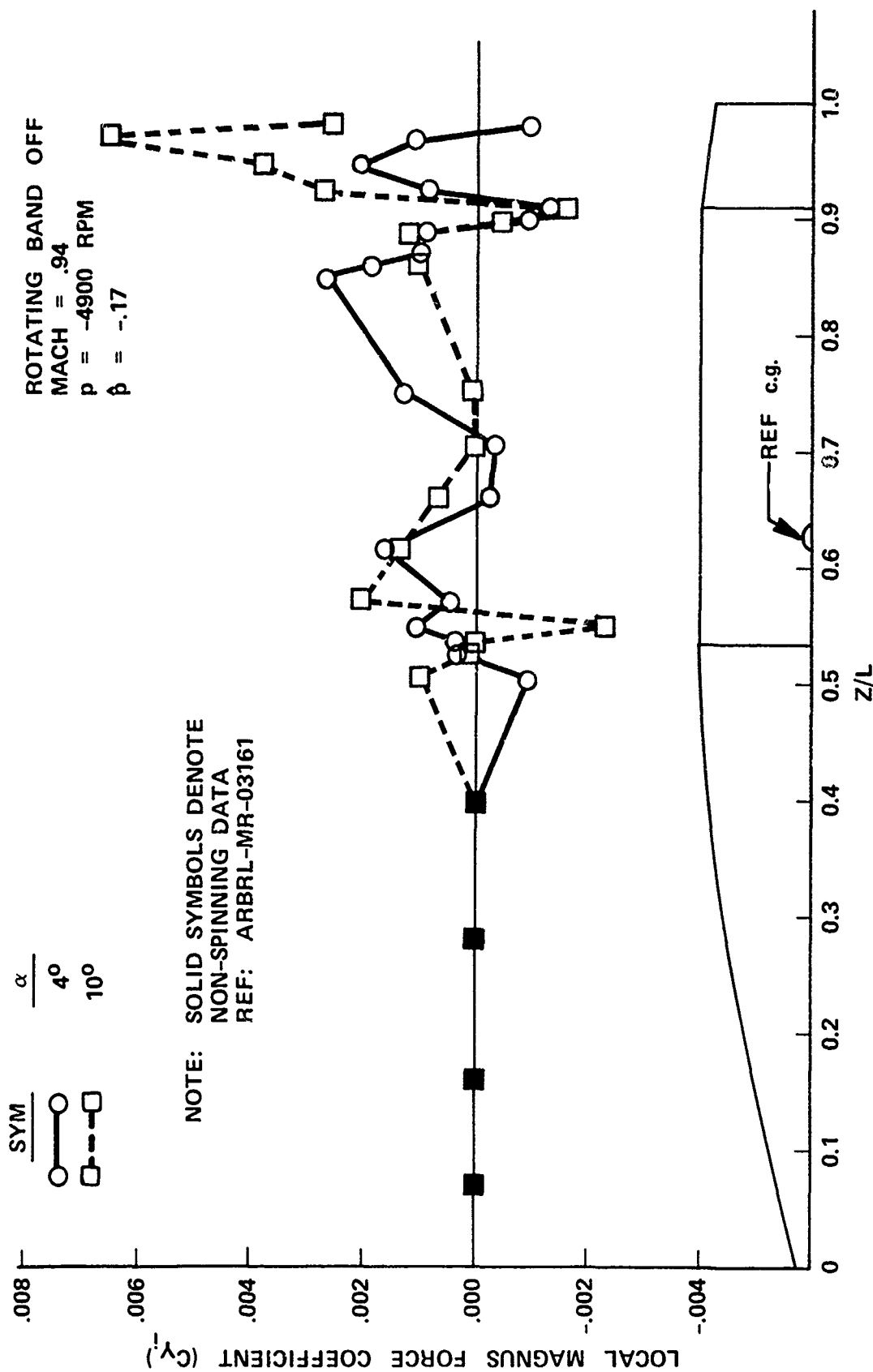


Figure 30. Side Force Longitudinal Distribution on Spinning Model for
 $\alpha = 4$ Degrees and $\alpha = 10$ Degrees

Table 2. Side Force and Moment Terms for $\alpha = 4$ Degrees and
 $\alpha = 10$ Degrees (Rotating Band Off)

	TERM	$\alpha = 4^\circ$		$\alpha = 10^\circ$	
MODEL CONFIGURATION:	3 CALIBER OGIVE	C_{Y_p} (OGIVE)	.000		-.004
	2 CALIBER CYLINDER	C_{Y_p} (CYLINDER)			
	.5 CALIBER BOATTAIL	C_{Y_p} (BOATTAIL)	-.085		-.092
	ROTATING BAND OFF	C_{Y_p} (BOATTAIL)	-.019		-.080
	$Z_{cg}/L = .625$	C_{Y_p} (TOTAL)	-.104		-.176
TEST CONDITIONS:	MACH .94	C_{n_p} (OGIVE)	.000		-.003
	$pd/2V = .162$	C_{n_p} (CYLINDER)	.056		.063
		C_{n_p} (BOATTAIL)	.033		.148
		C_{n_p} (TOTAL)	.090		.208
		Z_{cp}/L (MAGNUS)	.779		.836

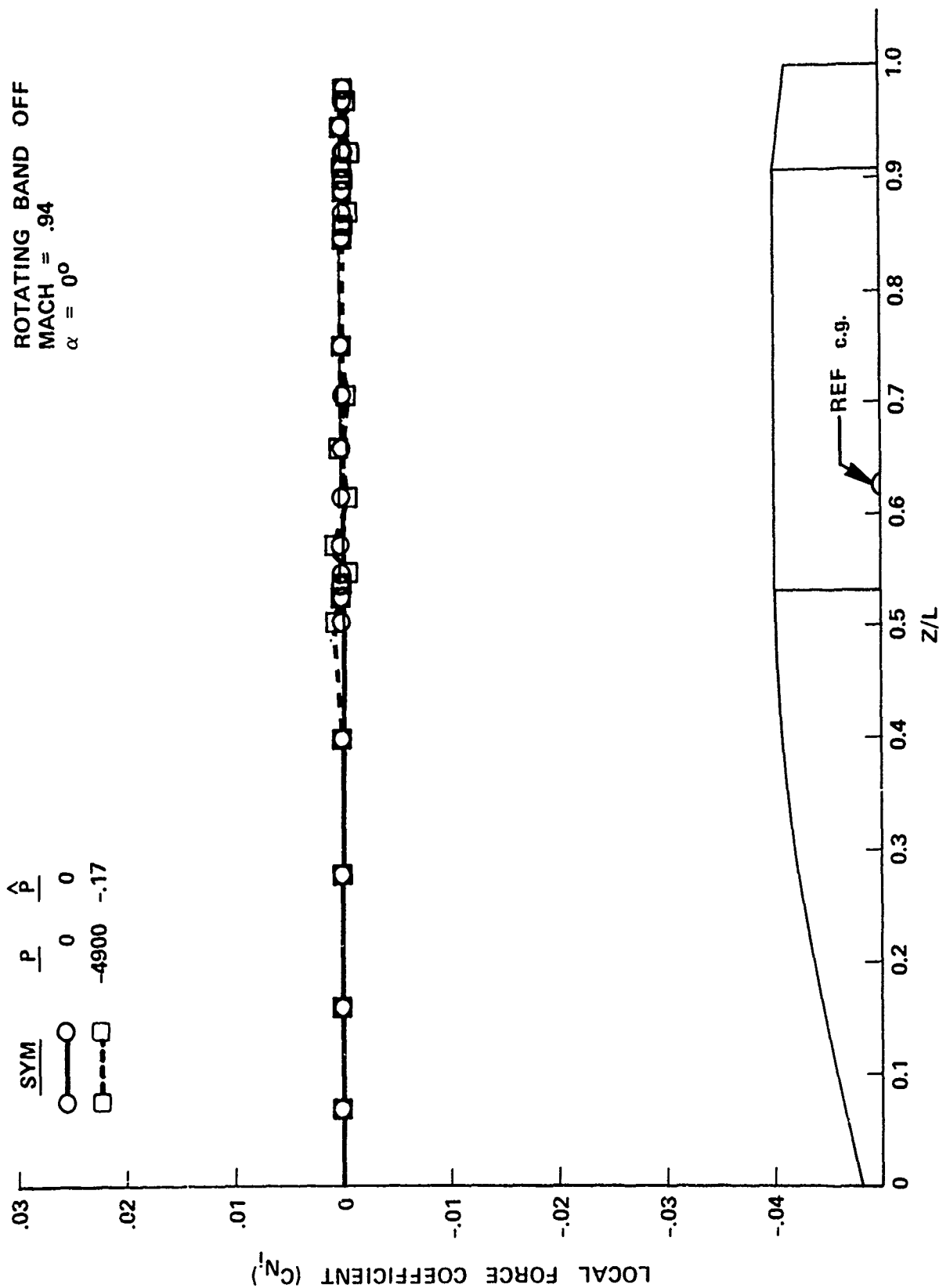


Figure 31. Effect of Spin on Normal force Longitudinal Distribution
($\alpha = 0$ Degrees)

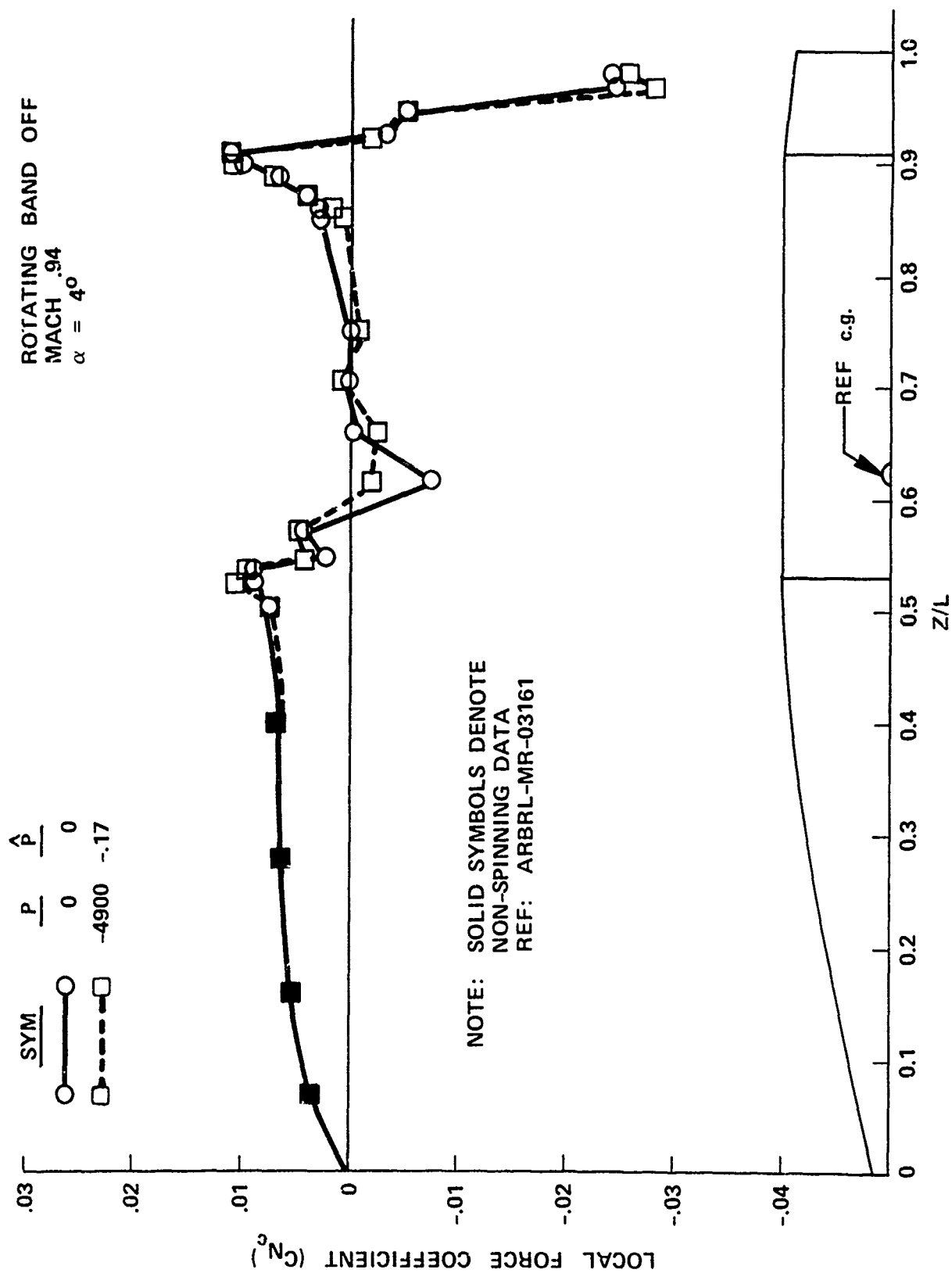


Figure 32. Effect of Spin on Normal Force Longitudinal Distribution
($\alpha = 4$ Degrees)

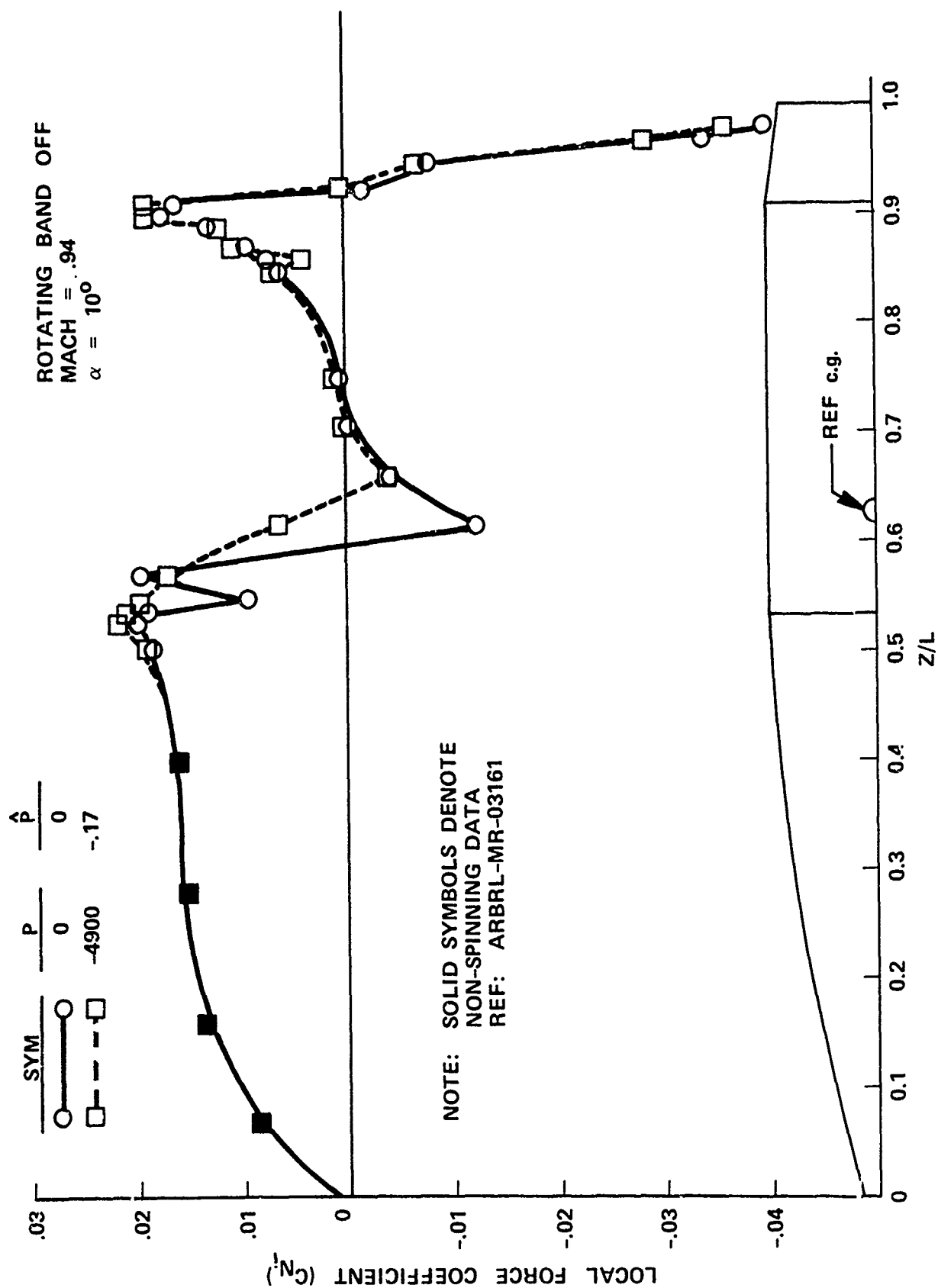


Figure 33. Effect of Spin on Normal Force Longitudinal Distribution
($\alpha = 10$ Degrees)

Table 3. Effect of Angle of Attack on Normal Force and Moment
Terms for $\hat{p} = 0$ (Rotating Band Off)

MODEL CONFIGURATION:	TERM	$\alpha = 4^\circ$		$\alpha = 10^\circ$	
3 CALIBER OGIVE 2 CALIBER CYLINDER .5 CALIBER BOATTAIL ROTATING BAND OFF $Z_{cg}/L = .625$	C_{N_α} (OGIVE)	1.94		1.93	
	C_{N_α} (CYLINDER)	.25		.33	
	C_{N_α} (BOATTAIL)	-.64		-.36	
	C_{N_α} (TOTAL)	1.55		1.90	
TEST CONDITIONS: MACH .94 $pd/2v = 0$	C_{m_α} (OGIVE)	3.45		3.46	
	C_{m_α} (CYLINDER)	-.50		-.35	
	C_{m_α} (BOATTAIL)	1.22		.70	
	C_{m_α} (TOTAL)	4.17		3.82	
	Z_{cp}/L	.15		.30	

Table 4. Effect of Angle of Attack on Normal force and Moment
Terms for $\hat{p} = -.162$ (Rotating Band Off)

MODEL CONFIGURATION-	TERM	$\alpha = 4^\circ$		$\alpha = 10^\circ$	
3 CALIBER OGIVE 2 CALIBER CYLINDER .5 CALIBER BOATTAIL ROTATING BAND OFF $Z_{cg}/L = .625$	C_{N_α} (OGIVE)	1.96		1.94	
	C_{N_α} (CYLINDER)	.30		.60	
	C_{N_α} (BOATTAIL)	-.68		-.31	
	C_{N_α} (TOTAL)	1.59		2.24	
TEST CONDITIONS: MACH .94 $pd/2V = .162$	C_{m_α} (OGIVE)	3.47		3.47	
	C_{m_α} (CYLINDER)	-.36		-.36	
	C_{m_α} (BOATTAIL)	1.30		.60	
	C_{m_α} (TOTAL)	4.41		3.71	
	Z_{cp}/L	.13		33	

Table 5. Effect of Spin on Normal force and Moment Terms for
 $\alpha = 4$ degrees (Rotating Band Off)

MODEL CONFIGURATION:	TERM	$p = 0$ ($\hat{p} = 0$)		$p = -4900$ RPM ($\hat{p} = -.162$)	
8 INCH DIAMETER MODEL 3 CALIBER OGIVE 2 CALIBER CYLINDER .5 CAL BOATTAIL REF c.g. AT Z/L = .625	$C_{N_{\alpha}}$ (OG:VE)	1.94		1.96	
	$C_{N_{\alpha}}$ (CYLINDER)	.25		.30	
	$C_{N_{\alpha}}$ (BOATTAIL)	-.64		-.68	
	$C_{N_{\alpha}}$ (TOTAL)	1.55		1.59	
MACH .94 $\alpha = 4^{\circ}$ $R_d = 4 \times 10^6$ /FT	$C_{m_{\alpha}}$ (OGIVE)	3.45		3.47	
	$C_{m_{\alpha}}$ (CYLINDER)	-.50		-.36	
	$C_{m_{\alpha}}$ (BOATTAIL)	1.22		1.30	
	$C_{m_{\alpha}}$ (TOTAL)	4.17		4.41	
TEST CONDITION:	Z_{cp}/L	.15		.13	

Table 6. Effect of Spin on Normal Force and Moment Terms for
 $\alpha = 10$ Degrees (Rotating Band Off)

MODEL CONFIGURATION:	TERM	$\dot{\alpha} = 0$ ($\dot{\beta} = 0$)	$\dot{\alpha} = -4900$ RPM ($\dot{\beta} = -.162$)
8 INCH DIAMETER MODEL 3 CALIBER OGIVE 2 CALIBER CYLINDER .5 CAL BOATTAIL REF c.g. AT Z/L = .625	$C_{N_{\alpha}}$ (OGIVE)	1.93	1.94
	$C_{N_{\alpha}}$ (CYLINDER)	.33	.60
	$C_{N_{\alpha}}$ (BOATTAIL)	-.36	-.31
	$C_{N_{\alpha}}$ (TOTAL)	1.90	2.24
MACH .94 $\alpha = 10^{\circ}$ $R_d = 4 \times 10^6$ /FT	$C_{m_{\alpha}}$ (OGIVE)	3.46	3.47
	$C_{m_{\alpha}}$ (CYLINDER)	-.35	-.36
	$C_{m_{\alpha}}$ (BOATTAIL)	-.70	.60
	$C_{m_{\alpha}}$ (TOTAL)	3.82	3.71
TEST CONDITION:	Z_{cp}/L	.27	.33

5.4 Rotating Band Effect.

Details of the rotating band configuration used with the model are contained in Appendix D. Figure 34 compares the longitudinal surface pressure distribution over the non-spinning model at zero angle of attack, both with and without the rotating band. The presence of the rotating band creates larger negative surface pressures in the area of the band and has the effect of moving the low pressure expansion region over the boattail slightly forward. The effect of spin on the pressure distribution over the spinning model with the rotating band at zero angle of attack is illustrated in Figure 35. Spin has the main effect of evening out the pressures on the lands and in the grooves of the rotating band which could be important to theoretical and numerical analyses. The influence of the rotating band on the side force distribution of the spinning model at an angle of attack of 10 degrees is presented in Figure 36. As can be seen, the presence of the rotating band results in significantly larger local Magnus forces in the band area compared to the no band case. On the boattail, the effect of the rotating band reduces the peak local Magnus force, as well as the area over which it acts, relative to the no rotating band condition. The relatively large effects of the band on the cylinder and boattail are essentially self-compensating and result in very little difference in the total Magnus force and moment coefficients between the rotating band on and off cases, as shown in Table 7.

The normal force distribution due to spin for the projectile with rotating band at a 10 degree angle of attack is shown in Figure 37. The effect of the rotating band on the normal force and moment terms is contained in Table 8. For the projectile having the rotating band, the influence of spin is to reduce the local normal force over both the cylinder and the boattail compared to the non-spinning case. The net result is that the spinning projectile possesses a greatly reduced normal force and a slightly lower pitching moment than when not spinning.

5.5 Base Pressure.

Data obtained from pressure tap 20, located on the rear facing surface of the projectile model base, are summarized in Figure 38. At an angle of attack of 0 degrees, the base pressure is very small, and, in fact, is positive for the spinning case. The pressure becomes more negative with increasing angle of attack. No definite trend is evident with spin and angle of attack.

5.6 Comparison of Surface Pressure Test Results With Other Data Sources.

The data from the surface pressure wind tunnel test can be compared with data from other experimental and theoretical sources in order to validate and assess the results. First, the non-spinning pressure distribution from this test can be directly compared with similar data obtained on a model configuration and size in the Langley 16-Foot Transonic Wind Tunnel.⁷ Because of the non-spinning condition, only the normal force and moment terms are available and are shown for angles of attack of 4 and 10 degrees in Tables 9 and 10, respectively. Although both projectile models had identical ogive and cylindrical sections, the Langley test model included a 1-caliber boattail; whereas the Ames test model we used had a 0.5-caliber boattail. This difference is evident in the force and moment terms for the boattail and the subsequently larger coefficient derivative for the unstable pitching moment of the larger boattail.

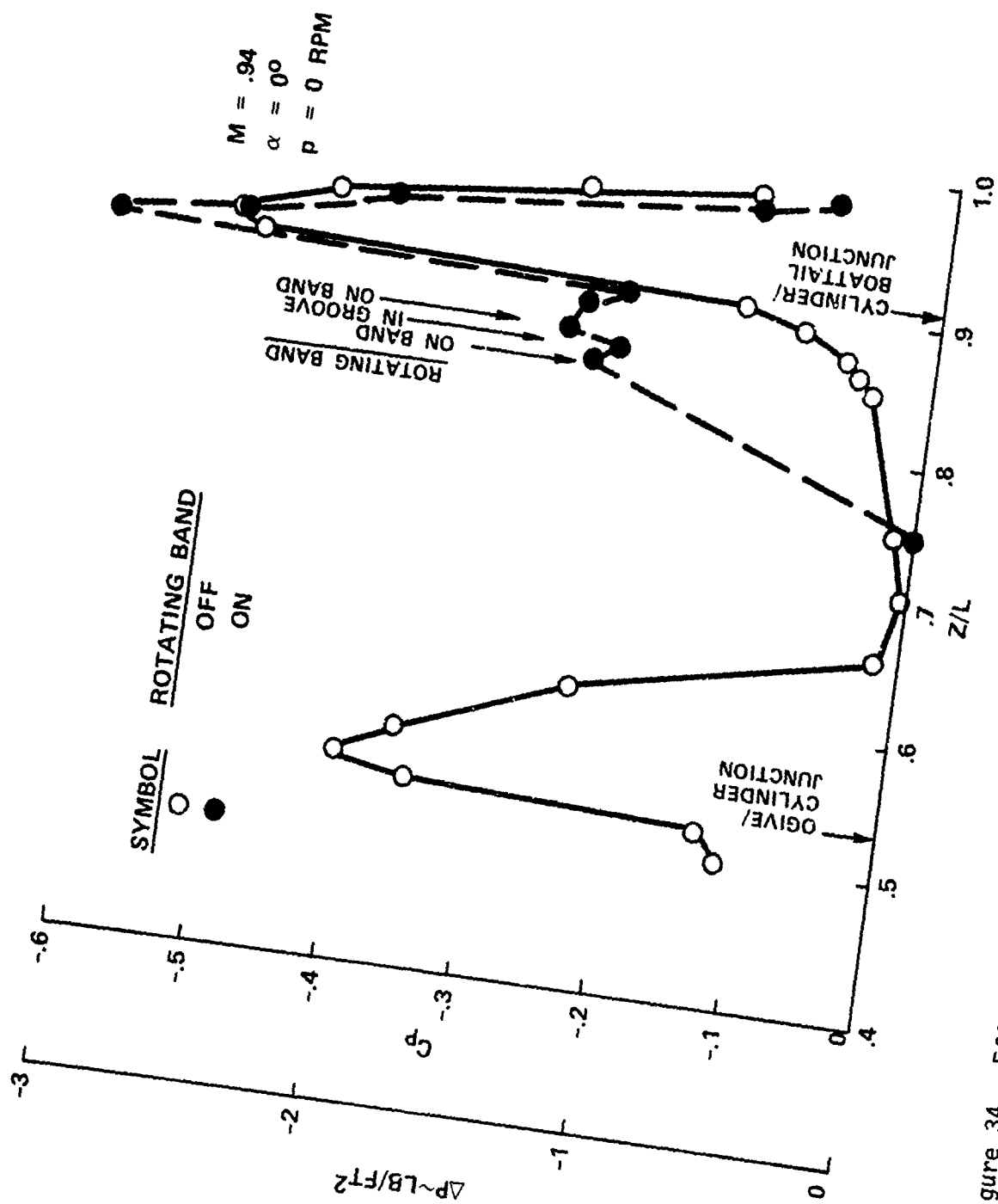


Figure 34. Effect of Rotating Band on Longitudinal Pressure Distribution ($\alpha = 0$ Degree)

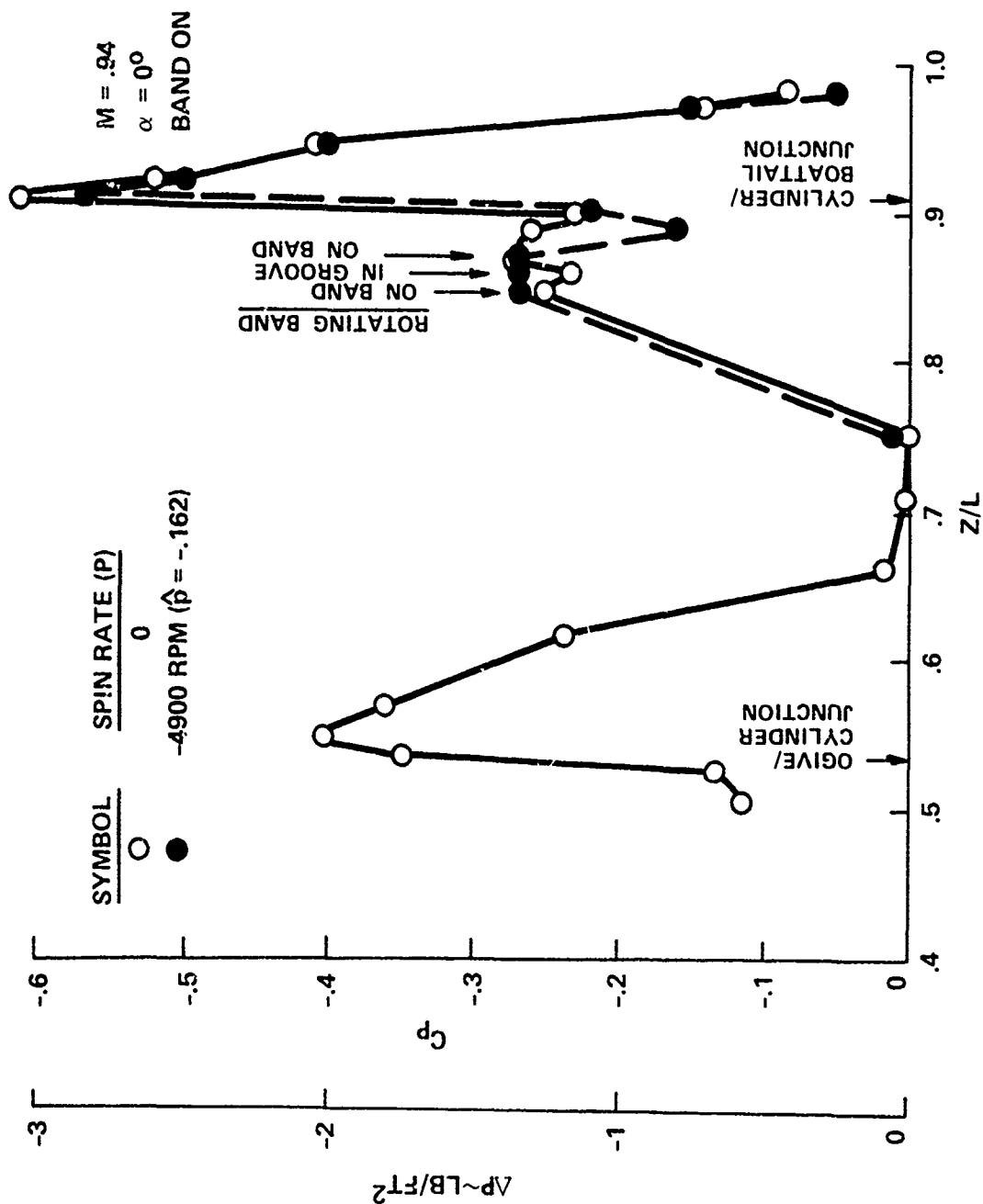


Figure 35. Effect of Spin on Longitudinal Pressure Distribution Over Model With rotating Band ($\alpha = 0$ Degrees)

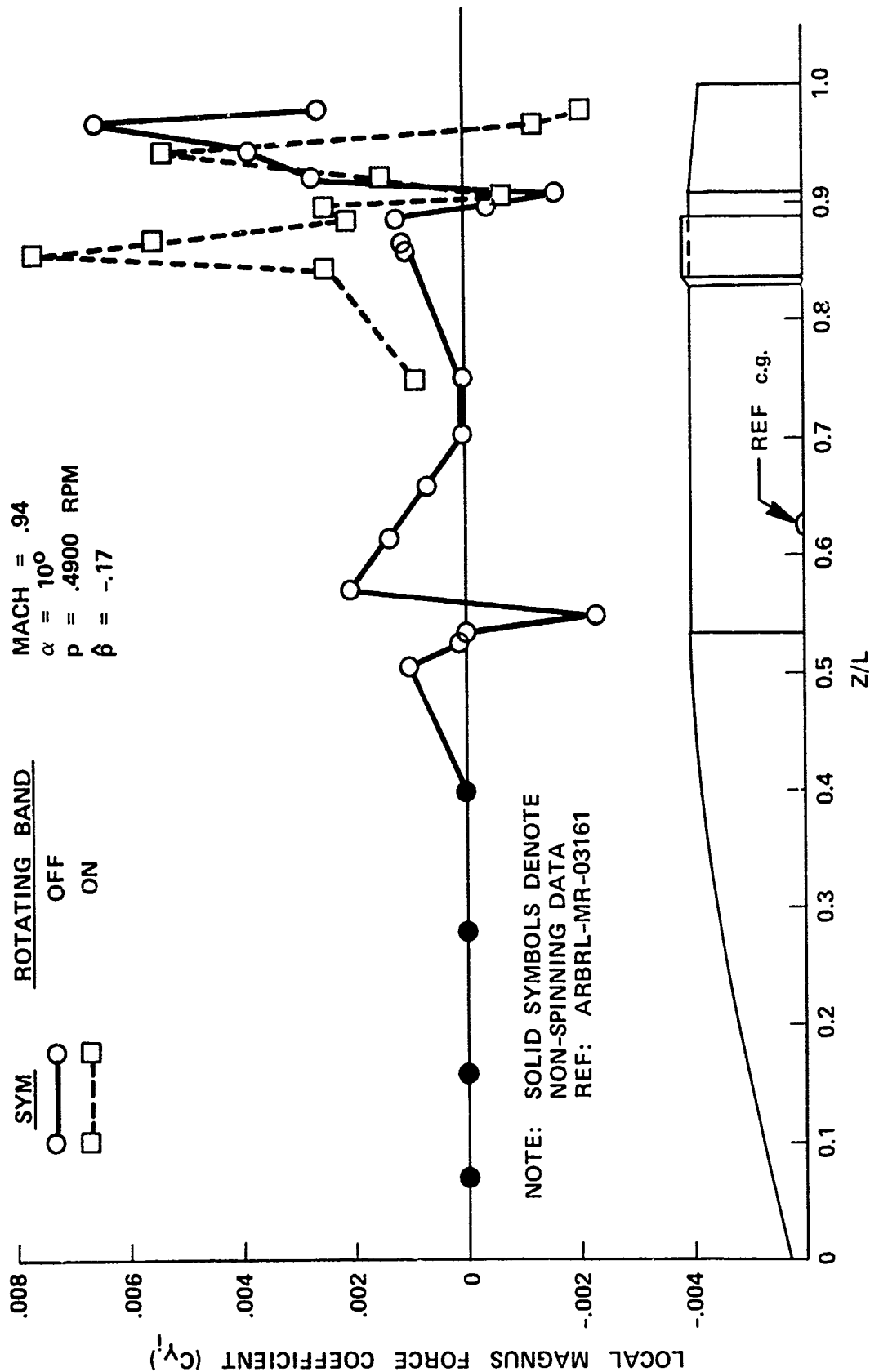


Figure 36. Magnus Side force Distribution on Spinning Model With and Without Rotating Band ($\alpha = 10$ Degrees)

Table 7. Effect of Rotating Band on Side Force and Moment Terms
($\alpha = 10$ Degrees)

MODEL CONFIGURATION:	TERM	ROTATING BAND	ROTATING BAND
		OFF	ON
8 INCH DIAMETER MODEL 3 CALIBER OGIVE 2 CALIBER CYLINDER .5 CALIBER BOATTAIL	C_{Y_p} (OGIVE)	-.004	-.004
	C_{Y_p} (CYLINDER)	-.092	-.149
	C_{Y_p} (BOATTAIL)	-.080	-.026
	C_{Y_p} (TOTAL)	-.176	-.179
TEST CONDITIONS: MACH .94 pd/2V = .162	C_{n_p} (OGIVE)	-.003	-.003
	C_{n_p} (CYLINDER)	.063	-.139
	C_{n_p} (BOATTAIL)	.148	.043
	C_{n_p} (TOTAL)	.208	.180
	$Z_{cp/L}$ (MAGNUS)	.836	.804

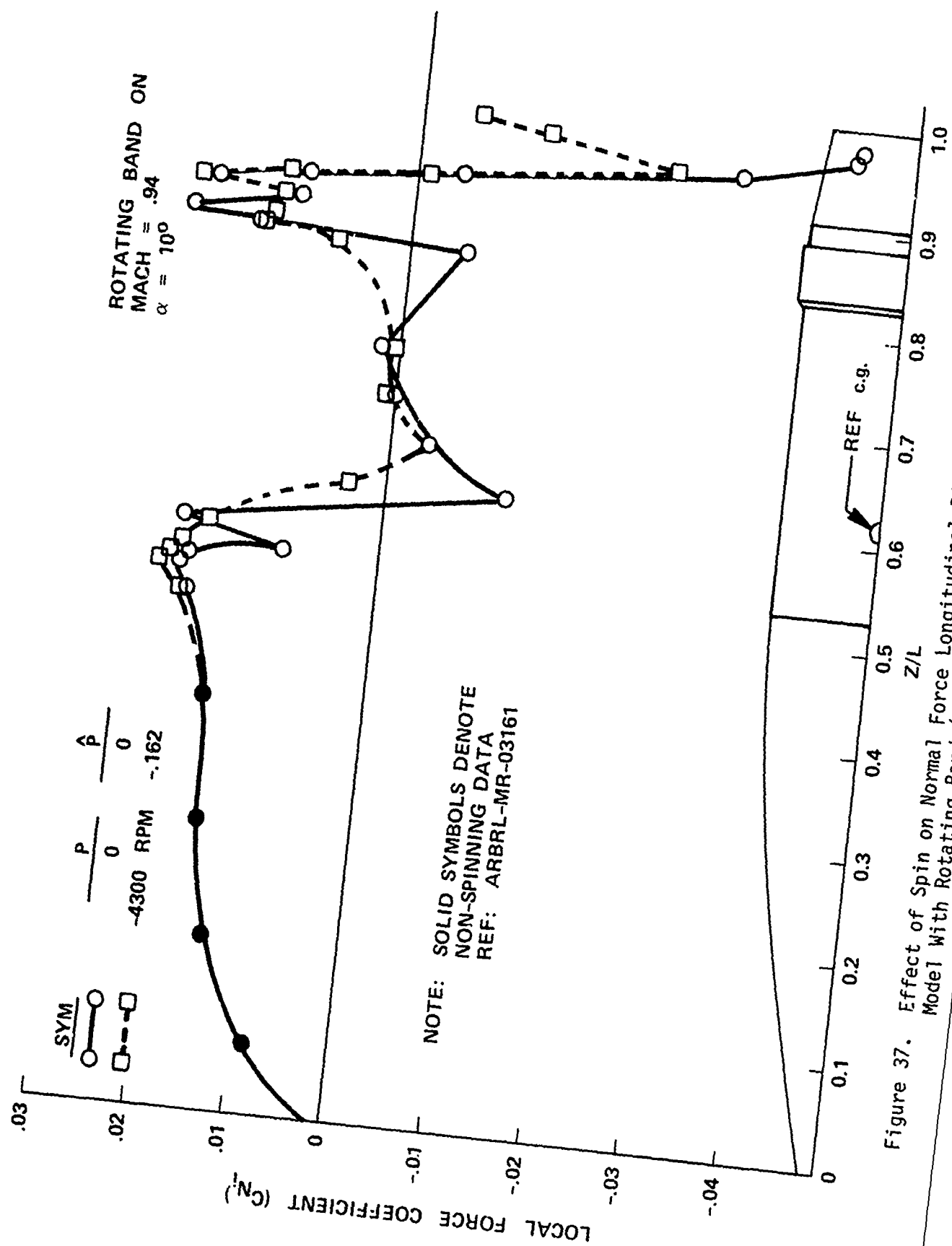


Figure 37. Effect of Spin on Normal Force Longitudinal Distribution Over
 Model With Rotating Band ($\alpha = 10$ Degrees)

Table 8. Effect of Rotating Band on Normal Force and Moment Terms
($\alpha = 10$ Degrees)

MODEL CONFIGURATION:	TERM	ROTATING BAND	
		OFF	ON
8 INCH DIAMETER MODEL 3 CALIBER OGIVE 2 CALIBER CYLINDER .5 CAL BOATTAIL REF c.g. AT Z/L = .625	$C_{N_{\alpha}}$ (OGIVE)	1.94	1.95
	$C_{N_{\alpha}}$ (CYLINDER)	.60	.62
	$C_{N_{\alpha}}$ (BOATTAIL)	-.31	-.25
	$C_{N_{\alpha}}$ (TOTAL)	2.24	2.32
TEST CONDITION: MACH .94 $\alpha = 10^{\circ}$ $R_d = 4 \times 10^6$ /FT $p = -4900$ RPM $\hat{p} = -.162$	$C_{m_{\alpha}}$ (OGIVE)	3.47	3.47
	$C_{m_{\alpha}}$ (CYLINDER)	-.36	-.39
	$C_{m_{\alpha}}$ (BOATTAIL)	.60	.46
	$C_{m_{\alpha}}$ (TOTAL)	3.71	3.54
	Z_{cp}/L	.33	.35

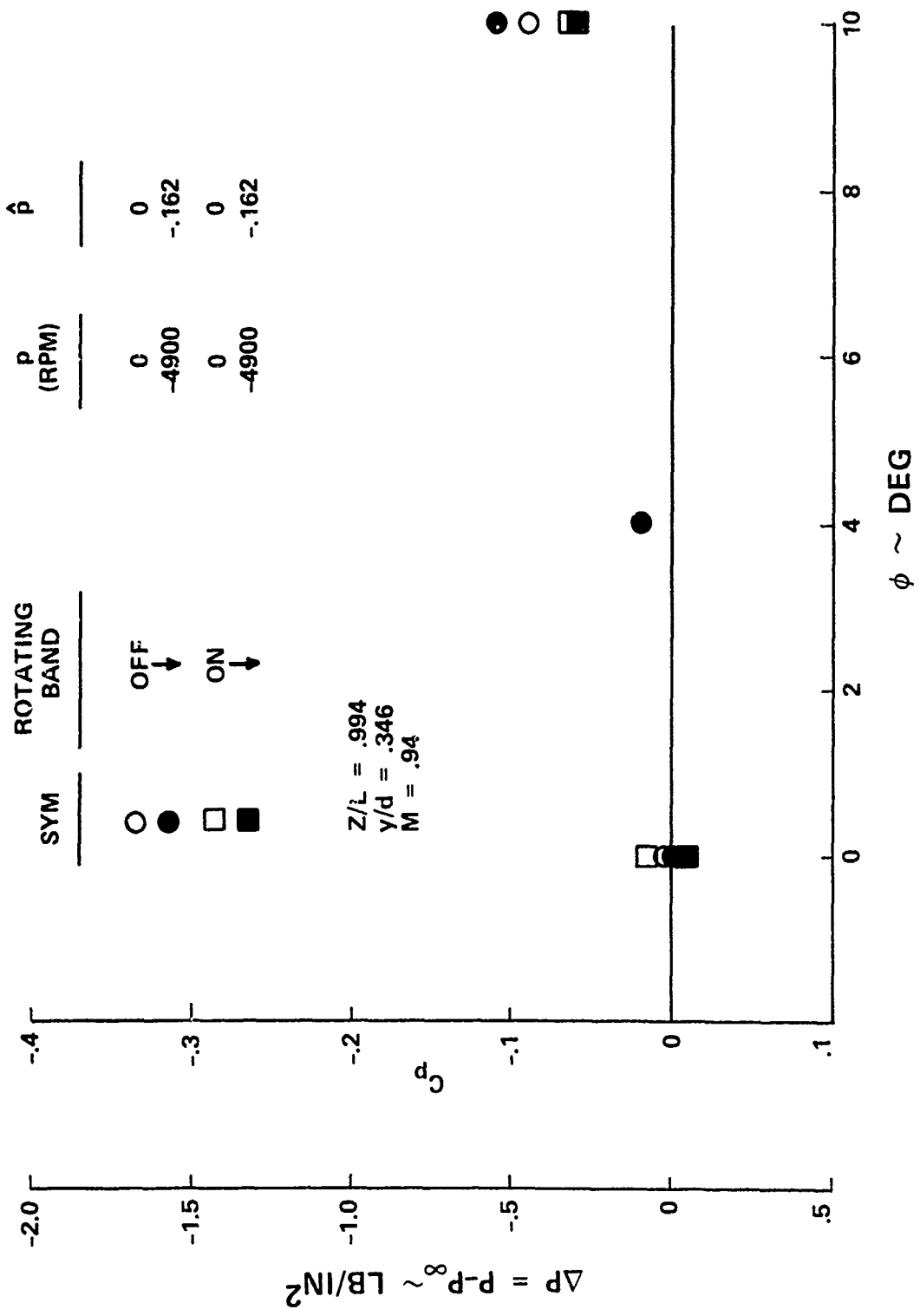


Figure 38. Effect of Angle of Attack and Spin on Model 1 Base Pressure

Table 9. Comparison of Normal Force and Moment Data on Non-Spinning Model from Surface Pressure Test Data ($\alpha = 4$ Degrees)

MODEL CONFIGURATION: 8 INCH DIAMETER MODEL 3 CALIBER OGIVE 2 CALIBER CYLINDER ROTATING BAND OFF (SEE NOTE FOR BOATTAIL) REF c.g. AT Z/L = .625		TERM	PRESSURE MODEL NASA-AMES 14-FT TRANSONIC .5 CAL BOATTAIL	PRESSURE MODEL NASA-LANGLEY 16-FT TRANSONIC 1 CAL BOATTAIL
TEST CONDITION: MACH .94 $\alpha = 4^\circ$ $R_d = 4 \times 10^6/\text{FT}$ $p = 0$ RPM		C_{N_α} (OGIVE)	1.94	2.05
		C_{N_α} (CYLINDER)	.25	.17
		C_{N_α} (BOATTAIL)	-.64	-.60
		C_{N_α} (TOTAL)	1.55	1.62
		C_{m_α} (OGIVE)	3.45	3.57
		C_{m_α} (CYLINDER)	-.50	-.14
		C_{m_α} (BOATTAIL)	1.22	1.07
		C_{m_α} (TOTAL)	4.17	4.50
		Z_{cp}/L	.145	.130

Table 10. Comparison of Normal Force and Moment Data on Non-Spinning Model from Surface Pressure Test Data ($\alpha = 10$ Degrees)

MODEL CONFIGURATION: 8 INCH DIAMETER MODEL 3 CALIBER OGIVE 2 CALIBER CYLINDER (SEE NOTE FOR BOATTAIL) ROTATING BAND OFF REF c.g. AT Z/L = .625		TERM	PRESSURE MODEL NASA-AMES 14-FT TRANSONIC .5 CAL BOATTAIL	PRESSURE MODEL NASA-LANGLEY 16-FT TRANSONIC 1 CAL BOATTAIL
TEST CONDITION: MACH .94 $\alpha = 10^\circ$ $R_d = 4 \times 10^6 / \text{FT}$ $p = 0$ RPM		C_{N_α} (OGIVE)	1.93	2.02
		C_{N_α} (CYLINDER)	.33	.21
		C_{N_α} (BOATTAIL)	-.36	-.67
		C_{N_α} (TOTAL)	1.90	1.56
		C_{m_α} (OGIVE)	3.46	3.55
		C_{m_α} (CYLINDER)	-.35	-.20
		C_{m_α} (BOATTAIL)	.70	1.14
		C_{m_α} (TOTAL)	3.82	4.50
		Z_{cp}/L	.27	.11

An internal balance was employed to directly measure the force and moment acting on a spinning projectile model.² Using this method, only the total force and moment coefficients could be determined. These directly measured terms are compared in Tables 11 and 12 with the same terms obtained by integrating the results of the surface pressure tests. The comparison is excellent, especially for the 10 degree angle-of-attack case where the model configurations both include rotating bands and are most similar.

One of the primary objectives of this test was to obtain experimental data that could be used to evaluate and evolve the Computational Fluid Dynamic (CFD) codes being developed to predict the flow field and resulting aerodynamic effects on spinning projectiles. A CFD code currently under development was used to calculate the aerodynamic terms for a projectile configuration and flight condition identical to that used in the wind tunnel test. The code is based on the solution to the thin-layer Navier-Stokes equations, as described by Nietubicz et al.,⁸ and was run on a CRAY I computer. Table 13 compares the normal force term from the code with that from the surface pressure wind tunnel test and illustrates the excellent agreement achieved. The Magnus terms are compared in Table 14. In this case, the code under predicts the Magnus force by a significant amount.

6. CONCLUSIONS

- The sliding seal technique is capable of accurately measuring the Magnus-induced surface pressures on a spinning projectile wind tunnel model at transonic Mach numbers.
- Check runs showed excellent repeatability and demonstrated the absence of model or instrumentation asymmetries.
- Surface pressure data obtained in this test showed good agreement with the surface pressure data obtained on an identical, non-spinning model at the NASA-Langley 8-Foot Transonic Wind Tunnel.
- Total coefficients for Magnus force and moment computed by integrating the measured surface pressure data showed good agreement with directly measured force and moment data obtained from other spinning models.
- The data indicated the quantitative influence of spin and angle of attack and reveal that, for a given condition, different portions of the projectile can experience both positive and negative local Magnus forces.
- Quantitative pressure data were obtained to indicate the relative contribution of the various projectile elements (i.e., ogive, cylinder, boattail, rotating band) to the Magnus effect.
- A significant negative pressure region was detected on the advancing side of the leeward location at all longitudinal stations for a 10-degree angle of attack. This phenomenon was not noted at a 4-degree angle of attack.
- Base pressures at the test Mach number were found to be near free-stream static values.

Figure 11. Comparison of Side Force and Moment Data on Spinning From Surface Pressure and Direct Force Tests for $\alpha = 4$ Degrees

MODEL CONFIGURATION:		TERM	INTEGRATION OF SURFACE PRESSURE DATA	DIRECT FORCE AND MOMENT DATA, REF: BRLMR22B4
3 CALIBER OGIVE 2 CALIBER CYLINDER .5 CALIBER BOATTAIL ROTATING BAND ON $Z_{cg}/L = .625$		C_{Y_p} (OGIVE)	-.004	-
		C_{Y_p} (CYLINDER)	-.149	-
		C_{Y_p} (BOATTAIL)	-.026	-
		C_{Y_p} (TOTAL)	-.179	-.175
TEST CONDITIONS: MACH .94 $\alpha = 10^\circ$ $p_0/2V = .162$		C_{n_n} (OGIVE)	-.003	-
		C_{n_p} (CYLINDER)	.139	-
		C_{n_p} (BOATTAIL)	.043	-
		C_{n_p} (TOTAL)	.180	.180
		Z_{cp}/L (MAGNUS)	.804	.808

Table 12. Comparison of Side Force and Moment Data on Spinning Model from Surface Pressure and Direct Force Tests for $\alpha = 10$ Degrees

		TERM	*INTEGRATION OF SURFACE PRESSURE DATA	**DIRECT FORCE AND MOMENT DATA, REF: BRLMR22B4
MODEL CONFIGURATION:	3 CALIBER OGIVE	C_{V_p} (OGIVE)	.000	—
	2 CALIBER CYLINDER	C_{Y_p} (CYLINDER)	-.085	—
	.5 CALIBER BOATTAIL	C_{Y_p} (BOATTAIL)	-.019	—
	* ROTATING BAND OFF	C_{Y_p} (TOTAL)	-.104	-.090
	** ROTATING BAND ON			
TEST CONDITIONS:	$Z_{cg}/L = .625$			
	MACH .94			
	$\alpha = 10^\circ$			
	$pd/2V = .162$			
		C_{n_p} (OGIVE)	.000	—
		C_{n_p} (CYLINDER)	.056	—
		C_{n_p} (BOATTAIL)	.033	—
		C_{n_p} (TOTAL)	.090	.085
		Z_{cp}/L (MAGNUS)	.779	.793

Table 13. Comparison of Normal Force and Moment Terms From Surface Pressure Test Data and Computational Fluid Dynamic Code

MODEL CONFIGURATION:	TERM	INTEGRATION OF SURFACE PRESSURE WIND TUNNEL TEST DATA	COMPUTATIONAL FLUID DYNAMIC CODE
MODEL CONFIGURATION:	8 INCH DIAMETER MODEL		
	3 CALIBER OGIVE	$C_{N_{\alpha}}$ (OGIVE)	1.96
	2 CALIBER CYLINDER	$C_{N_{\alpha}}$ (CYLINDER)	.30
	.5 CALIBER BOATTAIL	$C_{N_{\alpha}}$ (BOATTAIL)	-.68
	ROTATING BAND OFF	$C_{N_{\alpha}}$ (TOTAL)	1.59
TEST CONDITIONS:	REF c.g. AT Z/L = .625		1.58
	MACH .94		
	$\alpha = 4^{\circ}$		
	$R_d = 4 \times 10^6 / \text{FT}$		
	$pd/2V = .162$		
	$C_{m_{\alpha}}$ (OGIVE)		3.47
	$C_{m_{\alpha}}$ (CYLINDER)		-.36
	$C_{m_{\alpha}}$ (BOATTAIL)		1.30
	$C_{m_{\alpha}}$ (TOTAL)		4.41
	Z_{cp}/L		.13

Table 14. Comparison of Side Force and Moment Terms from Surface Pressure
Test Data and Computational Fluid Dynamic Code

MODEL CONFIGURATION:	TERM:	INTEGRATION OF SURFACE PRESSURE WIND TUNNEL TEST DATA	COMPUTATIONAL FLUID DYNAMIC CODE
MODEL CONFIGURATION: 8 INCH DIAMETER MODEL 3 CALIBER OGIVE 2 CALIBER CYLINDER .5 CALIBER BOATTAIL ROTATING BAND OFF $Z_{cg}/L = .625$	C_{Y_p} (OGIVE)	.000	
	C_{Y_p} (CYLINDER)	-.085	
	C_{Y_p} (BOATTAIL)	-.019	
	C_{Y_p} (TOTAL)	-.104	-.015
TEST CONDITIONS: $MACH .94$ $\alpha = 4^\circ$ $R_d = 4 \times 10^6 / FT$ $pd/2V = .162$	C_{n_p} (OGIVE)	.000	
	C_{n_p} (CYLINDER)	.056	
	C_{n_p} (BOATTAIL)	.033	
	C_{n_p} (TOTAL)	.090	
	Z_{cp}/L (MAGNUS)	.78	

- The presence of the rotating band influenced the Magnus effects both upstream and downstream of the band, but in a compensating manner resulting in very little difference in the total Magnus effect between the band-off and band-on cases.
- Model components and instrumentation functioned well; however, pressure settling times of about 60 seconds were experienced. Future tests should employ shorter lengths of pressure tubing to decrease the data acquisition time.

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GLOSSARY

C_N	normal force coefficient N/qS
C_{N_i}	local normal force coefficient, $\frac{360/\Delta\phi}{\sum_{j=1}^2} C_{p_j} \frac{d_i \Delta z_i \sin\Delta\phi \cos\phi_j}{\pi d^2}$
C_{N_α}	$\partial C_N / \partial \alpha$
C_m	pitching moment coefficient, PM/qsd
C_{m_α}	$\partial C_m / \partial \alpha$
C_n	yawing moment coefficient, YM/qsd
C_{n_p}	$\partial C_n / \partial \hat{p}$
C_p	pressure coefficient, $(P - P_\infty)/q$
C_y	side force coefficient
C_{y_i}	local side force coefficient, $\frac{360/\Delta\phi}{\sum_{j=1}^2} C_{p_j} \frac{d_i \Delta z_i \sin\Delta\phi \sin\phi_j}{\pi d^2}$
C_{y_p}	$\partial C_y / \partial \hat{p}$
d	model reference diameter (7.95 inches)
i	subscript denotes value at location Z_i
j	subscript denotes value at location ϕ_j
L	projectile length (44.616 inches)
M	Mach number
N	normal force

P	surface pressure
P_{∞}	free stream static pressure
PM	pitching moment
p	spin rate
\hat{p}	tip speed ratio, $pd/2V$
q	dynamic pressure, $\rho v^2/2$
R_d	Reynolds number, v/ν
S	reference area, $\pi d^2/4$
SF	side force
SIGMA N	angle between the projectile center line and the sun direction
T_{∞}	free stream temperature
t	time
V	total free stream velocity
x, y, z	body axes
YM	yawing moment
Z	distance along model measured from nose
Z_{cg}	longitudinal location of reference center of gravity from nose
Z_{cp}/L	normal force center-of-pressure location from nose, $.625 - .1782(C_{m_{\alpha}}/C_{N_{\alpha}})$
Z_{cp}/L (Magnus)	Magnus force center-of-pressure location from nose, $.625 + .1782(C_{n_p}/C_{Y_p})$
α	angle of attack
ΔP	$P - P_{\infty}$
$\Delta\phi$	increment between circumferential locations
ν	air kinematic viscosity
π	ratio of circle circumference to diameter

ρ	air density
ϕ_j	circumferential location
θ	angle of projectile surface to projectile centerline

APPENDIX A

TABULATED WIND TUNNEL TEST DATA

This appendix presents the measured pressure data in tabulated format. Each set of data relates to a specific model configuration and test condition: rotating band on or rotating band off, angle of attack of 0, 4, or 10 degrees, and spinning or non-spinning. The resulting pressure coefficients are presented as a function of azimuthal location (ϕ) for each longitudinal tap location (Z/L).

Data for the ogive area obtained during the Langley non-spinning test are also included to provide the total pressure distribution. The appendix figures contain the following data:

Figure	Rotating band	Angle of attack (deg)	Spin rate (rpm)	Run no.
A1	OFF	0	0	7-11, 12-25
A2	OFF	0	4900	73-92
A3	OFF	4	0	30-49
A4	OFF	4	4900	98-112
A5	OFF	10	0	113-122, 127-135
A6	OFF	10	4900	50-69
A7	ON	0	0	144-154
A8	ON	0	4900	181-192
A9	ON	10	0	157-168
A10	ON	10	4900	169-180

Appendix A

DATA SOURCE : LANGLEY

TAP LOCATION (Z/L): 0.07
TAP LOCATION (Z/D): 0.393

0.16
0.998
0.29
1.571
0.4
2.245
0.5
2.806

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.000	0.000	0.000	0.000	0.000	0.000
22.5	0.000	0.000	0.000	0.000	0.000	0.000
45.0	0.000	0.000	0.000	0.000	0.000	0.000
67.5	0.000	0.000	0.000	0.000	0.000	0.000
90.0	0.000	0.000	0.000	0.000	0.000	0.000
112.5	0.000	0.000	0.000	0.000	0.000	0.000
135.0	0.000	0.000	0.000	0.000	0.000	0.000
157.5	0.000	0.000	0.000	0.000	0.000	0.000
180.0	0.000	0.000	0.000	0.000	0.000	0.000
202.5	0.000	0.000	0.000	0.000	0.000	0.000
225.0	0.000	0.000	0.000	0.000	0.000	0.000
247.5	0.000	0.000	0.000	0.000	0.000	0.000
270.0	0.000	0.000	0.000	0.000	0.000	0.000
292.5	0.000	0.000	0.000	0.000	0.000	0.000
315.0	0.000	0.000	0.000	0.000	0.000	0.000
337.5	0.000	0.000	0.000	0.000	0.000	0.000

REF. LENGTH (L): 44.616 IN.
REF. DIAMETER (D): 4.95 IN.
ROTARY SPEED (RPM): 0.94
XINCH NO.: 0
ANGLE OF ATTACK (ALPHA): 0 DEG.
SPIN RATE (PSI): 0
TIP SPEED RATIO (PD/2V): 0
X CG-L: 0.625112067

DATA SOURCE : AMES

TAP LOCATION (Z/L): 0.583
TAP LOCATION (Z/D): 2.824

0.526
2.93
0.537
3.014
0.548
3.077
0.571
3.283
0.615
3.454
0.66
3.706
0.705
3.957

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
10.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
20.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
30.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
40.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
50.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
60.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
70.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
80.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
90.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
100.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
110.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
120.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
130.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
140.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
150.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
160.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
170.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
180.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
190.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
200.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
210.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
220.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
230.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
240.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
250.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
260.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
270.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
280.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
290.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
300.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
310.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
320.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
330.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
340.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006
350.0	-0.116	-0.133	-0.352	-0.488	-0.363	-0.240	-0.019	-0.006	-0.006

DATA SOURCE : - LANGLEY

TMP LOCATION (Z/L): 0.97
TMP LOCATION (Z/B): 0.393

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.114	0.027	-0.044	-0.186	-0.484
22.5	0.000	0.000	0.000	0.000	0.000
45.0	0.000	0.000	0.000	0.000	0.000
67.5	0.000	0.000	0.000	0.000	0.000
90.0	0.123	0.035	-0.037	-0.160	-0.442
112.5	0.000	0.000	0.000	0.000	0.000
135.0	0.000	0.000	0.000	0.000	0.000
157.5	0.000	0.000	0.000	0.000	0.000
180.0	0.122	0.033	-0.039	-0.161	-0.445
202.5	0.000	0.000	0.000	0.000	0.000
225.0	0.000	0.000	0.000	0.000	0.000
247.5	0.122	0.033	-0.037	-0.160	-0.445
270.0	0.000	0.000	0.000	0.000	0.000
292.5	0.000	0.000	0.000	0.000	0.000
315.0	0.000	0.000	0.000	0.000	0.000
337.5	0.000	0.000	0.000	0.000	0.000

REF. LENGTH (L): 44.616 IN.
REF. DIMETER (D): 7.95 IN.
ROTATING BORE: OFF
MACHINE NO.: 0-94 DEG.
WHEEL NO.: 4900 REV/MIN
SPIN RATE (RPM): 0.152027427
TIP SPEED RATIO (PS/2V): 0.625112667
X CC/L

DATA SOURCE : RMES

TMP LOCATION (Z/L): 0.593
TMP LOCATION (Z/B): 2.824

CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	-0.127	-0.148	-0.361	-0.420	-0.366	-0.274	-0.834
18.0	-0.127	-0.148	-0.361	-0.420	-0.366	-0.273	-0.832
36.0	-0.127	-0.148	-0.361	-0.420	-0.369	-0.271	-0.831
54.0	-0.127	-0.148	-0.361	-0.420	-0.370	-0.269	-0.830
72.0	-0.127	-0.148	-0.361	-0.420	-0.370	-0.268	-0.829
90.0	-0.127	-0.148	-0.361	-0.417	-0.370	-0.266	-0.827
108.0	-0.127	-0.148	-0.361	-0.415	-0.370	-0.265	-0.825
126.0	-0.128	-0.148	-0.360	-0.414	-0.370	-0.263	-0.825
144.0	-0.128	-0.148	-0.360	-0.413	-0.370	-0.262	-0.826
162.0	-0.128	-0.148	-0.360	-0.413	-0.370	-0.261	-0.827
180.0	-0.129	-0.148	-0.360	-0.414	-0.371	-0.260	-0.827
198.0	-0.129	-0.148	-0.360	-0.415	-0.371	-0.259	-0.827
216.0	-0.129	-0.148	-0.360	-0.417	-0.371	-0.258	-0.827
234.0	-0.133	-0.148	-0.364	-0.418	-0.372	-0.256	-0.828
252.0	-0.135	-0.148	-0.362	-0.420	-0.372	-0.255	-0.828
270.0	-0.135	-0.148	-0.362	-0.420	-0.371	-0.253	-0.829
288.0	-0.134	-0.148	-0.362	-0.420	-0.371	-0.252	-0.830
306.0	-0.134	-0.148	-0.362	-0.420	-0.370	-0.251	-0.830
324.0	-0.132	-0.148	-0.361	-0.420	-0.369	-0.251	-0.831
342.0	-0.131	-0.148	-0.361	-0.420	-0.368	-0.250	-0.832
360.0	-0.129	-0.148	-0.361	-0.420	-0.367	-0.249	-0.833
378.0	-0.128	-0.148	-0.361	-0.420	-0.367	-0.248	-0.834
396.0	-0.128	-0.148	-0.361	-0.420	-0.366	-0.246	-0.834
414.0	-0.127	-0.148	-0.361	-0.420	-0.366	-0.245	-0.835
432.0	-0.127	-0.148	-0.361	-0.420	-0.366	-0.245	-0.834
450.0	-0.127	-0.148	-0.361	-0.420	-0.366	-0.244	-0.834

Figure A-2. Rotating Band Off, $\alpha = 0^\circ$, $P = 4900$ rpm

DATA SOURCE : LANGLEY

TAP LOCATION (Z/L): 0.07		0.76		0.20		0.4		0.5	
TAP LOCATION (Z/D): 0.393		0.896		1.571		2.245		2.806	
CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.111	0.079	0.091	0.068	0.068	0.068	0.068	0.068	0.068
22.5	0.118	0.075	0.082	0.064	0.064	0.064	0.064	0.064	0.064
45.0	0.125	0.069	0.076	0.058	0.058	0.058	0.058	0.058	0.058
67.5	0.132	0.060	0.067	0.050	0.050	0.050	0.050	0.050	0.050
90.0	0.110	0.042	0.042	0.033	0.033	0.033	0.033	0.033	0.033
112.5	0.092	0.021	0.021	0.013	0.013	0.013	0.013	0.013	0.013
135.0	0.073	0.004	0.004	0.004	0.004	0.004	0.004	0.004	0.004
157.5	0.073	-0.004	-0.004	-0.004	-0.004	-0.004	-0.004	-0.004	-0.004
180.0	0.073	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009
202.5	0.073	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009
225.0	0.073	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009
247.5	0.073	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009	-0.009
270.0	0.110	0.021	0.021	0.013	0.013	0.013	0.013	0.013	0.013
292.5	0.132	0.060	0.067	0.050	0.050	0.050	0.050	0.050	0.050
315.0	0.152	0.060	0.067	0.050	0.050	0.050	0.050	0.050	0.050
337.5	0.163	0.075	0.082	0.064	0.064	0.064	0.064	0.064	0.064

REF. LENGTH (L): 44.616 IN.
 REF. DIAMETER (D): 7.95 IN.
 ROTATING BAND: 0.94
 MACH NO.: 4
 ANGLE OF ATTACK (ALPHA): 0 DEG.
 SPIN RATE (P): 0 REV/MIN
 TIP SPEED RATIO (PD/2V): 0.625112667
 X CCL

DATA SOURCE : AMES

TAP LOCATION (Z/L): 0.503		0.526		0.537		0.548		0.571	
TAP LOCATION (Z/D): 2.824		2.93		3.014		3.077		3.203	
CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.079	0.088	0.080	0.080	0.080	0.080	0.080	0.080	0.080
10.0	0.094	0.092	0.085	0.085	0.085	0.085	0.085	0.085	0.085
20.0	0.097	0.089	0.088	0.088	0.088	0.088	0.088	0.088	0.088
30.0	0.103	0.099	0.098	0.098	0.098	0.098	0.098	0.098	0.098
40.0	0.110	0.102	0.102	0.102	0.102	0.102	0.102	0.102	0.102
50.0	0.118	0.105	0.105	0.105	0.105	0.105	0.105	0.105	0.105
60.0	0.125	0.111	0.111	0.111	0.111	0.111	0.111	0.111	0.111
70.0	0.130	0.119	0.119	0.119	0.119	0.119	0.119	0.119	0.119
80.0	0.135	0.124	0.124	0.124	0.124	0.124	0.124	0.124	0.124
90.0	0.141	0.130	0.130	0.130	0.130	0.130	0.130	0.130	0.130
100.0	0.142	0.140	0.140	0.140	0.140	0.140	0.140	0.140	0.140
110.0	0.145	0.149	0.149	0.149	0.149	0.149	0.149	0.149	0.149
120.0	0.145	0.153	0.153	0.153	0.153	0.153	0.153	0.153	0.153
130.0	0.145	0.156	0.156	0.156	0.156	0.156	0.156	0.156	0.156
140.0	0.145	0.160	0.160	0.160	0.160	0.160	0.160	0.160	0.160
150.0	0.144	0.162	0.162	0.162	0.162	0.162	0.162	0.162	0.162
160.0	0.144	0.164	0.164	0.164	0.164	0.164	0.164	0.164	0.164
170.0	0.144	0.165	0.165	0.165	0.165	0.165	0.165	0.165	0.165
180.0	0.145	0.164	0.164	0.164	0.164	0.164	0.164	0.164	0.164
190.0	0.145	0.163	0.163	0.163	0.163	0.163	0.163	0.163	0.163
200.0	0.145	0.164	0.164	0.164	0.164	0.164	0.164	0.164	0.164
210.0	0.145	0.164	0.164	0.164	0.164	0.164	0.164	0.164	0.164
220.0	0.145	0.163	0.163	0.163	0.163	0.163	0.163	0.163	0.163
230.0	0.145	0.162	0.162	0.162	0.162	0.162	0.162	0.162	0.162
240.0	0.145	0.161	0.161	0.161	0.161	0.161	0.161	0.161	0.161
250.0	0.144	0.160	0.160	0.160	0.160	0.160	0.160	0.160	0.160
260.0	0.141	0.156	0.156	0.156	0.156	0.156	0.156	0.156	0.156
270.0	0.135	0.151	0.151	0.151	0.151	0.151	0.151	0.151	0.151
280.0	0.131	0.146	0.146	0.146	0.146	0.146	0.146	0.146	0.146
290.0	0.125	0.139	0.139	0.139	0.139	0.139	0.139	0.139	0.139
300.0	0.118	0.132	0.132	0.132	0.132	0.132	0.132	0.132	0.132
310.0	0.110	0.122	0.122	0.122	0.122	0.122	0.122	0.122	0.122
320.0	0.109	0.116	0.116	0.116	0.116	0.116	0.116	0.116	0.116
330.0	0.097	0.109	0.109	0.109	0.109	0.109	0.109	0.109	0.109
340.0	0.097	0.103	0.103	0.103	0.103	0.103	0.103	0.103	0.103
350.0	0.091	0.098	0.098	0.098	0.098	0.098	0.098	0.098	0.098
360.0	0.085	0.092	0.092	0.092	0.092	0.092	0.092	0.092	0.092

Figure A-3. Rotating Band Off, $\alpha = 4^\circ$, $P = 0$ rpm

[illegible]

Figure A-3. (Cont'd)

TRAP LOCATION (Z/L/D):	0-07
TRAP LOCATION (Z/L/D):	0-393
CIRCUMFERENTIAL	
ANGLE (DEG):	
0	
22.5	0.171
45.0	0.168
67.5	0.152
90.0	0.132
112.5	0.102
135.0	0.079
157.5	0.073
180.0	0.071
202.5	0.073
225.0	0.069
247.5	0.116
270.0	0.132
292.5	0.152
315.0	0.168
337.5	
360.0	

REF. LENGTH (L):	44.616	IN.
REF. DIAMETER (D):	7.95	IN.
ROTATING BAND:	OFF	
MACH NO.:	0.94	DEG.
ANGLE OF ATTACK (ALPHA):	4	DEG.
SPIN RATE (P):	4900	REV/MIN
TIP SPEED RATIO (PD/2V):	0.162027427	
X CG/L	0.625112067	

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TAP LOCATION (Z/D): 0.533
TAP LOCATION (Z/D): 2.324

CIRCUMFERENTIAL
ANGLE (PHI)
*****
PRESSURE
COEFFICIENT (CP)
*****
-0.104
-0.107
-0.110
-0.113
-0.124
-0.131
-0.142
-0.149
-0.156
-0.164
-0.168
-0.163
-0.162
-0.163
-0.161
-0.166
-0.168
-0.165
-0.162
-0.164
-0.160
-0.156
-0.153
-0.146
-0.138
-0.133
-0.125
-0.114
-0.101
-0.106
-0.106

```

0.548	0.571	0.615	0.656
3.877	3.283	3.454	3.766
PRESSURE	PRESSURE	PRESSURE	PRESSURE
COEFFICIENT (CP)	COEFFICIENT (CP)	COEFFICIENT (CP)	COEFFICIENT (CP)
*****	*****	*****	*****
-0.389	-0.336	-0.247	-0.047
-0.389	-0.334	-0.248	-0.047
-0.389	-0.341	-0.249	-0.051
-0.392	-0.341	-0.252	-0.051
-0.398	-0.346	-0.264	-0.054
-0.402	-0.352	-0.266	-0.052
-0.405	-0.357	-0.275	-0.055
-0.412	-0.371	-0.276	-0.056
-0.417	-0.378	-0.274	-0.059
-0.421	-0.391	-0.273	-0.059
-0.421	-0.397	-0.264	-0.045
-0.425	-0.394	-0.246	-0.041
-0.428	-0.395	-0.248	-0.037
-0.427	-0.394	-0.242	-0.036
-0.422	-0.389	-0.233	-0.035
-0.424	-0.377	-0.232	-0.033
-0.418	-0.373	-0.232	-0.029
-0.416	-0.379	-0.219	-0.031
-0.413	-0.367	-0.224	-0.034
-0.417	-0.371	-0.238	-0.035
-0.427	-0.376	-0.259	-0.034
-0.432	-0.378	-0.269	-0.036
-0.432	-0.383	-0.279	-0.040
-0.436	-0.386	-0.280	-0.044
-0.437	-0.389	-0.286	-0.046
-0.435	-0.379	-0.284	-0.048
-0.431	-0.374	-0.285	-0.054
-0.425	-0.372	-0.278	-0.052
-0.421	-0.361	-0.274	-0.051
-0.419	-0.358	-0.267	-0.053
-0.408	-0.354	-0.264	-0.048
-0.405	-0.344	-0.258	-0.055
-0.366	-0.340	-0.252	-0.051
-0.389	-0.340	-0.246	

TAP LOCATION (Z/L): 0.765 TAP LOCATION (Z/D): 3.957		0.75 4.289		0.948 4.737		0.859 4.82		0.87 4.883		0.888 4.963		PRESSURE COEFFICIENT (CP) *****	
CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	-0.019	-0.032	-0.046	-0.059	-0.062	-0.064	-0.065	-0.065	-0.065	-0.065	-0.065	-0.065	-0.065
10.0	-0.012	-0.031	-0.046	-0.059	-0.062	-0.064	-0.065	-0.065	-0.065	-0.065	-0.065	-0.065	-0.065
20.0	-0.017	-0.035	-0.050	-0.062	-0.065	-0.067	-0.068	-0.068	-0.068	-0.068	-0.068	-0.068	-0.068
30.0	-0.022	-0.039	-0.054	-0.066	-0.069	-0.071	-0.072	-0.072	-0.072	-0.072	-0.072	-0.072	-0.072
40.0	-0.024	-0.040	-0.055	-0.067	-0.070	-0.072	-0.073	-0.073	-0.073	-0.073	-0.073	-0.073	-0.073
50.0	-0.027	-0.045	-0.060	-0.072	-0.075	-0.077	-0.078	-0.078	-0.078	-0.078	-0.078	-0.078	-0.078
60.0	-0.029	-0.046	-0.062	-0.073	-0.076	-0.078	-0.079	-0.079	-0.079	-0.079	-0.079	-0.079	-0.079
70.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
80.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
90.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
100.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
110.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
120.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
130.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
140.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
150.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
160.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
170.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
180.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
190.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
200.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
210.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
220.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
230.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
240.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
250.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
260.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
270.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
280.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
290.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
300.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
310.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
320.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
330.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
340.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082
350.0	-0.031	-0.048	-0.064	-0.075	-0.078	-0.080	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081	-0.081
360.0	-0.032	-0.049	-0.065	-0.076	-0.079	-0.081	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082	-0.082

REF. LENGTH (L): 44.516 IN.
REF. DIAMETER (D): 7.95 IN.
ROTATING BAND: 0.94 DEG
MACH NO.: 4.900
ANGLE OF ATTACK (ALPHA): 0.52027427
SPIN RATE (P): 0.625112067
TIP SPEED RATIO (PD/2V):
X CG/L

Figure A-4. (Cont'd)

DATA SOURCE : LANGLEY

TAP LOCATION (Z/L):	0.07	0.16	0.28	0.4	0.5	
TAP LOCATION (Z/D):	0.393	0.898	1.571	2.245	2.886	
CIRCUMFERENTIAL ANGLE (PHI)						
*****	*****	*****	*****	*****	*****	*****
0.0	0.272	0.172	0.083	0.008	-0.322	
22.5	0.249	0.149	0.061	-0.020	-0.339	
45.0	0.185	0.087	0.002	-0.075	-0.383	
67.5	0.103	-0.088	-0.071	-0.142	-0.445	
90.0	0.035	-0.056	-0.125	-0.187	-0.468	
112.5	-0.080	-0.084	-0.136	-0.199	-0.486	
135.0	-0.083	-0.091	-0.138	-0.184	-0.471	
157.5	0.065	-0.092	-0.118	-0.154	-0.446	
180.0	0.086	-0.072	-0.098	-0.132	-0.447	
202.5	0.086	-0.081	-0.118	-0.164	-0.476	
225.0	-0.003	-0.084	-0.138	-0.184	-0.476	
247.5	0.000	-0.084	-0.136	-0.199	-0.484	
270.0	0.035	-0.056	-0.125	-0.199	-0.445	
292.5	0.103	0.088	-0.071	-0.154	-0.445	
315.0	0.185	0.087	0.002	-0.075	-0.383	
337.5	0.249	0.149	0.061	-0.020	-0.339	

REF. LENGTH (L): 4-.616 IN.
 REF. DIAMETER (D): 7.95 IN.
 ROTATING BAND: OFF
 MACH NO.: 0.94
 ANGLE OF ATTACK (ALPHA): 10 DEG.
 SPIN RATE (P): 0 REV/MIN
 TAP SPEED RATIO (PD/2V): 0
 X CG/L 0.625112067

DATA SOURCE : AMES

TAP LOCATION (Z/L):	0.503	0.526	0.537	0.548	0.615	0.66	0.705
TAP LOCATION (Z/D):	2.824	2.75	3.014	3.077	3.454	3.706	3.957
CIRCUMFERENTIAL ANGLE (PHI)							
*****	*****	*****	*****	*****	*****	*****	*****
0.0	-0.010	-0.030	-0.250	-0.351	-0.166	-0.024	-0.012
10.0	-0.018	-0.041	-0.325	-0.357	-0.174	-0.030	-0.089
20.0	-0.030	-0.060	-0.270	-0.368	-0.186	-0.040	-0.086
30.0	-0.054	-0.078	-0.287	-0.385	-0.186	-0.052	-0.014
40.0	-0.084	-0.101	-0.314	-0.406	-0.203	-0.068	-0.024
50.0	-0.117	-0.131	-0.341	-0.430	-0.229	-0.081	-0.029
60.0	-0.146	-0.161	-0.364	-0.451	-0.259	-0.089	-0.068
70.0	-0.170	-0.190	-0.389	-0.475	-0.285	-0.099	-0.086
80.0	-0.195	-0.210	-0.410	-0.489	-0.325	-0.095	-0.097
90.0	-0.216	-0.230	-0.432	-0.500	-0.338	-0.088	-0.092
100.0	-0.224	-0.234	-0.421	-0.488	-0.321	-0.076	-0.079
110.0	-0.225	-0.238	-0.403	-0.453	-0.268	-0.060	-0.060
120.0	-0.220	-0.230	-0.378	-0.426	-0.216	-0.047	-0.045
130.0	-0.195	-0.219	-0.343	-0.396	-0.168	-0.033	-0.030
140.0	-0.168	-0.213	-0.321	-0.368	-0.140	-0.025	-0.020
150.0	-0.179	-0.208	-0.321	-0.368	-0.120	-0.018	-0.012
160.0	-0.164	-0.208	-0.411	-0.430	-0.108	-0.008	-0.005
180.0	-0.180	-0.206	-0.400	-0.429	-0.091	-0.002	-0.003
200.0	-0.180	-0.209	-0.411	-0.430	-0.096	-0.008	-0.005
210.0	-0.191	-0.213	-0.421	-0.449	-0.108	-0.018	-0.025
220.0	-0.200	-0.219	-0.421	-0.449	-0.120	-0.025	-0.030
230.0	-0.211	-0.227	-0.433	-0.468	-0.140	-0.032	-0.038
240.0	-0.221	-0.232	-0.433	-0.468	-0.152	-0.042	-0.045
250.0	-0.226	-0.238	-0.438	-0.486	-0.167	-0.050	-0.050
260.0	-0.223	-0.234	-0.438	-0.486	-0.177	-0.056	-0.059
270.0	-0.214	-0.230	-0.421	-0.468	-0.186	-0.058	-0.057
280.0	-0.214	-0.230	-0.421	-0.468	-0.186	-0.058	-0.057
290.0	-0.175	-0.200	-0.389	-0.432	-0.148	-0.039	-0.039
300.0	-0.140	-0.170	-0.354	-0.389	-0.132	-0.032	-0.032
310.0	-0.117	-0.151	-0.324	-0.354	-0.112	-0.029	-0.029
320.0	-0.083	-0.101	-0.314	-0.340	-0.089	-0.029	-0.029
330.0	-0.050	-0.078	-0.287	-0.314	-0.068	-0.025	-0.025
340.0	-0.030	-0.060	-0.270	-0.285	-0.052	-0.020	-0.014
350.0	-0.019	-0.041	-0.255	-0.270	-0.037	-0.014	-0.006

Figure A-5. Rotating Band Off, $\alpha = 10^\circ$, $P = 0$ rpm

DATA SOURCE : LANGLEY

TAP LOCATION (Z/L): 0.07
TAP LOCATION (Z/D): 0.393

10.4
2.245

0.28
1.571

0.16
0.898

0.5
2.806

CIRCUMFERENTIAL
ANGLE (PHI)

	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.272	0.172	0.083	0.000	-0.322
22.5	0.249	0.149	0.061	-0.020	-0.334
45.0	0.185	0.087	0.002	-0.075	-0.383
67.5	0.103	-0.008	-0.071	-0.142	-0.445
90.0	0.035	-0.056	-0.125	-0.187	-0.468
112.5	0.000	-0.084	-0.136	-0.194	-0.471
135.0	-0.003	-0.091	-0.130	-0.184	-0.445
157.5	0.003	-0.062	-0.118	-0.152	-0.416
180.0	0.013	-0.032	-0.093	-0.118	-0.471
202.5	0.002	-0.071	-0.130	-0.159	-0.462
225.0	-0.003	-0.084	-0.136	-0.187	-0.468
247.5	0.000	-0.070	-0.125	-0.142	-0.445
270.0	0.075	0.008	-0.071	-0.075	-0.383
292.5	0.103	0.087	0.002	0.000	-0.322
315.0	0.155	0.149	0.061	0.020	-0.334
337.5	0.249	0.172	0.083	0.083	-0.322

REF. LENGTH (L): 44.816 IN.
ROT. DIAMETER (D): 7.5 IN.
ROTATING BAND: 0.4 DEG.
MACH NO.: 4.980
ANGLE OF ATTACK (ALPHA): 10
SPIN RATE (P): 4980
TIP SPEED (FT/SEC): 0.16207427
X F/G/L: 0.52513067

DATA SOURCE : RHES

TAP LOCATION (Z/L): 0.503
TAP LOCATION (Z/D): 2.824

0.548
3.077

0.537
3.014

0.526
2.95

0.615
3.454

0.705
3.757

CIRCUMFERENTIAL
ANGLE (PHI)

	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	-0.075	-0.039	-0.250	-0.295	-0.155	0.013
10.0	-0.07	-0.042	-0.255	-0.25	-0.124	0.011
20.0	-0.073	-0.045	-0.256	-0.270	-0.136	0.000
30.0	-0.055	-0.075	-0.282	-0.291	-0.203	-0.015
40.0	-0.097	-0.101	-0.3	-0.318	-0.239	-0.035
50.0	-0.117	-0.131	-0.33	-0.345	-0.259	-0.050
60.0	-0.155	-0.174	-0.356	-0.37	-0.289	-0.065
70.0	-0.179	-0.187	-0.38	-0.407	-0.312	-0.075
80.0	-0.204	-0.211	-0.410	-0.428	-0.329	-0.104
90.0	-0.226	-0.229	-0.419	-0.449	-0.338	-0.105
100.0	-0.231	-0.241	-0.432	-0.458	-0.321	-0.083
120.0	-0.239	-0.246	-0.445	-0.465	-0.277	-0.055
130.0	-0.221	-0.234	-0.432	-0.459	-0.216	-0.053
140.0	-0.212	-0.221	-0.431	-0.452	-0.168	-0.048
150.0	-0.202	-0.211	-0.431	-0.451	-0.120	-0.041
160.0	-0.193	-0.202	-0.426	-0.441	-0.073	-0.028
170.0	-0.187	-0.193	-0.426	-0.441	-0.028	-0.008
180.0	-0.185	-0.185	-0.415	-0.438	0.000	0.000
190.0	-0.181	-0.181	-0.418	-0.436	0.005	0.007
200.0	-0.190	-0.227	-0.448	-0.457	0.011	0.001
210.0	-0.200	-0.219	-0.479	-0.479	0.022	-0.012
220.0	-0.211	-0.222	-0.479	-0.479	0.038	-0.010
230.0	-0.228	-0.232	-0.435	-0.435	0.057	-0.051
240.0	-0.239	-0.240	-0.435	-0.435	0.072	-0.051
250.0	-0.244	-0.243	-0.435	-0.435	0.089	-0.058
260.0	-0.241	-0.241	-0.422	-0.422	0.109	-0.058
270.0	-0.234	-0.234	-0.422	-0.422	0.113	-0.113
280.0	-0.225	-0.225	-0.422	-0.422	0.117	-0.114
290.0	-0.219	-0.219	-0.422	-0.422	0.115	-0.101
300.0	-0.216	-0.216	-0.422	-0.422	0.119	-0.087
310.0	-0.213	-0.213	-0.422	-0.422	0.105	-0.063
320.0	-0.209	-0.209	-0.422	-0.422	0.088	-0.044
330.0	-0.207	-0.207	-0.422	-0.422	0.061	-0.018
340.0	-0.204	-0.204	-0.422	-0.422	0.045	-0.001
350.0	-0.203	-0.203	-0.422	-0.422	0.174	0.012

TAP LOCATION (Z/L): TAP LOCATION (Z/D):	0.75 4.289	0.848 4.757	0.859 4.82	0.87 4.883	0.888 4.983	0.899 5.046	0.91 5.189	0.922 5.176
CIRCUMFERENTIAL ANGLE (PHI)	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0
0.0	-0.005	-0.005	-0.009	-0.010	-0.013	-0.016	-0.020	-0.024
10.0	-0.005	-0.010	-0.013	-0.016	-0.020	-0.024	-0.028	-0.032
20.0	-0.014	-0.019	-0.026	-0.032	-0.040	-0.048	-0.056	-0.064
30.0	-0.033	-0.045	-0.058	-0.072	-0.088	-0.104	-0.120	-0.136
40.0	-0.058	-0.076	-0.096	-0.116	-0.136	-0.156	-0.176	-0.196
50.0	-0.076	-0.103	-0.134	-0.162	-0.190	-0.218	-0.246	-0.274
60.0	-0.092	-0.121	-0.155	-0.187	-0.218	-0.246	-0.274	-0.302
70.0	-0.109	-0.140	-0.175	-0.208	-0.238	-0.266	-0.294	-0.322
80.0	-0.116	-0.150	-0.186	-0.218	-0.246	-0.274	-0.302	-0.330
90.0	-0.115	-0.152	-0.189	-0.220	-0.246	-0.274	-0.302	-0.330
100.0	-0.097	-0.137	-0.175	-0.208	-0.238	-0.266	-0.294	-0.322
110.0	-0.080	-0.120	-0.158	-0.190	-0.218	-0.246	-0.274	-0.302
120.0	-0.071	-0.110	-0.149	-0.181	-0.208	-0.238	-0.266	-0.294
130.0	-0.054	-0.093	-0.132	-0.164	-0.190	-0.218	-0.246	-0.274
140.0	-0.040	-0.079	-0.118	-0.150	-0.176	-0.204	-0.232	-0.260
150.0	-0.031	-0.070	-0.109	-0.141	-0.167	-0.193	-0.220	-0.246
160.0	-0.025	-0.064	-0.103	-0.136	-0.162	-0.188	-0.214	-0.240
170.0	-0.021	-0.061	-0.100	-0.133	-0.159	-0.185	-0.211	-0.237
180.0	-0.031	-0.070	-0.109	-0.141	-0.167	-0.193	-0.220	-0.246
190.0	-0.036	-0.075	-0.114	-0.147	-0.173	-0.200	-0.226	-0.252
200.0	-0.045	-0.084	-0.123	-0.156	-0.182	-0.208	-0.234	-0.260
210.0	-0.052	-0.091	-0.130	-0.163	-0.189	-0.215	-0.241	-0.267
220.0	-0.056	-0.095	-0.134	-0.167	-0.193	-0.219	-0.245	-0.271
230.0	-0.062	-0.101	-0.140	-0.173	-0.199	-0.225	-0.251	-0.277
240.0	-0.066	-0.105	-0.144	-0.177	-0.203	-0.229	-0.255	-0.281
250.0	-0.070	-0.109	-0.148	-0.181	-0.207	-0.233	-0.259	-0.285
260.0	-0.074	-0.113	-0.152	-0.185	-0.211	-0.237	-0.263	-0.289
270.0	-0.077	-0.116	-0.156	-0.189	-0.213	-0.239	-0.265	-0.293
280.0	-0.080	-0.119	-0.159	-0.192	-0.216	-0.242	-0.268	-0.297
290.0	-0.081	-0.120	-0.160	-0.193	-0.217	-0.243	-0.269	-0.299
300.0	-0.081	-0.120	-0.160	-0.193	-0.217	-0.243	-0.269	-0.299
310.0	-0.081	-0.120	-0.160	-0.193	-0.217	-0.243	-0.269	-0.299
320.0	-0.081	-0.120	-0.160	-0.193	-0.217	-0.243	-0.269	-0.299
330.0	-0.081	-0.120	-0.160	-0.193	-0.217	-0.243	-0.269	-0.299
340.0	-0.081	-0.120	-0.160	-0.193	-0.217	-0.243	-0.269	-0.299
350.0	-0.081	-0.120	-0.160	-0.193	-0.217	-0.243	-0.269	-0.299

TAP LOCATION (Z/L): TAP LOCATION (Z/D):	0.75 4.289	0.848 4.757	0.859 4.82	0.87 4.883	0.888 4.983	0.899 5.046	0.91 5.189	0.922 5.176
CIRCUMFERENTIAL ANGLE (PHI)	0.0	10.0	20.0	30.0	40.0	50.0	60.0	70.0
0.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
10.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
20.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
30.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
40.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
50.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
60.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
70.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
80.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
90.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
100.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
110.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
120.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
130.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
140.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
150.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
160.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
170.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
180.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
190.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
200.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
210.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
220.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
230.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
240.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
250.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
260.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
270.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
280.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
290.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
300.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
310.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
320.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
330.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
340.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421
350.0	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421	-0.421

Figure A-6. (Cont'd)

TAP LOCATION (Z/L): 0.75		0.848		0.87		0.888		0.899		0.91		0.922	
TAP LOCATION (Z/D): 4.209		4.757		4.883		4.983		5.046		5.109		5.176	
CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	0.002	-0.232	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
10.0	0.002	-0.232	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
20.0	0.002	-0.232	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
30.0	0.002	-0.232	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
40.0	0.002	-0.232	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
50.0	0.003	-0.234	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
60.0	0.003	-0.234	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
70.0	0.003	-0.234	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
80.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
90.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
100.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
110.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
120.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
130.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
140.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
150.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
160.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
170.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
180.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
190.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
200.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
210.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
220.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
230.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
240.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
250.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
260.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
270.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
280.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
290.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
300.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
310.0	0.003	-0.235	-0.231	-0.23	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
320.0	0.002	-0.251	-0.230	-0.23	-0.261	-0.230	-0.261	-0.230	-0.230	-0.230	-0.230	-0.230	-0.230
330.0	0.002	-0.251	-0.230	-0.23	-0.261	-0.230	-0.261	-0.230	-0.230	-0.230	-0.230	-0.230	-0.230
340.0	0.002	-0.252	-0.230	-0.23	-0.261	-0.230	-0.261	-0.230	-0.230	-0.230	-0.230	-0.230	-0.230
350.0	0.002	-0.252	-0.231	-0.23	-0.261	-0.231	-0.261	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231

TAP LOCATION (Z/L): 0.945		0.969		0.99		5.3	
TAP LOCATION (Z/D): 5.303		5.438		5.5		5.5	
CIRCUMFERENTIAL ANGLE (PHI)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)	PRESSURE COEFFICIENT (CP)
0.0	-0.412	-0.142	-0.090	-0.089	-0.089	-0.089	-0.089
10.0	-0.412	-0.142	-0.089	-0.089	-0.089	-0.089	-0.089
20.0	-0.413	-0.142	-0.089	-0.089	-0.089	-0.089	-0.089
30.0	-0.413	-0.142	-0.089	-0.089	-0.089	-0.089	-0.089
40.0	-0.414	-0.143	-0.086	-0.086	-0.086	-0.086	-0.086
50.0	-0.414	-0.143	-0.086	-0.086	-0.086	-0.086	-0.086
60.0	-0.414	-0.143	-0.084	-0.084	-0.084	-0.084	-0.084
70.0	-0.415	-0.143	-0.083	-0.083	-0.083	-0.083	-0.083
80.0	-0.415	-0.143	-0.083	-0.083	-0.083	-0.083	-0.083
90.0	-0.415	-0.143	-0.083	-0.083	-0.083	-0.083	-0.083
100.0	-0.415	-0.143	-0.083	-0.083	-0.083	-0.083	-0.083
110.0	-0.415	-0.143	-0.083	-0.083	-0.083	-0.083	-0.083
120.0	-0.414	-0.143	-0.084	-0.084	-0.084	-0.084	-0.084
130.0	-0.413	-0.142	-0.084	-0.084	-0.084	-0.084	-0.084
140.0	-0.412	-0.141	-0.085	-0.085	-0.085	-0.085	-0.085
150.0	-0.411	-0.140	-0.085	-0.085	-0.085	-0.085	-0.085
160.0	-0.410	-0.139	-0.085	-0.085	-0.085	-0.085	-0.085
170.0	-0.409	-0.138	-0.085	-0.085	-0.085	-0.085	-0.085
180.0	-0.409	-0.137	-0.085	-0.085	-0.085	-0.085	-0.085
190.0	-0.410	-0.136	-0.082	-0.082	-0.082	-0.082	-0.082
200.0	-0.410	-0.135	-0.082	-0.082	-0.082	-0.082	-0.082
210.0	-0.409	-0.133	-0.081	-0.081	-0.081	-0.081	-0.081
220.0	-0.409	-0.134	-0.081	-0.081	-0.081	-0.081	-0.081
230.0	-0.409	-0.135	-0.080	-0.080	-0.080	-0.080	-0.080
240.0	-0.409	-0.137	-0.080	-0.080	-0.080	-0.080	-0.080
250.0	-0.408	-0.137	-0.079	-0.079	-0.079	-0.079	-0.079
260.0	-0.408	-0.138	-0.078	-0.078	-0.078	-0.078	-0.078
270.0	-0.407	-0.139	-0.079	-0.079	-0.079	-0.079	-0.079
280.0	-0.407	-0.139	-0.081	-0.081	-0.081	-0.081	-0.081
290.0	-0.409	-0.140	-0.083	-0.083	-0.083	-0.083	-0.083
300.0	-0.410	-0.140	-0.083	-0.083	-0.083	-0.083	-0.083
310.0	-0.410	-0.140	-0.084	-0.084	-0.084	-0.084	-0.084
320.0	-0.410	-0.140	-0.086	-0.086	-0.086	-0.086	-0.086
330.0	-0.411	-0.141	-0.086	-0.086	-0.086	-0.086	-0.086
340.0	-0.411	-0.141	-0.089	-0.089	-0.089	-0.089	-0.089
350.0	-0.412	-0.141	-0.089	-0.089	-0.089	-0.089	-0.089

REF. LENGTH (L): 44.616 IN.
 REF. DIAMETER (D): 7.95 IN.
 POTATING BAND: 0.94 IN.
 TAP NO.: 0
 ANGLE OF ATTACK (ALPHA): 0 DEG.
 TAP RATE (CP): 0 PER MIN
 TAP SPEED (FT/20): 0.625112667 X 10⁻⁶

Figure A-7. (Cont'd)

DATA SOURCE : LANGLEY

TAP LOCATION (Z/D):	0.16	0.28	0.4	0.5
TAP LOCATION (Z/D):	0.33	1.571	2.245	2.886
CIRCUMFERENTIAL ANGLE (PHI):	0.0	0.0	0.0	0.0
0.0	0.027	-0.044	-0.105	-0.184
22.5	0.000	0.000	0.000	0.000
45.0	0.000	0.000	0.000	0.000
67.5	0.000	0.000	0.000	0.000
90.0	0.035	-0.037	-0.100	-0.186
112.5	0.000	0.000	0.000	0.000
135.0	0.000	0.000	0.000	0.000
157.5	0.000	0.000	0.000	0.000
180.0	0.122	-0.039	-0.101	-0.186
202.5	0.000	0.000	0.000	0.000
225.0	0.000	0.000	0.000	0.000
247.5	0.000	0.000	0.000	0.000
270.0	0.000	-0.037	-0.100	-0.186
292.5	0.000	0.000	0.000	0.000
315.0	0.000	0.000	0.000	0.000
337.5	0.000	0.000	0.000	0.000
360.0	0.000	0.000	0.000	0.000

REF. LENGTH (L): 44.616 IN.
 REF. DIAMETER (D): 7.95 IN.
 ROTATING BAND: 0.94 DEG
 MACH NO.: 0.900 REV/MIN
 ANGLE OF ATTACK (ALPHA): 0.12027427
 SPIN RATE (P): 0.625112667
 TIP SPEED RATIO (PD/2V): X CG/L

DATA SOURCE : OWES

TAP LOCATION (Z/D):	0.326	0.549	0.615	0.65
TAP LOCATION (Z/D):	2.55	3.877	3.454	3.766
CIRCUMFERENTIAL ANGLE (PHI):	0.0	0.0	0.0	0.0
0.0	-0.127	-0.361	-0.274	-0.036
18.0	-0.127	-0.361	-0.274	-0.036
36.0	-0.127	-0.361	-0.274	-0.036
54.0	-0.127	-0.361	-0.274	-0.036
72.0	-0.127	-0.361	-0.274	-0.036
90.0	-0.127	-0.361	-0.274	-0.036
108.0	-0.128	-0.360	-0.273	-0.036
126.0	-0.128	-0.360	-0.273	-0.036
144.0	-0.128	-0.360	-0.273	-0.036
162.0	-0.129	-0.359	-0.272	-0.036
180.0	-0.129	-0.359	-0.272	-0.036
198.0	-0.129	-0.359	-0.272	-0.036
216.0	-0.129	-0.359	-0.272	-0.036
234.0	-0.129	-0.359	-0.272	-0.036
252.0	-0.129	-0.359	-0.272	-0.036
270.0	-0.129	-0.359	-0.272	-0.036
288.0	-0.129	-0.359	-0.272	-0.036
306.0	-0.129	-0.359	-0.272	-0.036
324.0	-0.129	-0.359	-0.272	-0.036
342.0	-0.129	-0.359	-0.272	-0.036
360.0	-0.127	-0.361	-0.274	-0.036

Figure A-8. Rotating Band On, $\alpha = 0^\circ$, $P = 4900$ rpm

DATA SOURCE : LANGLEY

TAP LOCATION (Z, D)	0.07 0.395	0.16 0.846	0.28 1.571	0.4 2.445	0.5 2.806
CIRCUMFERENTIAL ANGLE (PHI)	0.0	0.0	0.0	0.0	0.0
0.0	0.244	0.172	0.083	0.000	-0.322
2.5	0.185	0.144	0.061	-0.020	-0.339
5.0	0.105	0.087	0.002	-0.075	-0.432
7.5	0.035	0.003	-0.071	-0.14	-0.482
10.0	-0.000	-0.056	-0.135	-0.187	-0.482
12.5	-0.030	-0.084	-0.136	-0.193	-0.471
15.0	-0.060	-0.081	-0.130	-0.184	-0.446
17.5	-0.086	-0.081	-0.118	-0.164	-0.446
20.0	-0.113	-0.085	-0.096	-0.152	-0.447
22.5	-0.140	-0.072	-0.113	-0.164	-0.446
25.0	-0.167	-0.081	-0.136	-0.194	-0.471
27.5	-0.194	-0.084	-0.136	-0.187	-0.482
30.0	-0.220	-0.098	-0.113	-0.167	-0.466
32.5	-0.245	-0.103	-0.081	-0.142	-0.445
35.0	-0.270	-0.108	-0.061	-0.117	-0.423
37.5	-0.295	-0.114	-0.061	-0.100	-0.399

REF. LENGTH (L): 44.616 IN.
 REF. DIAMETER (D): 7.95 IN.
 ROTATING BAND: ON
 ANGLE OF ATTACK (ALPHA): 0.94 DEG.
 SPIN RATE (RPM): 0
 TIP SPEED RATIO (PD/2V): 0
 X CG/L: 0.625113067

DATA SOURCE : AMES

TAP LOCATION (Z, D)	0.503 2.824	0.545 3.35	0.557 3.014	0.548 3.077	0.571 3.203	0.585 3.457	0.705 3.95
CIRCUMFERENTIAL ANGLE (PHI)	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	-0.010	-0.030	-0.250	-0.251	-0.260	-0.012	-0.012
2.5	-0.015	-0.041	-0.255	-0.37	-0.270	-0.009	-0.009
5.0	-0.030	-0.080	-0.270	-0.368	-0.285	-0.006	-0.006
7.5	-0.054	-0.092	-0.287	-0.385	-0.303	-0.002	-0.002
10.0	-0.084	-0.101	-0.314	-0.406	-0.330	-0.008	-0.014
12.5	-0.117	-0.111	-0.341	-0.430	-0.360	-0.029	-0.029
15.0	-0.146	-0.121	-0.369	-0.451	-0.387	-0.068	-0.049
17.5	-0.175	-0.130	-0.394	-0.475	-0.412	-0.081	-0.068
20.0	-0.205	-0.139	-0.421	-0.500	-0.432	-0.051	-0.051
22.5	-0.234	-0.144	-0.432	-0.503	-0.451	-0.032	-0.032
25.0	-0.264	-0.153	-0.433	-0.503	-0.458	-0.009	-0.009
27.5	-0.294	-0.161	-0.433	-0.498	-0.451	-0.002	-0.002
30.0	-0.324	-0.167	-0.432	-0.486	-0.438	-0.008	-0.008
32.5	-0.354	-0.173	-0.432	-0.468	-0.418	-0.025	-0.025
35.0	-0.384	-0.179	-0.432	-0.443	-0.400	-0.033	-0.033
37.5	-0.414	-0.184	-0.432	-0.434	-0.400	-0.020	-0.020
40.0	-0.444	-0.189	-0.432	-0.430	-0.400	-0.008	-0.008
42.5	-0.474	-0.194	-0.432	-0.430	-0.400	-0.002	-0.002
45.0	-0.504	-0.199	-0.432	-0.434	-0.400	-0.008	-0.008
47.5	-0.534	-0.204	-0.432	-0.434	-0.400	-0.008	-0.008
50.0	-0.564	-0.209	-0.432	-0.434	-0.400	-0.007	-0.007
52.5	-0.594	-0.214	-0.432	-0.434	-0.400	-0.005	-0.005
55.0	-0.624	-0.219	-0.432	-0.434	-0.400	-0.003	-0.003
57.5	-0.654	-0.224	-0.432	-0.434	-0.400	-0.002	-0.002
60.0	-0.684	-0.229	-0.432	-0.434	-0.400	-0.002	-0.002
62.5	-0.714	-0.234	-0.432	-0.434	-0.400	-0.001	-0.001
65.0	-0.744	-0.239	-0.432	-0.434	-0.400	-0.001	-0.001
67.5	-0.774	-0.244	-0.432	-0.434	-0.400	-0.001	-0.001
70.0	-0.804	-0.249	-0.432	-0.434	-0.400	-0.001	-0.001
72.5	-0.834	-0.254	-0.432	-0.434	-0.400	-0.001	-0.001
75.0	-0.864	-0.259	-0.432	-0.434	-0.400	-0.001	-0.001
77.5	-0.894	-0.264	-0.432	-0.434	-0.400	-0.001	-0.001
80.0	-0.924	-0.269	-0.432	-0.434	-0.400	-0.001	-0.001
82.5	-0.954	-0.274	-0.432	-0.434	-0.400	-0.001	-0.001
85.0	-0.984	-0.279	-0.432	-0.434	-0.400	-0.001	-0.001
87.5	-1.014	-0.284	-0.432	-0.434	-0.400	-0.001	-0.001
90.0	-1.044	-0.289	-0.432	-0.434	-0.400	-0.001	-0.001
92.5	-1.074	-0.294	-0.432	-0.434	-0.400	-0.001	-0.001
95.0	-1.104	-0.299	-0.432	-0.434	-0.400	-0.001	-0.001
97.5	-1.134	-0.304	-0.432	-0.434	-0.400	-0.001	-0.001
100.0	-1.164	-0.309	-0.432	-0.434	-0.400	-0.001	-0.001
102.5	-1.194	-0.314	-0.432	-0.434	-0.400	-0.001	-0.001
105.0	-1.224	-0.319	-0.432	-0.434	-0.400	-0.001	-0.001
107.5	-1.254	-0.324	-0.432	-0.434	-0.400	-0.001	-0.001
110.0	-1.284	-0.329	-0.432	-0.434	-0.400	-0.001	-0.001
112.5	-1.314	-0.334	-0.432	-0.434	-0.400	-0.001	-0.001
115.0	-1.344	-0.339	-0.432	-0.434	-0.400	-0.001	-0.001
117.5	-1.374	-0.344	-0.432	-0.434	-0.400	-0.001	-0.001
120.0	-1.404	-0.349	-0.432	-0.434	-0.400	-0.001	-0.001
122.5	-1.434	-0.354	-0.432	-0.434	-0.400	-0.001	-0.001
125.0	-1.464	-0.359	-0.432	-0.434	-0.400	-0.001	-0.001
127.5	-1.494	-0.364	-0.432	-0.434	-0.400	-0.001	-0.001
130.0	-1.524	-0.369	-0.432	-0.434	-0.400	-0.001	-0.001
132.5	-1.554	-0.374	-0.432	-0.434	-0.400	-0.001	-0.001
135.0	-1.584	-0.379	-0.432	-0.434	-0.400	-0.001	-0.001
137.5	-1.614	-0.384	-0.432	-0.434	-0.400	-0.001	-0.001
140.0	-1.644	-0.389	-0.432	-0.434	-0.400	-0.001	-0.001
142.5	-1.674	-0.394	-0.432	-0.434	-0.400	-0.001	-0.001
145.0	-1.704	-0.399	-0.432	-0.434	-0.400	-0.001	-0.001
147.5	-1.734	-0.404	-0.432	-0.434	-0.400	-0.001	-0.001
150.0	-1.764	-0.409	-0.432	-0.434	-0.400	-0.001	-0.001
152.5	-1.794	-0.414	-0.432	-0.434	-0.400	-0.001	-0.001
155.0	-1.824	-0.419	-0.432	-0.434	-0.400	-0.001	-0.001
157.5	-1.854	-0.424	-0.432	-0.434	-0.400	-0.001	-0.001
160.0	-1.884	-0.429	-0.432	-0.434	-0.400	-0.001	-0.001
162.5	-1.914	-0.434	-0.432	-0.434	-0.400	-0.001	-0.001
165.0	-1.944	-0.439	-0.432	-0.434	-0.400	-0.001	-0.001
167.5	-1.974	-0.444	-0.432	-0.434	-0.400	-0.001	-0.001
170.0	-2.004	-0.449	-0.432	-0.434	-0.400	-0.001	-0.001
172.5	-2.034	-0.454	-0.432	-0.434	-0.400	-0.001	-0.001
175.0	-2.064	-0.459	-0.432	-0.434	-0.400	-0.001	-0.001
177.5	-2.094	-0.464	-0.432	-0.434	-0.400	-0.001	-0.001
180.0	-2.124	-0.469	-0.432	-0.434	-0.400	-0.001	-0.001
182.5	-2.154	-0.474	-0.432	-0.434	-0.400	-0.001	-0.001
185.0	-2.184	-0.479	-0.432	-0.434	-0.400	-0.001	-0.001
187.5	-2.214	-0.484	-0.432	-0.434	-0.400	-0.001	-0.001
190.0	-2.244	-0.489	-0.432	-0.434	-0.400	-0.001	-0.001
192.5	-2.274	-0.494	-0.432	-0.434	-0.400	-0.001	-0.001
195.0	-2.304	-0.499	-0.432	-0.434	-0.400	-0.001	-0.001
197.5	-2.334	-0.504	-0.432	-0.434	-0.400	-0.001	-0.001
200.0	-2.364	-0.509	-0.432	-0.434	-0.400	-0.001	-0.001
202.5	-2.394	-0.514	-0.432	-0.434	-0.400	-0.001	-0.001
205.0	-2.424	-0.519	-0.432	-0.434	-0.400	-0.001	-0.001
207.5	-2.454	-0.524	-0.432	-0.434	-0.400	-0.001	-0.001
210.0	-2.484	-0.529	-0.432	-0.434	-0.400	-0.001	-0.001
212.5	-2.514	-0.534	-0.432	-0.434	-0.400	-0.001	-0.001
215.0	-2.544	-0.539	-0.432	-0.434	-0.400	-0.001	-0.001
217.5	-2.574	-0.544	-0.432	-0.434	-0.400	-0.001	-0.001
220.0	-2.604	-0.549	-0.432	-0.434	-0.400	-0.001	-0.001
222.5	-2.634	-0.554	-0.432	-0.434	-0.400	-0.001	-0.001
225.0	-2.664	-0.559	-0.432	-0.434	-0.400	-0.001	-0.001
227.5	-2.694	-0.564	-0.432	-0.434	-0.400	-0.001	-0.001
230.0	-2.724	-0.569	-0.432	-0.434	-0.400	-0.001	-0.001
232.5	-2.754	-0.574	-0.432	-0.434	-0.400	-0.001	-0.001
235.0	-2.784	-0.579	-0.432	-0.434	-0.400	-0.001	-0.001
237.5	-2.814	-0.584	-0.432	-0.434	-0.400	-0.001	-0.001
240.0	-2.844	-0.589	-0.432	-0.434	-0.400	-0.001	-0.001
242.5	-2.874	-0.594	-0.432	-0.434	-0.400	-0.001	-0.001
245.0	-2.904	-0.599	-0.432	-0.434	-0.400	-0.001	-0.001
247.5	-2.934	-0.604	-0.432	-0.434	-0.400	-0.001	-0.001
250.0	-2.964	-0.609	-0.432	-0.434	-0.400	-0.001	-0.001
252.5	-2.994	-0.614	-0.432	-0.434	-0.400	-0.001	-0.001
255.0	-3.024	-0.619	-0.432	-0.434	-0.400	-0.001	-0.001
257.5	-3.054	-0.624	-0.432	-0.434	-0.400	-0.001	-0.001
260.0	-3.084	-0.629	-0.432	-0.434	-0.400	-0.001	-0.001
262.5	-3.114	-0.634	-0.432	-0.434	-0.400	-0.001	-0.001
265.0	-3.144	-0.639	-0.432	-0.434	-0.400	-0.001	-0.001
267.5	-3.174	-0.644	-0.432	-0.434	-0.400	-0.001	-0.001
270.0	-3.204	-0.649	-0.432	-0.434	-0.400	-0.001	-0.001
272.5	-3.234	-0.654	-0.432	-0.434	-0.400	-0.001	-0.001
275.0	-3.264	-0.659	-0.432	-0.434	-0.400	-0.001	-0.001
277.5	-3.294	-0.664	-0.432	-0.434	-0.400	-0.001	-0.001
280.0	-3.324	-0.669	-0.432	-0.434	-0.400	-0.001	-0.001
282.5	-3.354	-0.674	-0.432	-0.434	-0.400	-0.001	-0.001
285.0	-3.384	-0.679	-0.432	-0.434	-0.400	-0.001	-0.001
287.5	-3.414	-0.684	-0.432	-0.434	-0.400	-0.001	-0.001
290.0	-3.444	-0.689	-0.432	-0.434	-0.400	-0.001	-0.001
292.5	-3.474	-0.694	-0.432	-0.434	-0.400	-0.001	-0.001
295.0	-3.504	-0.699	-0.432	-0.434	-0.400	-0.001	-0.001
297.5	-3.534	-0.704	-0.432	-0.434	-0.400	-0.001	-0.001
300.0	-3.564	-0.709	-0.432	-0.434	-0.400	-0.001	-0.001
302.5	-3.594	-0.714	-0.432	-0.434	-0.400	-0.001	-0.001
305.0	-3.624	-0.719	-0.432	-0.434	-0.400	-0.001	-0.001
307.5	-3.654	-0.724	-0.432	-0.434	-0.400	-0.001	-0.001
310.0	-3.684	-0.729	-0.432	-0.434	-0.400	-0.001	-0.001
312.5	-3.714	-0.734	-0.432	-0.434	-0.400	-0.001	-0.001
315.0	-3.744	-0.739	-0.432	-0.434	-0.400	-0.001	-0.001
317.5	-3.774	-0.744	-0.432	-0.434	-0.400	-0.001	-0.001
320.0	-3.804	-0.749	-0.432	-0.434	-0.400	-0.001	-0.001
322.5	-3.834	-0.754	-0.432	-0.434	-0.400	-0.001	-0.001
325.0	-3.864	-0.759	-0.432	-0.434	-0.400	-0.001	-0.001
327.5	-3.894	-0.764	-0.432	-0.434	-0.400	-0.001	-0.001
330.0	-3.924	-0.769	-0.432	-0.434	-0.400	-0.001	-0.001
332.5	-3.954	-0.774	-0.432	-0.434	-0.400	-0.001	-0.001
335.0	-3.984	-0.779	-0.432	-0.434	-0.400	-0.001	-0.001
337.5	-4.014	-0.784	-0.432	-0.434	-0.400	-0.001	-0.001
340.0	-4.044	-0.789	-0.432	-0.434	-0.400	-0.001	-0.001
342.5	-4.074	-0.794	-0.432	-0.434	-0.400	-0.001	-0.001
345.0	-4.104	-0.799	-0.432	-0.434	-0.400	-0.001	-0.001
347.5	-4.134	-0.804	-0.432	-0.434	-0.400	-0.001	-0.001
350.0	-4.164	-0.809	-0.432	-0.434	-0.400	-0.001	-0.001
352.5	-4.194	-0.814	-0.432	-0.434	-0.400	-0.001	-0.001
355.0	-4.224	-0.819	-0.432	-0.434	-0.400	-0.001	-0.001
357.5	-4.254	-0.824	-0.432	-0.434	-0.400	-0.001	-0.001
360.0	-4.284	-0.829	-0.432	-0.434	-0.400	-0.001	-0.001
362.5	-4.314	-0.834	-0.432</				

CIRCUMFERENTIAL ANGLE (PHI)	LOCATION (Z/L): LOCATION (Z/D):	0.75 4.289	0.848 4.757	0.959 4.82	0.87 4.883	0.888 4.983	0.899 5.046	0.91 5.189	0.922 5.176
0.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
10.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
20.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
30.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
40.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
50.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
60.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
70.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
80.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
90.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
100.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
110.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
120.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
130.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
140.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
150.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
160.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
170.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
180.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
190.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
200.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
210.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
220.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
230.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
240.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
250.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
260.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
270.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
280.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
290.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
300.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
310.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
320.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
330.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
340.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81
350.0		0.81	0.81	0.81	0.81	0.81	0.81	0.81	0.81

CIRCUMFERENTIAL ANGLE (PHI)	TAP LOCATION (Z/L): TAP LOCATION (Z/D):	0.945 5.303	0.969 5.438	0.98 5.5	0.969 5.438	0.969 5.438	0.969 5.438	0.969 5.438	0.969 5.438
0.0		0.421	0.375	0.368	0.368	0.368	0.368	0.368	0.368
10.0		0.428	0.371	0.375	0.375	0.375	0.375	0.375	0.375
20.0		0.435	0.362	0.383	0.383	0.383	0.383	0.383	0.383
30.0		0.450	0.397	0.399	0.399	0.399	0.399	0.399	0.399
40.0		0.471	0.418	0.414	0.414	0.414	0.414	0.414	0.414
50.0		0.492	0.436	0.415	0.415	0.415	0.415	0.415	0.415
60.0		0.518	0.455	0.411	0.411	0.411	0.411	0.411	0.411
70.0		0.535	0.458	0.358	0.358	0.358	0.358	0.358	0.358
80.0		0.552	0.411	0.269	0.269	0.269	0.269	0.269	0.269
90.0		0.574	0.333	0.187	0.187	0.187	0.187	0.187	0.187
100.0		0.598	0.259	0.137	0.137	0.137	0.137	0.137	0.137
110.0		0.618	0.177	0.089	0.089	0.089	0.089	0.089	0.089
120.0		0.635	0.123	0.081	0.081	0.081	0.081	0.081	0.081
130.0		0.655	0.117	0.075	0.075	0.075	0.075	0.075	0.075
140.0		0.679	0.109	0.073	0.073	0.073	0.073	0.073	0.073
150.0		0.700	0.087	0.069	0.069	0.069	0.069	0.069	0.069
160.0		0.727	0.068	0.054	0.054	0.054	0.054	0.054	0.054
170.0		0.758	0.055	0.024	0.024	0.024	0.024	0.024	0.024
180.0		0.793	0.055	0.065	0.065	0.065	0.065	0.065	0.065
190.0		0.833	0.088	0.083	0.083	0.083	0.083	0.083	0.083
200.0		0.878	0.110	0.092	0.092	0.092	0.092	0.092	0.092
210.0		0.924	0.128	0.094	0.094	0.094	0.094	0.094	0.094
220.0		0.972	0.131	0.094	0.094	0.094	0.094	0.094	0.094
230.0		1.022	0.142	0.095	0.095	0.095	0.095	0.095	0.095
240.0		1.074	0.153	0.101	0.101	0.101	0.101	0.101	0.101
250.0		1.128	0.168	0.109	0.109	0.109	0.109	0.109	0.109
260.0		1.184	0.178	0.127	0.127	0.127	0.127	0.127	0.127
270.0		1.242	0.189	0.136	0.136	0.136	0.136	0.136	0.136
280.0		1.302	0.199	0.145	0.145	0.145	0.145	0.145	0.145
290.0		1.364	0.208	0.153	0.153	0.153	0.153	0.153	0.153
300.0		1.428	0.216	0.161	0.161	0.161	0.161	0.161	0.161
310.0		1.494	0.223	0.168	0.168	0.168	0.168	0.168	0.168
320.0		1.562	0.229	0.174	0.174	0.174	0.174	0.174	0.174
330.0		1.632	0.234	0.179	0.179	0.179	0.179	0.179	0.179
340.0		1.704	0.238	0.183	0.183	0.183	0.183	0.183	0.183
350.0		1.778	0.241	0.186	0.186	0.186	0.186	0.186	0.186

REF. LENGTH (L): 44.616 IN.
 REF. DIAMETER (D): 7.95 IN.
 ROTATING BAND: ON
 MACH NO.: 0.94
 ANGLE OF ATTACK (ALPHA): 10 DEG.
 SPIN RATE (P): 0 REV/MIN
 TIP SPEED RATIO (PD/2V): 0.62512067
 X CG/L

Figure A-9. (Cont'd)

DATA SOURCE : LANGLEY

TAP LOCATION (Z/L):	0.07	0.16	0.28	0.4	0.5
TAP LOCATION (Z/D):	0.393	0.898	1.571	2.245	2.886
CIRCUMFERENTIAL					
ANGLE (PHI)					

0.0	0.272	0.172	0.083	0.008	-0.325
22.5	0.249	0.149	0.061	-0.028	-0.353
45.0	0.185	0.087	0.002	-0.075	-0.383
67.5	0.103	0.008	-0.071	-0.145	-0.445
90.0	0.005	-0.056	-0.152	-0.187	-0.468
112.5	-0.080	-0.084	-0.136	-0.189	-0.485
135.0	-0.003	-0.081	-0.108	-0.184	-0.471
157.5	0.006	-0.072	-0.118	-0.184	-0.445
180.0	0.013	-0.059	-0.098	-0.152	-0.447
202.5	0.006	-0.072	-0.118	-0.152	-0.446
225.0	-0.003	-0.081	-0.136	-0.184	-0.471
247.5	0.003	-0.084	-0.136	-0.189	-0.485
270.0	0.030	-0.056	-0.125	-0.142	-0.445
292.5	0.103	0.009	-0.071	-0.075	-0.383
315.0	0.185	0.087	0.002	-0.028	-0.353
337.5	0.249	0.149	0.061	-0.028	-0.325

REF. LENGTH (L): 44.616 IN.
 REF. DIAMETER (D): 7.95 IN.
 ROTATING BAND: ON
 MACH NO.: 0.94
 ANGLE OF ATTACK (ALPHA): 10 DEG.
 SPIN RATE (P): 4900 REV/MIN
 TIP SPEED RATIO (PD/2V): 0.162827427
 X CC/L 0.625112867

DATA SOURCE : NMEP

TAP LOCATION (Z/L):	0.503	0.526	0.537	0.548	0.571
TAP LOCATION (Z/D):	2.824	2.95	3.014	3.077	3.203
CIRCUMFERENTIAL					
ANGLE (PHI)					

0.0	0.227	0.132	0.049	-0.349	-0.532
15.0	0.230	0.135	0.052	-0.350	-0.532
30.0	0.233	0.138	0.055	-0.353	-0.535
45.0	0.236	0.141	0.058	-0.356	-0.538
60.0	0.239	0.144	0.061	-0.359	-0.541
75.0	0.242	0.147	0.064	-0.362	-0.544
90.0	0.245	0.150	0.067	-0.365	-0.547
105.0	0.248	0.153	0.070	-0.368	-0.550
120.0	0.251	0.156	0.073	-0.371	-0.553
135.0	0.254	0.159	0.076	-0.374	-0.556
150.0	0.257	0.162	0.079	-0.377	-0.559
165.0	0.260	0.165	0.082	-0.380	-0.562
180.0	0.263	0.168	0.085	-0.383	-0.565
195.0	0.266	0.171	0.088	-0.386	-0.568
210.0	0.269	0.174	0.091	-0.389	-0.571
225.0	0.272	0.177	0.094	-0.392	-0.574
240.0	0.275	0.180	0.097	-0.395	-0.577
255.0	0.278	0.183	0.100	-0.398	-0.580
270.0	0.281	0.186	0.103	-0.401	-0.583
285.0	0.284	0.189	0.106	-0.404	-0.586
300.0	0.287	0.192	0.109	-0.407	-0.589
315.0	0.290	0.195	0.112	-0.410	-0.592
330.0	0.293	0.198	0.115	-0.413	-0.595
345.0	0.296	0.201	0.118	-0.416	-0.598
360.0	0.299	0.204	0.121	-0.419	-0.601
375.0	0.302	0.207	0.124	-0.422	-0.604
390.0	0.305	0.210	0.127	-0.425	-0.607
405.0	0.308	0.213	0.130	-0.428	-0.610
420.0	0.311	0.216	0.133	-0.431	-0.613
435.0	0.314	0.219	0.136	-0.434	-0.616
450.0	0.317	0.222	0.139	-0.437	-0.619
465.0	0.320	0.225	0.142	-0.440	-0.622
480.0	0.323	0.228	0.145	-0.443	-0.625
495.0	0.326	0.231	0.148	-0.446	-0.628
510.0	0.329	0.234	0.151	-0.449	-0.631
525.0	0.332	0.237	0.154	-0.452	-0.634
540.0	0.335	0.240	0.157	-0.455	-0.637
555.0	0.338	0.243	0.160	-0.458	-0.640
570.0	0.341	0.246	0.163	-0.461	-0.643
585.0	0.344	0.249	0.166	-0.464	-0.646
600.0	0.347	0.252	0.169	-0.467	-0.649
615.0	0.350	0.255	0.172	-0.470	-0.652
630.0	0.353	0.258	0.175	-0.473	-0.655
645.0	0.356	0.261	0.178	-0.476	-0.658
660.0	0.359	0.264	0.181	-0.479	-0.661
675.0	0.362	0.267	0.184	-0.482	-0.664
690.0	0.365	0.270	0.187	-0.485	-0.667
705.0	0.368	0.273	0.190	-0.488	-0.670
720.0	0.371	0.276	0.193	-0.491	-0.673
735.0	0.374	0.279	0.196	-0.494	-0.676
750.0	0.377	0.282	0.199	-0.497	-0.679
765.0	0.380	0.285	0.202	-0.500	-0.682
780.0	0.383	0.288	0.205	-0.503	-0.685
795.0	0.386	0.291	0.208	-0.506	-0.688
810.0	0.389	0.294	0.211	-0.509	-0.691
825.0	0.392	0.297	0.214	-0.512	-0.694
840.0	0.395	0.300	0.217	-0.515	-0.697
855.0	0.398	0.303	0.220	-0.518	-0.700
870.0	0.401	0.306	0.223	-0.521	-0.703
885.0	0.404	0.309	0.226	-0.524	-0.706
900.0	0.407	0.312	0.229	-0.527	-0.709
915.0	0.410	0.315	0.232	-0.530	-0.712
930.0	0.413	0.318	0.235	-0.533	-0.715
945.0	0.416	0.321	0.238	-0.536	-0.718
960.0	0.419	0.324	0.241	-0.539	-0.721
975.0	0.422	0.327	0.244	-0.542	-0.724
990.0	0.425	0.330	0.247	-0.545	-0.727
1005.0	0.428	0.333	0.250	-0.548	-0.730
1020.0	0.431	0.336	0.253	-0.551	-0.733
1035.0	0.434	0.339	0.256	-0.554	-0.736
1050.0	0.437	0.342	0.259	-0.557	-0.739
1065.0	0.440	0.345	0.262	-0.560	-0.742
1080.0	0.443	0.348	0.265	-0.563	-0.745
1095.0	0.446	0.351	0.268	-0.566	-0.748
1110.0	0.449	0.354	0.271	-0.569	-0.751
1125.0	0.452	0.357	0.274	-0.572	-0.754
1140.0	0.455	0.360	0.277	-0.575	-0.757
1155.0	0.458	0.363	0.280	-0.578	-0.760
1170.0	0.461	0.366	0.283	-0.581	-0.763
1185.0	0.464	0.369	0.286	-0.584	-0.766
1200.0	0.467	0.372	0.289	-0.587	-0.769
1215.0	0.470	0.375	0.292	-0.590	-0.772
1230.0	0.473	0.378	0.295	-0.593	-0.775
1245.0	0.476	0.381	0.298	-0.596	-0.778
1260.0	0.479	0.384	0.301	-0.599	-0.781
1275.0	0.482	0.387	0.304	-0.602	-0.784
1290.0	0.485	0.390	0.307	-0.605	-0.787
1305.0	0.488	0.393	0.310	-0.608	-0.790
1320.0	0.491	0.396	0.313	-0.611	-0.793
1335.0	0.494	0.399	0.316	-0.614	-0.796
1350.0	0.497	0.402	0.319	-0.617	-0.799
1365.0	0.500	0.405	0.322	-0.620	-0.802
1380.0	0.503	0.408	0.325	-0.623	-0.805
1395.0	0.506	0.411	0.328	-0.626	-0.808
1410.0	0.509	0.414	0.331	-0.629	-0.811
1425.0	0.512	0.417	0.334	-0.632	-0.814
1440.0	0.515	0.420	0.337	-0.635	-0.817
1455.0	0.518	0.423	0.340	-0.638	-0.820
1470.0	0.521	0.426	0.343	-0.641	-0.823
1485.0	0.524	0.429	0.346	-0.644	-0.826
1500.0	0.527	0.432	0.349	-0.647	-0.829
1515.0	0.530	0.435	0.352	-0.650	-0.832
1530.0	0.533	0.438	0.355	-0.653	-0.835
1545.0	0.536	0.441	0.358	-0.656	-0.838
1560.0	0.539	0.444	0.361	-0.659	-0.841
1575.0	0.542	0.447	0.364	-0.662	-0.844
1590.0	0.545	0.450	0.367	-0.665	-0.847
1605.0	0.548	0.453	0.370	-0.668	-0.850
1620.0	0.551	0.456	0.373	-0.671	-0.853
1635.0	0.554	0.459	0.376	-0.674	-0.856
1650.0	0.557	0.462	0.379	-0.677	-0.859
1665.0	0.560	0.465	0.382	-0.680	-0.862
1680.0	0.563	0.468	0.385	-0.683	-0.865
1695.0	0.566	0.471	0.388	-0.686	-0.868
1710.0	0.569	0.474	0.391	-0.689	-0.871
1725.0	0.572	0.477	0.394	-0.692	-0.874
1740.0	0.575	0.480	0.397	-0.695	-0.877
1755.0	0.578	0.483	0.400	-0.698	-0.880
1770.0	0.581	0.486	0.403	-0.701	-0.883
1785.0	0.584	0.489	0.406	-0.704	-0.886
1800.0	0.587	0.492	0.409	-0.707	-0.889
1815.0	0.590	0.495	0.412	-0.710	-0.892
1830.0	0.593	0.498	0.415	-0.713	-0.895
1845.0	0.596	0.501	0.418	-0.716	-0.898
1860.0	0.599	0.504	0.421	-0.719	-0.901
1875.0	0.602	0.507	0.424	-0.722	-0.904
1890.0	0.605	0.510	0.427	-0.725	-0.907
1905.0	0.608	0.513	0.430	-0.728	-0.910
1920.0	0.611	0.516	0.433	-0.731	-0.913
1935.0	0.614	0.519	0.436	-0.734	-0.916
1950.0	0.617	0.522	0.439	-0.737	-0.919
1965.0	0.620	0.525	0.442	-0.740	-0.922
1980.0	0.623	0.528	0.445	-0.743	-0.925
1995.0	0.626	0.531	0.448	-0.746	-0.928
2010.0	0.629	0.534	0.451	-0.749	-0.931
2025.0	0.632	0.537	0.454	-0.752	-0.934
2040.0	0.635	0.540	0.457	-0.755	-0.937
2055.0	0.638	0.543	0.460	-0.758	-0.940
2070.0	0.641	0.546	0.463	-0.761	-0.943
2085.0	0.644	0.549	0.466	-0.764	-0.946
2100.0	0.647	0.552	0.469	-0.	

TAP LOCATION (Z/L): TAP LOCATION (Z/D):	0.75 4.289	0.848 4.757	0.859 4.82	0.87 4.883	0.888 4.983	0.899 5.046	0.91 5.189	0.922 5.176
CIRCUMFERENTIAL ANGLE (PHI)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.011	0.009	0.007	0.006	0.005	0.004	0.003	0.002
10.0	0.008	0.006	0.005	0.004	0.003	0.002	0.001	0.000
20.0	0.002	0.001	0.000	0.000	0.000	0.000	0.000	0.000
30.0	0.012	0.009	0.006	0.005	0.004	0.003	0.002	0.001
40.0	0.030	0.025	0.018	0.016	0.014	0.012	0.010	0.008
50.0	0.044	0.035	0.025	0.022	0.019	0.016	0.014	0.012
60.0	0.057	0.043	0.030	0.027	0.023	0.019	0.016	0.014
70.0	0.075	0.055	0.038	0.034	0.029	0.024	0.020	0.017
80.0	0.086	0.066	0.044	0.040	0.034	0.028	0.023	0.019
90.0	0.095	0.072	0.050	0.046	0.039	0.032	0.026	0.021
100.0	0.097	0.074	0.052	0.048	0.040	0.033	0.027	0.022
110.0	0.092	0.067	0.045	0.041	0.034	0.027	0.021	0.017
120.0	0.085	0.060	0.038	0.034	0.027	0.020	0.015	0.011
130.0	0.076	0.051	0.030	0.026	0.020	0.014	0.009	0.005
140.0	0.065	0.040	0.019	0.015	0.010	0.005	0.001	0.000
150.0	0.052	0.027	0.006	0.002	0.000	0.000	0.000	0.000
160.0	0.038	0.013	0.000	0.000	0.000	0.000	0.000	0.000
170.0	0.025	0.000	0.000	0.000	0.000	0.000	0.000	0.000
180.0	0.011	0.000	0.000	0.000	0.000	0.000	0.000	0.000
190.0	0.004	0.000	0.000	0.000	0.000	0.000	0.000	0.000
200.0	0.002	0.000	0.000	0.000	0.000	0.000	0.000	0.000
210.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
220.0	0.004	0.000	0.000	0.000	0.000	0.000	0.000	0.000
230.0	0.006	0.000	0.000	0.000	0.000	0.000	0.000	0.000
240.0	0.009	0.000	0.000	0.000	0.000	0.000	0.000	0.000
250.0	0.013	0.000	0.000	0.000	0.000	0.000	0.000	0.000
260.0	0.016	0.000	0.000	0.000	0.000	0.000	0.000	0.000
270.0	0.019	0.000	0.000	0.000	0.000	0.000	0.000	0.000
280.0	0.022	0.000	0.000	0.000	0.000	0.000	0.000	0.000
290.0	0.025	0.000	0.000	0.000	0.000	0.000	0.000	0.000
300.0	0.028	0.000	0.000	0.000	0.000	0.000	0.000	0.000
310.0	0.032	0.000	0.000	0.000	0.000	0.000	0.000	0.000
320.0	0.035	0.000	0.000	0.000	0.000	0.000	0.000	0.000
330.0	0.038	0.000	0.000	0.000	0.000	0.000	0.000	0.000
340.0	0.040	0.000	0.000	0.000	0.000	0.000	0.000	0.000
350.0	0.042	0.000	0.000	0.000	0.000	0.000	0.000	0.000

TAP LOCATION (Z/L): TAP LOCATION (Z/D):	0.945 5.383	0.969 5.438	0.98 5.5	0.98 5.5	0.98 5.5	0.98 5.5	0.98 5.5	0.98 5.5
CIRCUMFERENTIAL ANGLE (PHI)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
10.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
20.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
30.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
40.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
50.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
60.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
70.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
80.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
90.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
100.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
110.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
120.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
130.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
140.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
150.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
160.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
170.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
180.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
190.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
200.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
210.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
220.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
230.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
240.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
250.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
260.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
270.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
280.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
290.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
300.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
310.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
320.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
330.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
340.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
350.0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

Figure A-10. (Cont'd)

APPENDIX B PLOTTED WIND TUNNEL TEST DATA

This appendix contains the measured pressure data in plotted format. Each set of plots relates to a specific model configuration and test condition with data for both the spinning and non-spinning cases presented on each plot. The appendix figures include the following data:

Figure	Rotating band	Angle of attack (deg)	Spin rate (rpm)
B1	OFF	0	0, 4900
B2	OFF	4	0, 4900
B3	OFF	10	0, 4900
B4	ON	0	0, 4900
B5	ON	10	0, 4900

Because of the computer format, some of the terms in Appendix B are different from those of the main report text. The following define these terms:

<u>Term</u>	<u>Symbol used in report text</u>
P-P STATIC	ΔP
C.P.	C_p
PHI	ϕ

ROTATING BAND = OFF
 PATCH NUMBER = .94
 ANGLE OF ATTACK (DEG) = 0

SYMBOL SPIN RATE (RPM)
 Δ 0
 O 1000

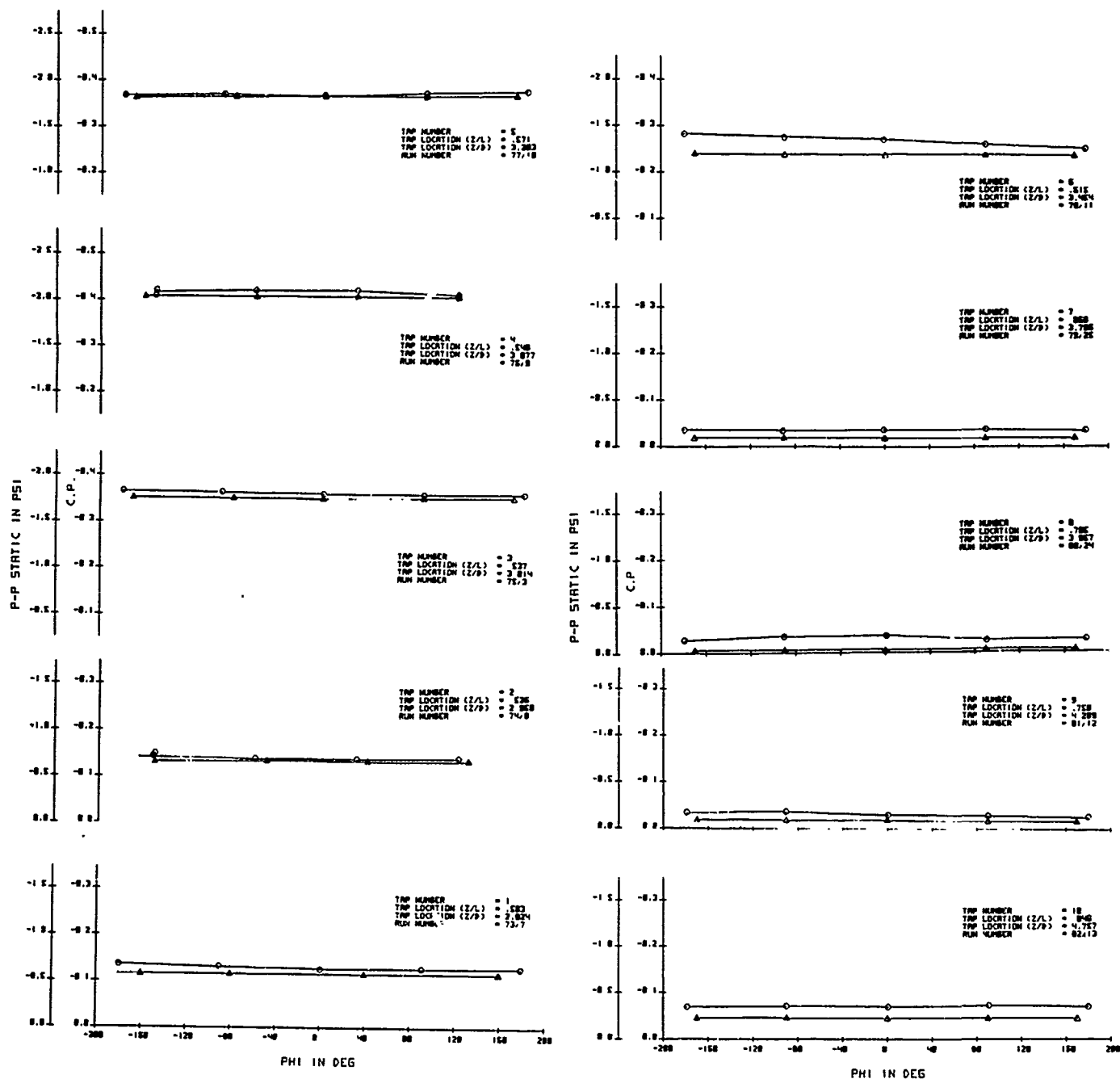


Figure B-1. Rotating Band Off, $\alpha = 0^\circ$

ROTATION SPEED = 0 FT
 HATCH NUMBER = 84
 NUMBER OF ATTACKS (PCS) = 8

SYMBOL
 Δ
 O
 SPIN RATE (RPM)
 8
 1000

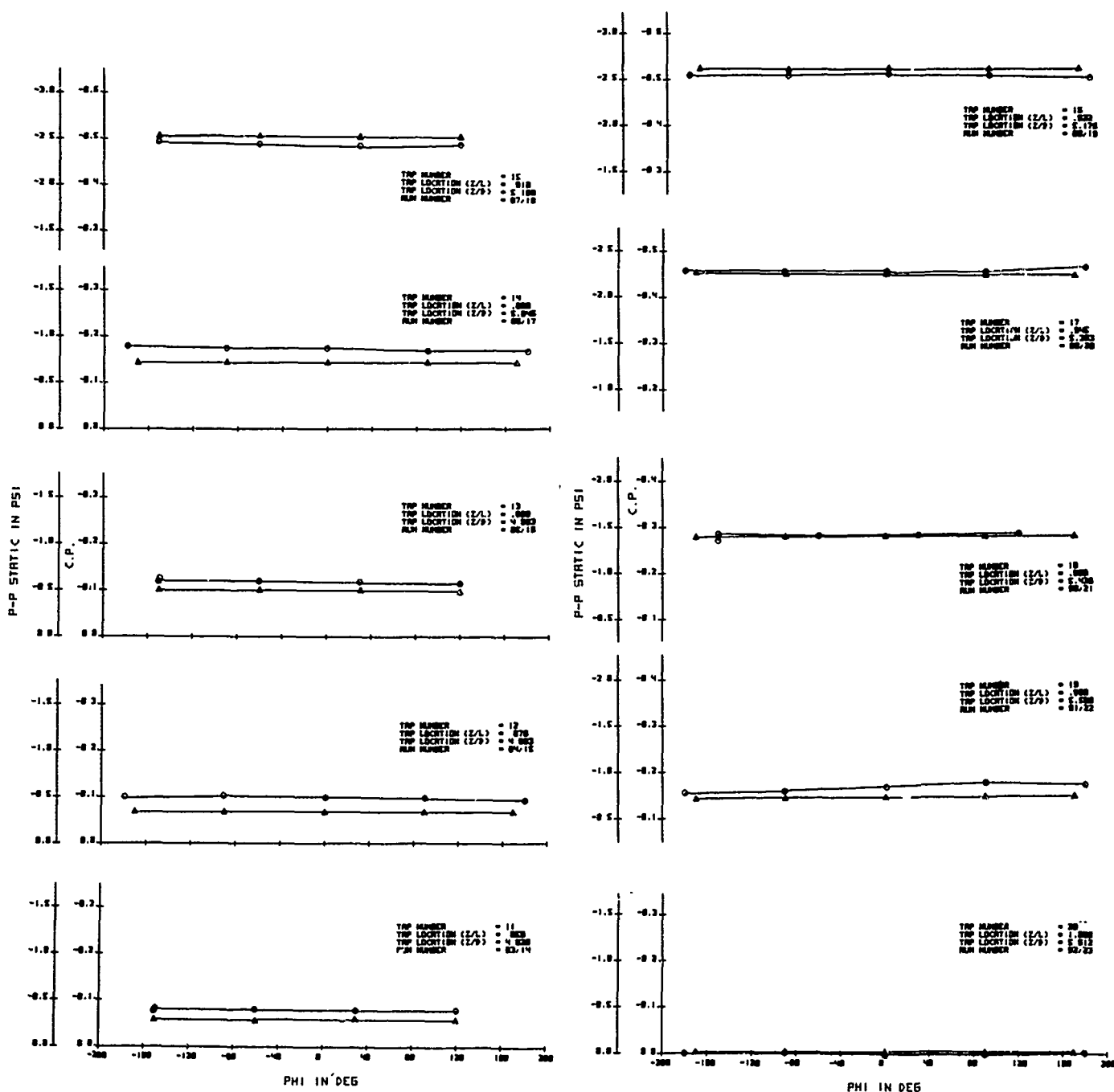


Figure B-1 (Continued)

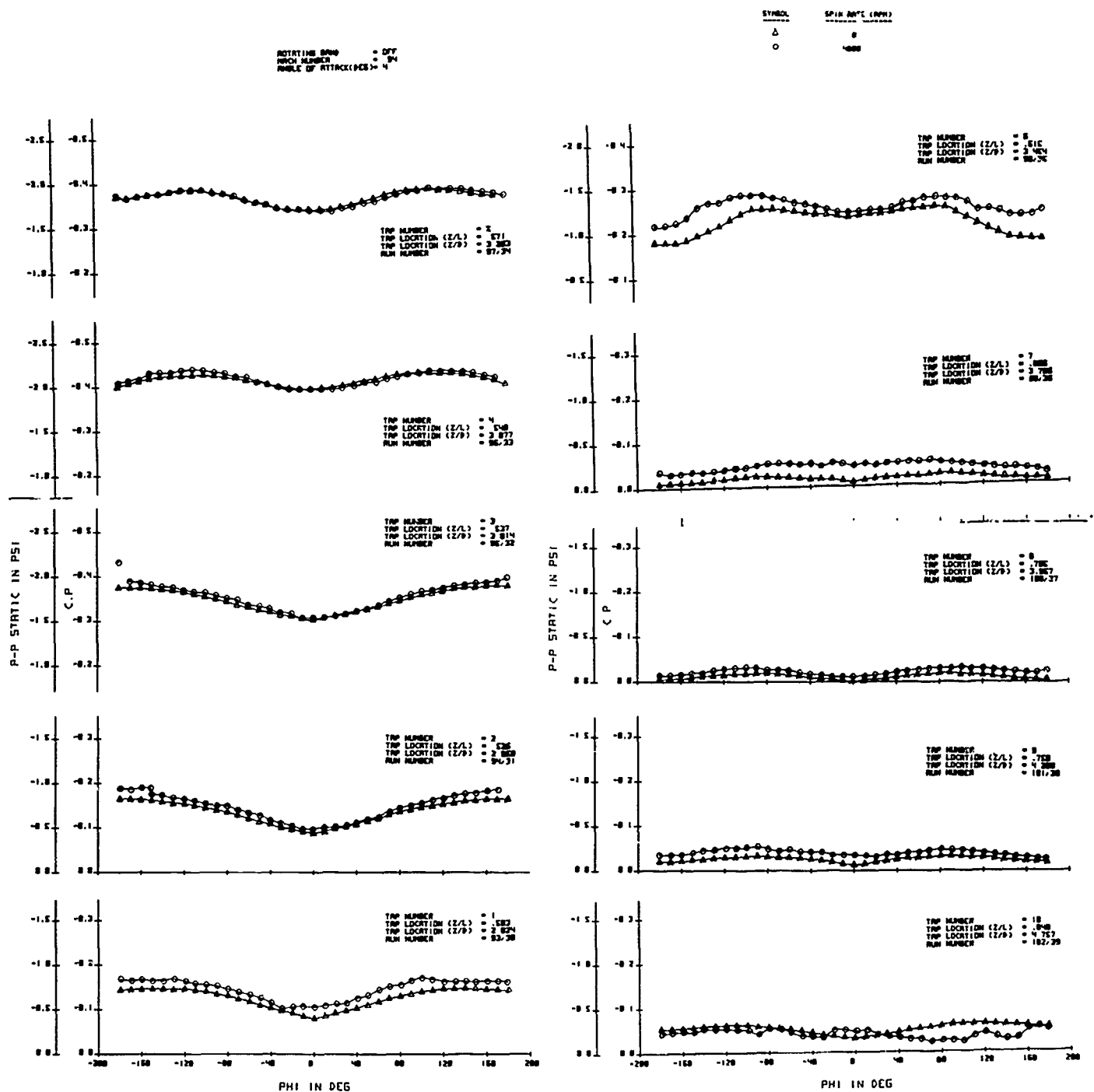


Figure B-2. Rotating Band Off, $\alpha = 4^\circ$

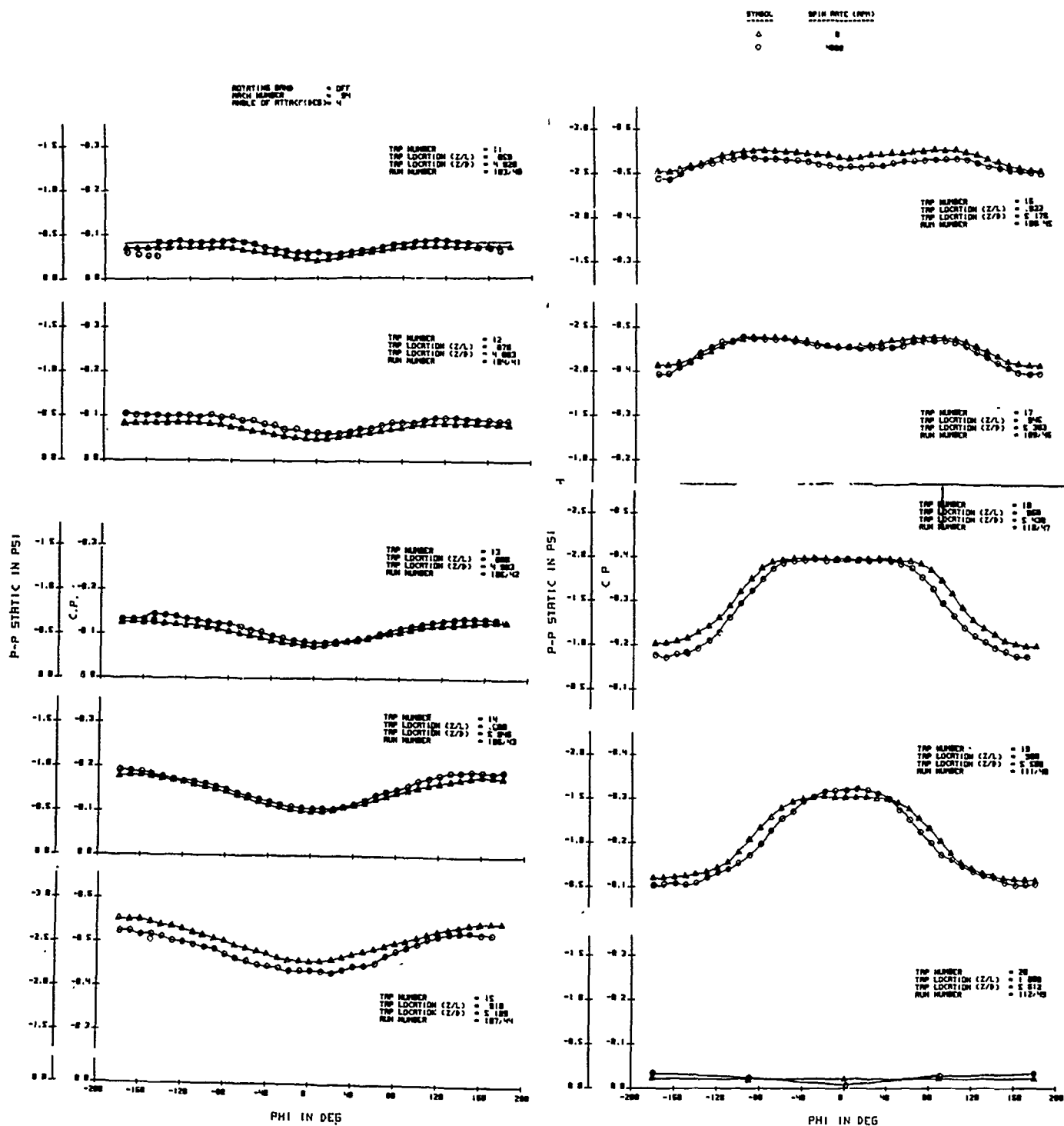


Figure B-2 (Continued)

TRIP NUMBER = 10
 PROFILE OF ATTITUDE (PSI) = 10

SYMBOL
 A
 O

SPIN RATE (RPM)
 0
 1000

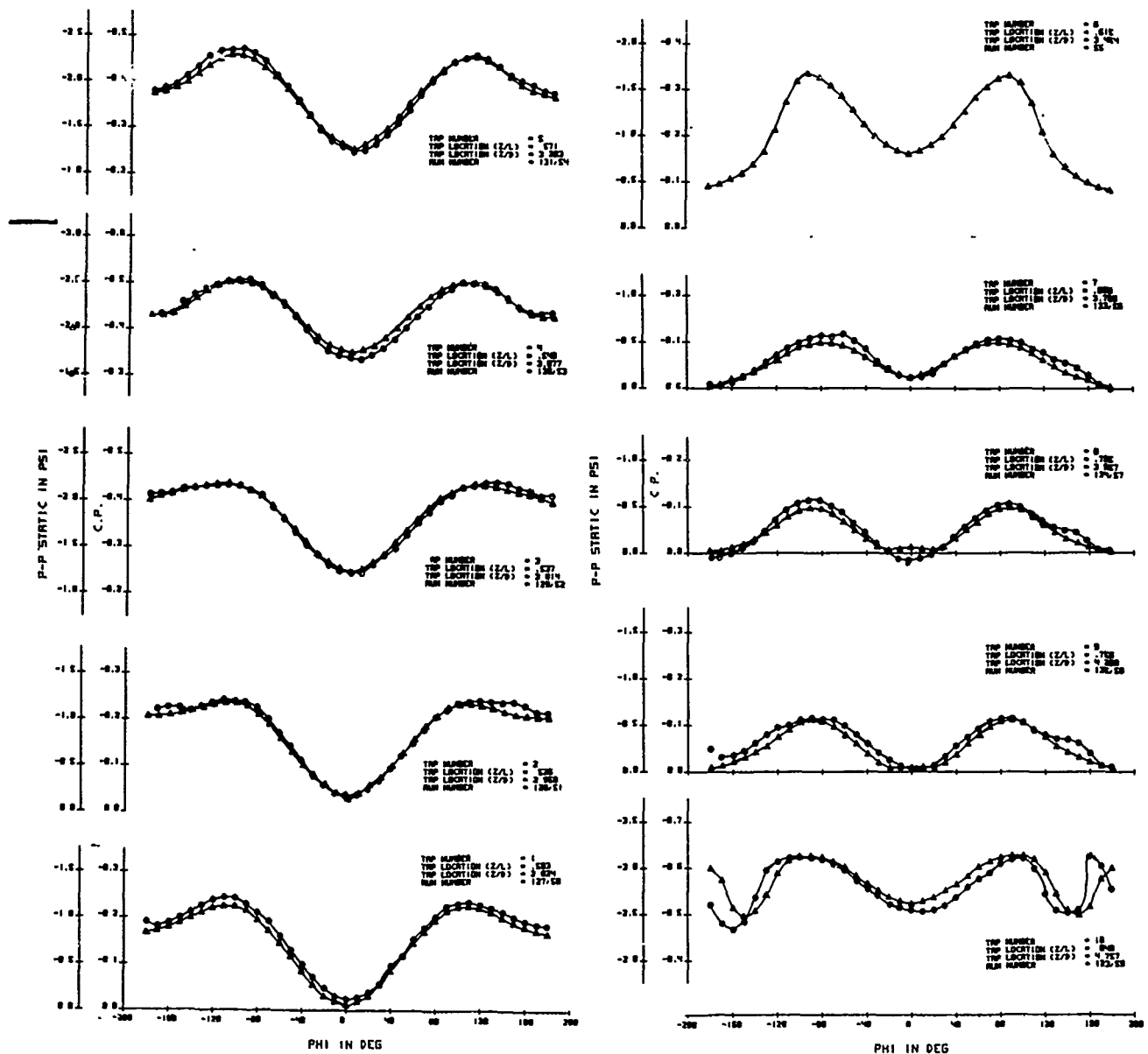


Figure B-3. Rotating Band Off, $\alpha = 10^\circ$

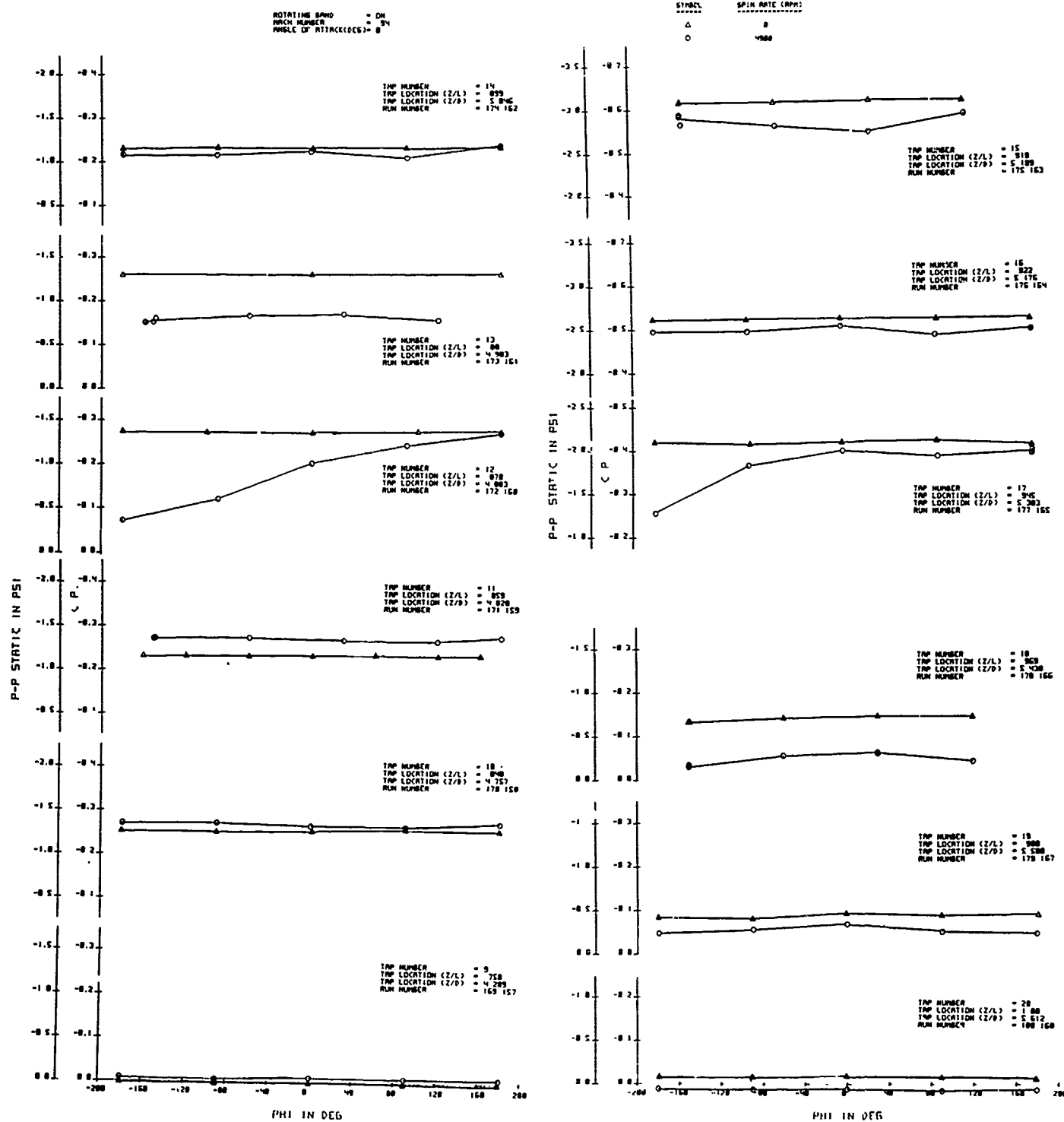


Figure B-4. Rotating Band On, $\alpha = 0^\circ$

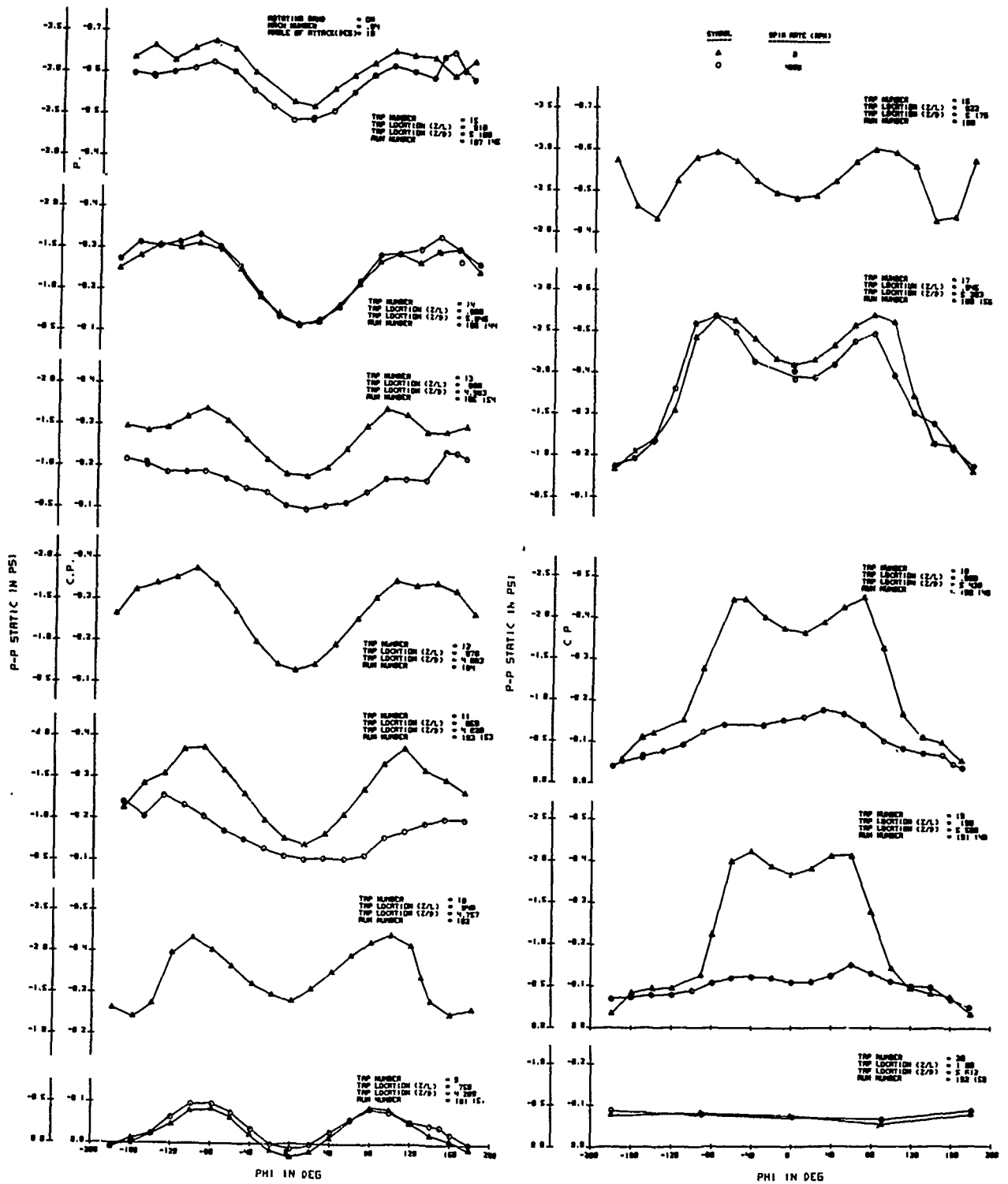


Figure B-5. Rotating Band On, $\alpha = 10^\circ$

APPENDIX C

FORCE AND MOMENT TERMS
COMPUTED FROM SURFACE PRESSURE DATA

This appendix contains both local and total force and moment coefficients and related terms as computed from the measured surface pressure data. Each set of data relates to a specific model configuration and test condition as follows:

Figure	Rotating band	Angle of attack (deg)	Spin rate (rpm)
C1	OFF	0	0
C2	OFF	0	4900
C3	OFF	4	0
C4	OFF	4	4900
C5	OFF	10	0
C6	OFF	10	4900
C7	ON	0	0
C8	ON	0	4900
C9	ON	10	0
C10	ON	10	4900

These data indicate the total coefficient values as well as the contribution to the coefficient values due to the nose, cylinder, and boattail portions of model where:

<u>Portion</u>	<u>Region (Z/L)</u>
nose	0 to .537
cylinder	.537 to .910
boattail	.910 to 1.00

The terms are listed for the longitudinal location at which they were computed. Because of the computer format, some of the terms are different from those in the main report text. The following define these terms:

<u>Terms</u>	<u>Symbol used in report text</u>	<u>Definition (if not in report text)</u>
XCG/L	X_{cg}/L	
ZI/L	Z_i/L	
ZI	Z_i	
DZI	ΔZ_i	
DIA	d_i	Diameter of model at Z_i
CNI LOCAL	C_N	Local normal force coefficient normal to local surface
CN	C_{N_i}	Local normal force coefficient normal to longitudinal (Z) axis
C SUM	$\sum C_{N_i}$	Summation of local normal force coefficients from nose
CM	C_{M_i}	Local pitching moment coefficient
CYI LOCAL	C_{Y_i}	Local side (Magnus) force coef- ficient normal to local surface
CY SUM	$\sum C_Y$	Summation of local side (Magnus) force coefficients from nose
Cn	C_{n_i}	Local yawing (Magnus) moment coefficient
NORMAL FORCE COEFFICIENT	C_N	Total normal force coefficient
PITCHING MOMENT COEFFICIENT (NOSE)	C_M	Total pitching moment Coefficient referred to tip of nose ($Z/L = 0$)
PITCHING MOMENT COEFFICIENT (CG)		Total pitching moment coefficient referred to Ref C.G. ($Z/L = .625$)
NORMAL FORCE COEFFICIENT (NOSE)		Normal force coefficient due to nose portion of model
PITCHING MOMENT COEFFICIENT (NOSE) (NOSE)		Pitching moment coefficient due to nose portion of model referred to tip of nose ($Z/L = 0$)

PITCHING MOMENT
COEFFICIENT
(CG) (NOSE)

Pitching moment coefficient due
to nose portion of model referred
to Ref C.G. ($Z/L = .625$)

NORMAL FORCE
COEFFICIENT
(CYL)

Normal force coefficient due to
cylindrical portion of model

PITCHING MOMENT
COEFFICIENT
(CYL) (NOSE)

Pitching moment coefficient due
to cylindrical portion of model
referred to tip of nose ($Z/L = 0$)

PITCHING MOMENT
COEFFICIENT
(CG) (CYL)

Pitching moment coefficient due
to cylindrical portion of model
referred to Ref C.G. ($Z/L = .625$)

NORMAL FORCE
COEFFICIENT
(BT)

Normal force coefficient due to
boattail portion of model

PITCHING MOMENT
COEFFICIENT
(NOSE) (BT)

Pitching moment coefficient due
to boattail portion of model
referred to tip of nose ($Z/L = 0$)

PITCHING MOMENT
COEFFICIENT
(CG) (BT)

Pitching moment coefficient due
to boattail portion of model
referred to Ref C.G. ($Z/L = .625$)

REF. LENGTH (L):
REF. DIAMETER (D):
ROTATING BAND:
MACH NO.:
ANGLE OF ATTACK (ALPHA):
SPIN RATE (P):
TIP SPEED RATIO (PD/2V):
X CG/L

[illegible][illegible]

Figure C-1. Rotating Band Off, $\alpha = 0^\circ$ P = 0 rpm

REF. LENGTH (L):
REF. DIAMETER (D):
ROTATING BAND:
TACH NO.:
ANGLE OF ATTACK (ALPHA):
RPM IN RATE (P):
LIP SPEED RATIO (PD/2V):
CG/L

[illegible][illegible]

Figure C-2. Rotating Band Off, $\alpha = 0^\circ$, $P = 4900$ rpm

REF. LENGTH (L):
REF. DIAMETER (D):
ROTATING BAND:
MACH NO.:
ANGLE OF ATTACK (ALPHA):
SPIN RATE (P):
TIP SPEED RATIO (PD/2V):
X CG/L

	Z1/L	Z1/L (IN)	Z1/L (IN)	CM	CN	CN SUM	CNI LOCAL	DIA. (IN)	D21 (IN)	LOCAL	CY	CY SUM	CM
NORMAL	0.070	3.123	5.130	0.072	0.0168	0.0168	0.0168	0.070	3.123	0.00500	0.00500	0.00500	0.00500
PITCHING	0.160	7.139	4.685	0.0249	0.0014	0.0014	0.0014	0.160	7.139	0.00500	0.00500	0.00500	0.00500
PITCHING	0.260	12.492	5.354	0.0342	0.0032	0.0032	0.0032	0.260	12.492	0.00500	0.00500	0.00500	0.00500
PITCHING	0.400	17.446	6.332	0.0392	0.0052	0.0052	0.0052	0.400	17.446	0.00500	0.00500	0.00500	0.00500
PITCHING	0.500	22.449	6.763	0.0438	0.0072	0.0072	0.0072	0.500	22.449	0.00500	0.00500	0.00500	0.00500
PITCHING	0.600	27.450	6.971	0.0486	0.0094	0.0094	0.0094	0.600	27.450	0.00500	0.00500	0.00500	0.00500
PITCHING	0.700	32.450	6.971	0.0537	0.0130	0.0130	0.0130	0.700	32.450	0.00500	0.00500	0.00500	0.00500
PITCHING	0.800	37.461	6.756	0.0586	0.0166	0.0166	0.0166	0.800	37.461	0.00500	0.00500	0.00500	0.00500
PITCHING	0.900	42.461	6.356	0.0635	0.0204	0.0204	0.0204	0.900	42.461	0.00500	0.00500	0.00500	0.00500
PITCHING	1.000	47.461	5.500	0.0684	0.0243	0.0243	0.0243	1.000	47.461	0.00500	0.00500	0.00500	0.00500
PITCHING	1.100	52.461	4.246	0.0732	0.0283	0.0283	0.0283	1.100	52.461	0.00500	0.00500	0.00500	0.00500
PITCHING	1.200	57.461	2.800	0.0779	0.0323	0.0323	0.0323	1.200	57.461	0.00500	0.00500	0.00500	0.00500
PITCHING	1.300	62.461	1.300	0.0823	0.0363	0.0363	0.0363	1.300	62.461	0.00500	0.00500	0.00500	0.00500
PITCHING	1.400	67.461	0.000	0.0866	0.0404	0.0404	0.0404	1.400	67.461	0.00500	0.00500	0.00500	0.00500
PITCHING	1.500	72.461	0.000	0.0908	0.0445	0.0445	0.0445	1.500	72.461	0.00500	0.00500	0.00500	0.00500
PITCHING	1.600	77.461	0.000	0.0949	0.0485	0.0485	0.0485	1.600	77.461	0.00500	0.00500	0.00500	0.00500
PITCHING	1.700	82.461	0.000	0.0989	0.0525	0.0525	0.0525	1.700	82.461	0.00500	0.00500	0.00500	0.00500
PITCHING	1.800	87.461	0.000	0.1028	0.0565	0.0565	0.0565	1.800	87.461	0.00500	0.00500	0.00500	0.00500
PITCHING	1.900	92.461	0.000	0.1067	0.0605	0.0605	0.0605	1.900	92.461	0.00500	0.00500	0.00500	0.00500
PITCHING	2.000	97.461	0.000	0.1105	0.0645	0.0645	0.0645	2.000	97.461	0.00500	0.00500	0.00500	0.00500
PITCHING	2.100	102.461	0.000	0.1143	0.0684	0.0684	0.0684	2.100	102.461	0.00500	0.00500	0.00500	0.00500
PITCHING	2.200	107.461	0.000	0.1181	0.0723	0.0723	0.0723	2.200	107.461	0.00500	0.00500	0.00500	0.00500
PITCHING	2.300	112.461	0.000	0.1219	0.0762	0.0762	0.0762	2.300	112.461	0.00500	0.00500	0.00500	0.00500
PITCHING	2.400	117.461	0.000	0.1257	0.0801	0.0801	0.0801	2.400	117.461	0.00500	0.00500	0.00500	0.00500
PITCHING	2.500	122.461	0.000	0.1295	0.0840	0.0840	0.0840	2.500	122.461	0.00500	0.00500	0.00500	0.00500
PITCHING	2.600	127.461	0.000	0.1									

Figure C-3. Rotating Band Off, $\alpha = 4^\circ$, $\beta = 0$ rpm

REF. LENGTH (L): 44.616 IN. ROTATING BAND: 7.95 IN. MACH NO.: 0.94 ANGLE OF ATTACK (ALPHA): 4 DEG. SPIN RATE (RPM): 4900 REV/MIN TIP SPEED RATIO (PD/2V): 0.162027427 X CC/L: 0.625112867									
ZI/L	ZI	DIA.	CH	CH	ZI/L	ZI	DIA.	CH	CH
*****	(IN)	(IN)	*****	*****	*****	(IN)	(IN)	*****	*****
0.070	3.123	2.125	0.0168	0.0168	0.070	3.123	2.125	0.0168	0.0168
0.160	7.139	4.685	0.0246	0.0246	0.160	7.139	4.685	0.0246	0.0246
0.280	12.492	5.334	0.0339	0.0339	0.280	12.492	5.334	0.0339	0.0339
0.400	17.846	4.988	0.0419	0.0419	0.400	17.846	4.988	0.0419	0.0419
0.500	22.308	2.362	0.0503	0.0503	0.500	22.308	2.362	0.0503	0.0503
0.593	22.449	0.571	0.0571	0.0571	0.593	22.449	0.571	0.0571	0.0571
0.626	23.450	0.756	0.0605	0.0605	0.626	23.450	0.756	0.0605	0.0605
0.637	23.961	0.793	0.0637	0.0637	0.637	23.961	0.793	0.0637	0.0637
0.648	24.461	0.793	0.0648	0.0648	0.648	24.461	0.793	0.0648	0.0648
0.659	24.961	0.793	0.0659	0.0659	0.659	24.961	0.793	0.0659	0.0659
0.670	25.461	0.793	0.0670	0.0670	0.670	25.461	0.793	0.0670	0.0670
0.681	25.961	0.793	0.0681	0.0681	0.681	25.961	0.793	0.0681	0.0681
0.692	26.461	0.793	0.0692	0.0692	0.692	26.461	0.793	0.0692	0.0692
0.703	26.961	0.793	0.0703	0.0703	0.703	26.961	0.793	0.0703	0.0703
0.714	27.461	0.793	0.0714	0.0714	0.714	27.461	0.793	0.0714	0.0714
0.725	27.961	0.793	0.0725	0.0725	0.725	27.961	0.793	0.0725	0.0725
0.736	28.461	0.793	0.0736	0.0736	0.736	28.461	0.793	0.0736	0.0736
0.747	28.961	0.793	0.0747	0.0747	0.747	28.961	0.793	0.0747	0.0747
0.758	29.461	0.793	0.0758	0.0758	0.758	29.461	0.793	0.0758	0.0758
0.769	29.961	0.793	0.0769	0.0769	0.769	29.961	0.793	0.0769	0.0769
0.780	30.461	0.793	0.0780	0.0780	0.780	30.461	0.793	0.0780	0.0780
0.791	30.961	0.793	0.0791	0.0791	0.791	30.961	0.793	0.0791	0.0791
0.802	31.461	0.793	0.0802	0.0802	0.802	31.461	0.793	0.0802	0.0802
0.813	31.961	0.793	0.0813	0.0813	0.813	31.961	0.793	0.0813	0.0813
0.824	32.461	0.793	0.0824	0.0824	0.824	32.461	0.793	0.0824	0.0824
0.835	32.961	0.793	0.0835	0.0835	0.835	32.961	0.793	0.0835	0.0835
0.846	33.461	0.793	0.0846	0.0846	0.846	33.461	0.793	0.0846	0.0846
0.857	33.961	0.793	0.0857	0.0857	0.857	33.961	0.793	0.0857	0.0857
0.868	34.461	0.793	0.0868	0.0868	0.868	34.461	0.793	0.0868	0.0868
0.879	34.961	0.793	0.0879	0.0879	0.879	34.961	0.793	0.0879	0.0879
0.890	35.461	0.793	0.0890	0.0890	0.890	35.461	0.793	0.0890	0.0890
0.901	35.961	0.793	0.0901	0.0901	0.901	35.961	0.793	0.0901	0.0901
0.912	36.461	0.793	0.0912	0.0912	0.912	36.461	0.793	0.0912	0.0912
0.923	36.961	0.793	0.0923	0.0923	0.923	36.961	0.793	0.0923	0.0923
0.934	37.461	0.793	0.0934	0.0934	0.934	37.461	0.793	0.0934	0.0934
0.945	37.961	0.793	0.0945	0.0945	0.945	37.961	0.793	0.0945	0.0945
0.956	38.461	0.793	0.0956	0.0956	0.956	38.461	0.793	0.0956	0.0956
0.967	38.961	0.793	0.0967	0.0967	0.967	38.961	0.793	0.0967	0.0967
0.978	39.461	0.793	0.0978	0.0978	0.978	39.461	0.793	0.0978	0.0978
0.989	39.961	0.793	0.0989	0.0989	0.989	39.961	0.793	0.0989	0.0989
0.990	40.461	0.793	0.0990	0.0990	0.990	40.461	0.793	0.0990	0.0990
0.991	40.961	0.793	0.0991	0.0991	0.991	40.961	0.793	0.0991	0.0991
0.992	41.461	0.793	0.0992	0.0992	0.992	41.461	0.793	0.0992	0.0992
0.993	41.961	0.793	0.0993	0.0993	0.993	41.961	0.793	0.0993	0.0993
0.994	42.461	0.793	0.0994	0.0994	0.994	42.461	0.793	0.0994	0.0994
0.995	42.961	0.793	0.0995	0.0995	0.995	42.961	0.793	0.0995	0.0995
0.996	43.461	0.793	0.0996	0.0996	0.996	43.461	0.793	0.0996	0.0996
0.997	43.961	0.793	0.0997	0.0997	0.997	43.961	0.793	0.0997	0.0997
0.998	44.461	0.793	0.0998	0.0998	0.998	44.461	0.793	0.0998	0.0998
0.999	44.961	0.793	0.0999	0.0999	0.999	44.961	0.793	0.0999	0.0999
1.000	45.461	0.793	0.0999	0.0999	1.000	45.461	0.793	0.0999	0.0999

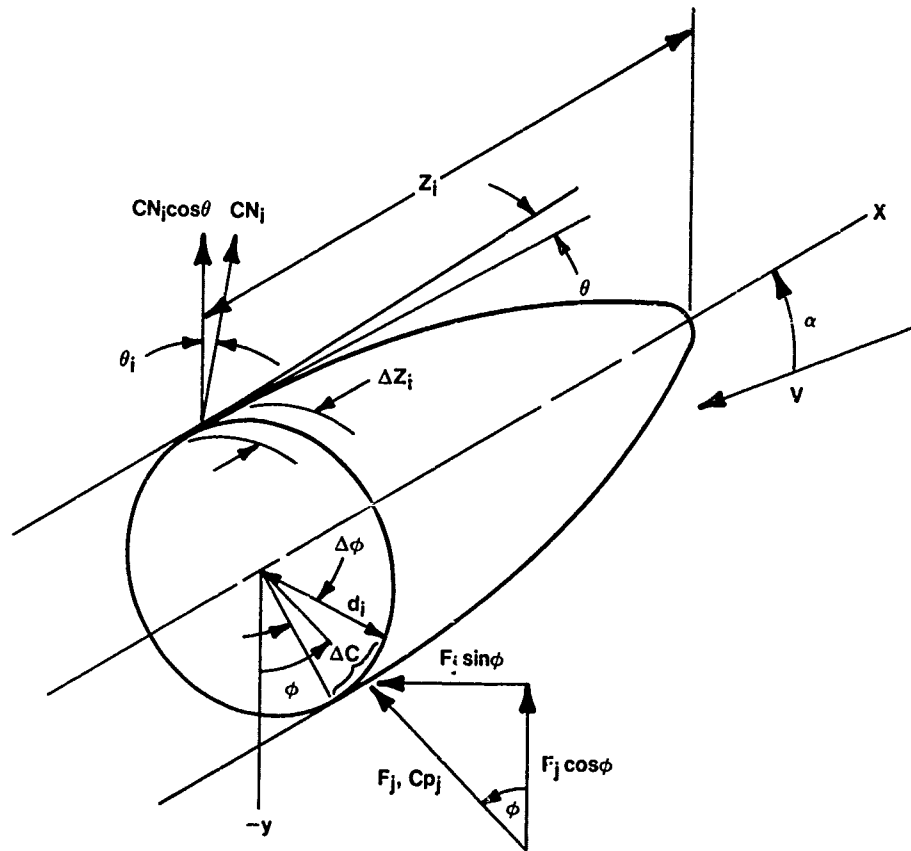
Figure C-4. Rotating Band Off, $\alpha = 4^\circ$, $P = 4900$ rpm

Figure C-7. Rotating Band On, $\alpha = 0^\circ$, $p = 0$ rpm

Figure C-9. Rotating Band On, $\alpha = 10^\circ$, $P = 0^\circ$ rpm

The following are derivations of selected data reduction terms included in Appendix C.

1. Derivation of Local Force and Moment Coefficient:



At pressure tap location Z_i : $\Delta P_j = C_{p_j} q$

$$F_j = C_{p_j} q S_j$$

$$q = \frac{\rho v^2}{2}$$

$$S_j = \Delta C \Delta Z_i$$

$$\Delta C = \frac{d_i}{2} \sin \Delta \phi$$

$$S_j = \frac{d_i}{2} \Delta Z_i \sin \Delta \phi$$

$$F_j = C_{p_j} q \frac{d_i}{2} \Delta Z_i \sin \Delta \phi$$

$$N_i = \sum_{j=1}^{360/\Delta\phi} F_j \cos \phi_j$$

$$N_i = \sum_{j=1}^{360/\Delta\phi} C_{p_j} q \frac{d_i}{2} \Delta Z_i \sin \Delta\phi \cos \phi_j$$

$$C_{N_i} = \frac{N_i}{qs}$$

$$S = \frac{\pi d^2}{4}$$

$$C_{N_i} = \sum_{j=1}^{360/\Delta\phi} \frac{2 C_{p_j} d_i \Delta Z_i \sin \Delta\phi \cos \phi_j}{\pi d^2}$$

$$C_{N_i} = \frac{2 d_i \Delta Z_i \sin \Delta\phi}{\pi d^2} \sum_{j=1}^{360/\Delta\phi} C_{p_j} \cos \phi_j$$

similarly:

$$C_{y_i} = \frac{2 d_i \Delta Z_i \sin \Delta\phi}{\pi d^2} \sum_{j=1}^{360/\Delta\phi} C_{p_j} \sin \phi_j$$

$$\Delta\phi = 10^\circ$$

$$j = 1 \longrightarrow 36$$

$$C_N = \sum_{i=1}^{27} C_{N_i} \Delta Z_i \cos \theta_i$$

For this report, $i = 1 \longrightarrow 27$ includes data from the 19 tap locations used in the Ames test model, plus data from 8 ogive locations obtained in reference 7.

where:

$$\Delta Z_i = \frac{Z_{i+1} - Z_i}{2} + \frac{Z_i - Z_{i-1}}{2}$$

$$\Delta Z_i = \frac{Z_{i+1} - Z_{i-1}}{2}$$

$$\text{@ } Z_i = 1 \quad Z_{i-1} = L - Z_{i-1}$$

$$\text{@ } Z_i = 27 \quad Z_{i+1} = L$$

similarly:

$$C_y = \sum_{i=1}^{27} C_{y_i} \Delta Z_i \cos \theta$$

$$M_i = N_i Z_i$$

$$M_i = \sum_{j=1}^{360/\Delta\phi} F_j Z_i \cos \phi_j$$

$$M_i = \sum_{j=1}^{360/\Delta\phi} C_{p_j} q \frac{d_i}{2} \Delta Z_i \sin \Delta\phi Z_i \cos \phi_j$$

$$C_{m_i} = \frac{M_i}{qsd}$$

$$S = \frac{\pi d^2}{4}$$

$$C_{m_i} = \sum_{j=1}^{360/\Delta\phi} \frac{2 C_{p_j} d_i \Delta Z_i Z_i \sin \Delta\phi \cos \phi_j}{\pi d^3}$$

$$C_{m_i} = \frac{2 d_i \Delta Z_i Z_i \sin \Delta\phi}{\pi d^3} \sum_{j=1}^{360/\Delta\phi} C_{p_j} \cos \phi_j$$

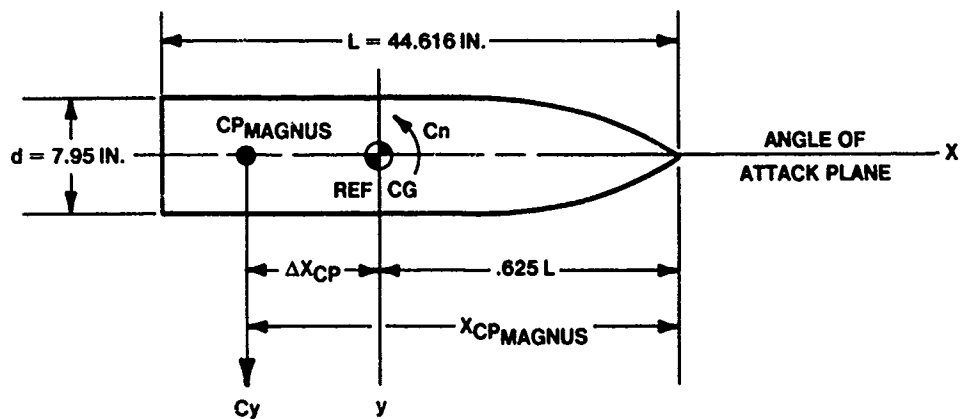
similarly:

$$C_{n_i} = \frac{2 d_i \Delta Z_i Z_i \sin \Delta\phi}{\pi d^3} \sum_{j=1}^{360/\Delta\phi} C_{p_j} \sin \phi_j$$

$$C_{m_{nose}} = \sum_{i=1}^{27} C_{m_i} \Delta Z_i$$

$$C_{n_{nose}} = \sum_{i=1}^{27} C_{n_i} \Delta Z_i$$

2. Derivation of Normal Force and Magnus Force Centers of Pressure Locations:



$$X_{CP \text{ MAGNUS}} = \Delta X_{CP \text{ MAGNUS}} + .625 L$$

$$\frac{X_{CP \text{ MAGNUS}}}{L} = \frac{\Delta X_{CP \text{ MAGNUS}}}{L} + .625$$

$$\frac{X_{CP \text{ MAGNUS}}}{L} = \frac{\Delta X_{CP \text{ MAGNUS}}}{L} \cdot \frac{d}{L} + .625$$

$$\frac{X_{CP \text{ MAGNUS}}}{L} = .1782 \frac{\Delta X_{CP \text{ MAGNUS}}}{d} + .625$$

$$\frac{\Delta X_{CP \text{ MAGNUS}}}{d} = \frac{C_{n_p}}{C_{y_p}}$$

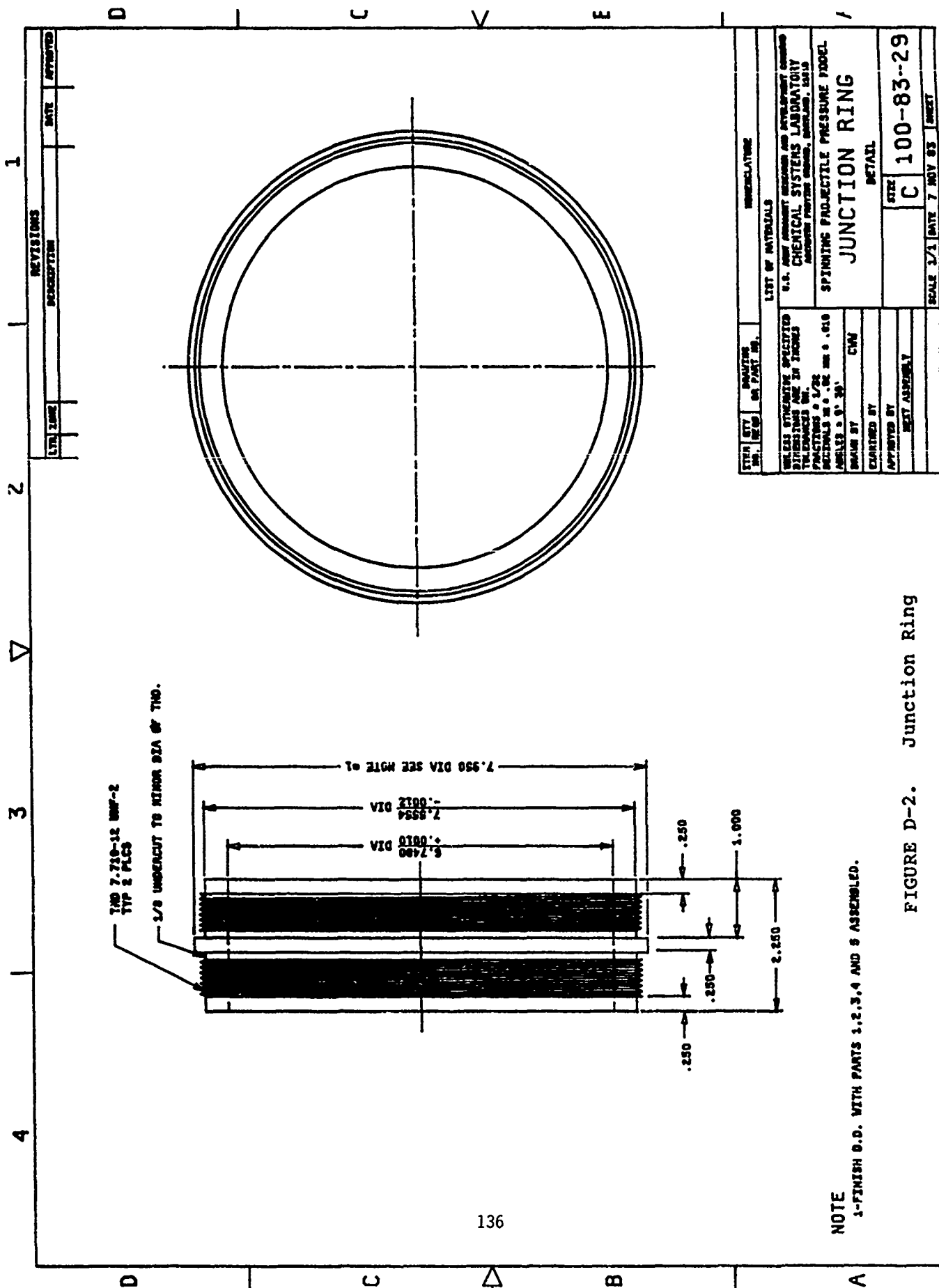
$$\frac{X_{CP \text{ MAGNUS}}}{L} = .625 + .1782 \frac{C_{n_p}}{C_{y_p}}$$

APPENDIX D
ENGINEERING DRAWINGS OF WIND
TUNNEL MODEL COMPONENTS

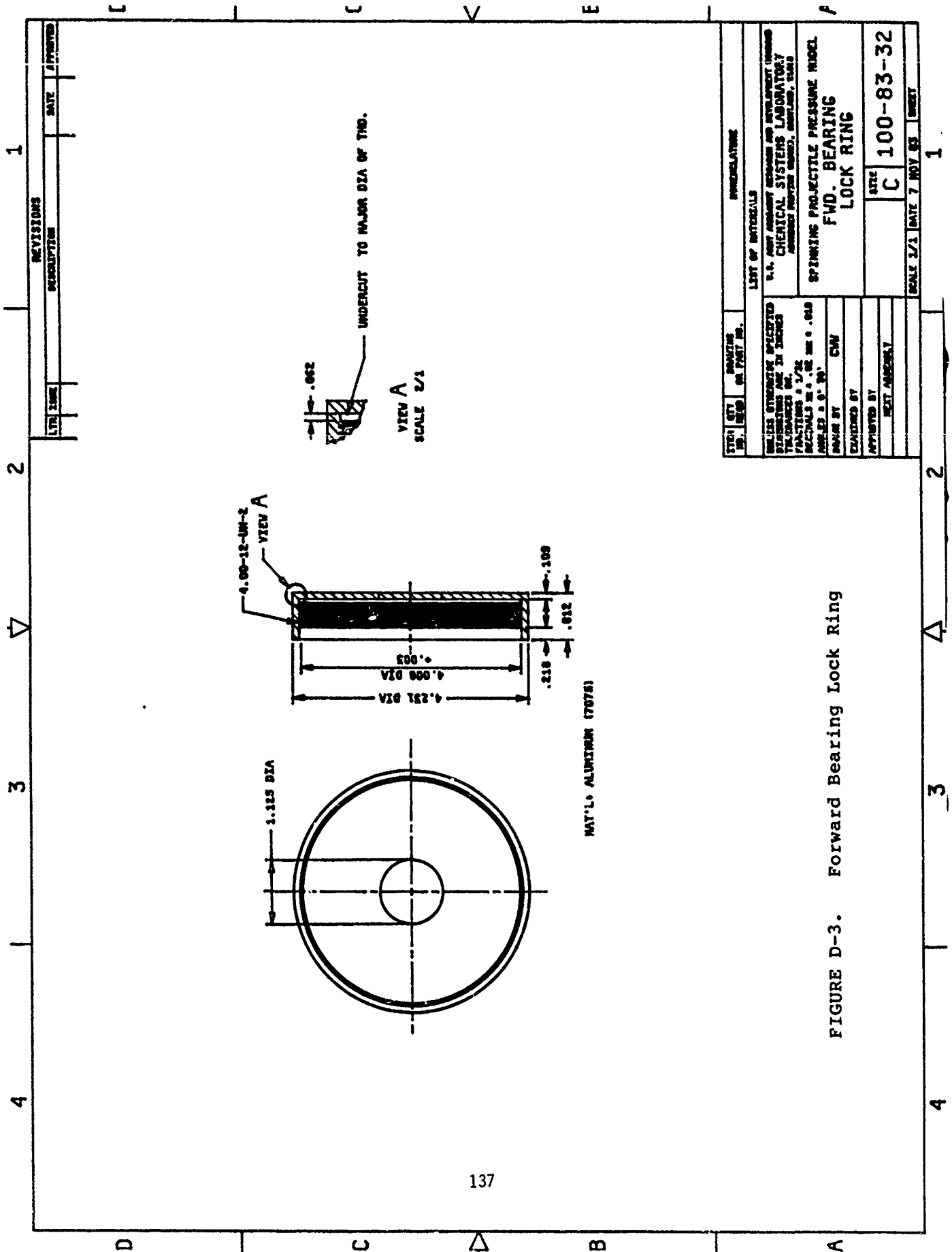
Appendix D contains the engineering drawings of the model and sting components, including an assembly drawing.

Figure

- | | |
|------|---|
| D-1 | Nose |
| D-2 | Junction Ring |
| D-3 | Forward Bearing Lock Ring |
| D-4 | Aft Bearing Lock Ring |
| D-5 | Drive Shaft |
| D-6 | Armature Adapter Lock Nut |
| D-7 | Motor Drive Adapter |
| D-8 | Motor Lock Screw |
| D-9 | Strut Nut |
| D-10 | Core/Sting Lock Pin |
| D-11 | Forward Ogive |
| D-12 | Tail Section, Version A (Rotating Band Off) |
| D-13 | Forward Core Motor/Bearing Support Section |
| D-14 | Strut |
| D-15 | Aft Core Section |
| D-16 | Spinning Projectile Pressure Model Assembly |
| D-17 | Mid Section |
| D-18 | Tail Section, Version B (Rotating Band On) |
| D-19 | Main Core Section (View 1) |
| D-20 | Main Core Section (View 2) |

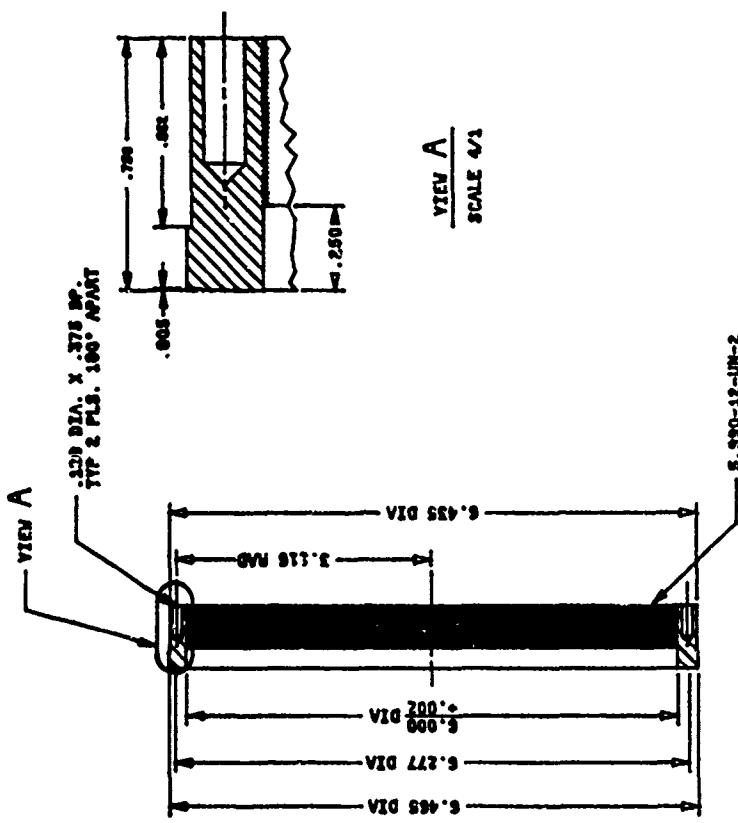


NOTE
1-FINISH D.P. WITH PARTS 1.2,3,4 AND 5 ASSEMBLED.



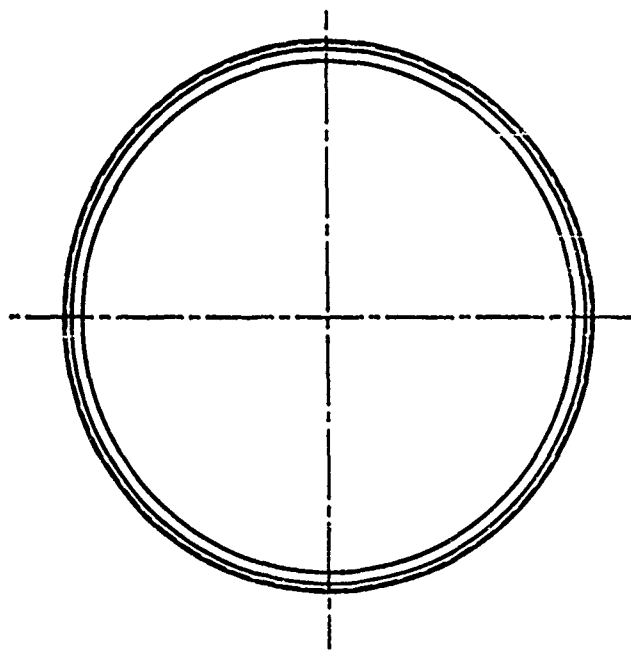
4 3 2 1

REVISIONS		
DATE	DESCRIPTION	APPROVED



VIEW A
SCALE 4/1

MAT'L: ALUMINUM (7075)



138

ITEM	QTY	DESCRIPTION	REMARKS

LIST OF MATERIALS	
UNLESS OTHERWISE SPECIFIED	U.S. GOVT. PROPERTY AND INVENTION RIGHTS
DIMENSIONS ARE IN INCHES	CHEMICAL SYSTEMS LABORATORY
TOLERANCES ARE:	PRECISION PARTS DIVISION, BIRMINGHAM, ALABAMA
FRACTIONS ± 1/32	
DECIMALS TO 0.0005 ± 0.0005	
ANGLES ± 0° 30'	
DRAWN BY	CW
EXAMINED BY	
APPROVED BY	
TEST ASSEMBLY	

DATE	DATE	SCALE	100-83-35
C	7 NOV 83	3/1	1

FIGURE D-4. Aft Bearing Lock Ring

4 3 2 1

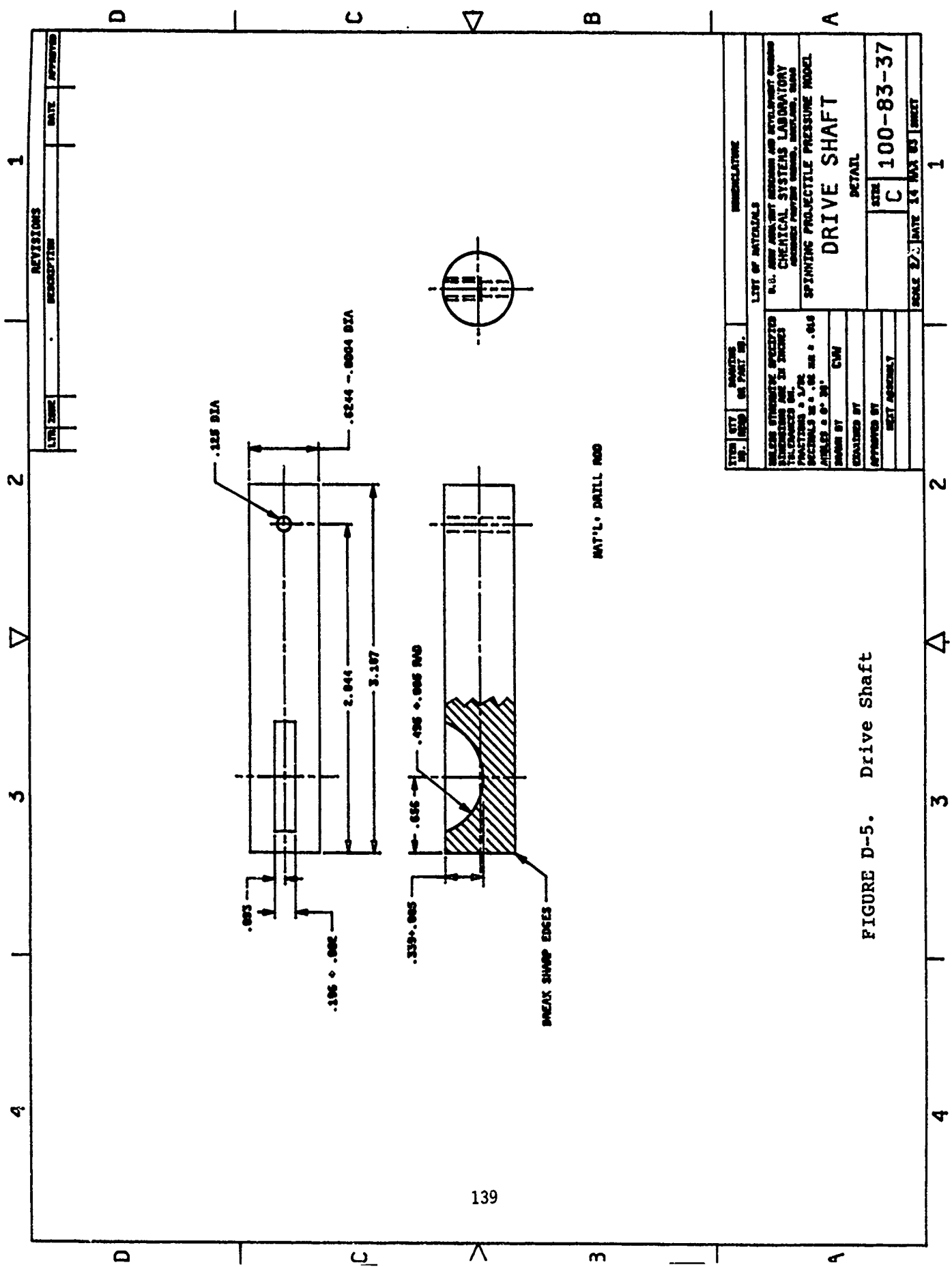


FIGURE D-5. Drive Shaft

ITEM	QTY	DESCRIPTION	REVISIONS
1	1	DRIVE SHAFT	
2	1	DRIVE SHAFT	
3	1	DRIVE SHAFT	
4	1	DRIVE SHAFT	
5	1	DRIVE SHAFT	
6	1	DRIVE SHAFT	
7	1	DRIVE SHAFT	
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10	1	DRIVE SHAFT	
11	1	DRIVE SHAFT	
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99	1	DRIVE SHAFT	
100	1	DRIVE SHAFT	

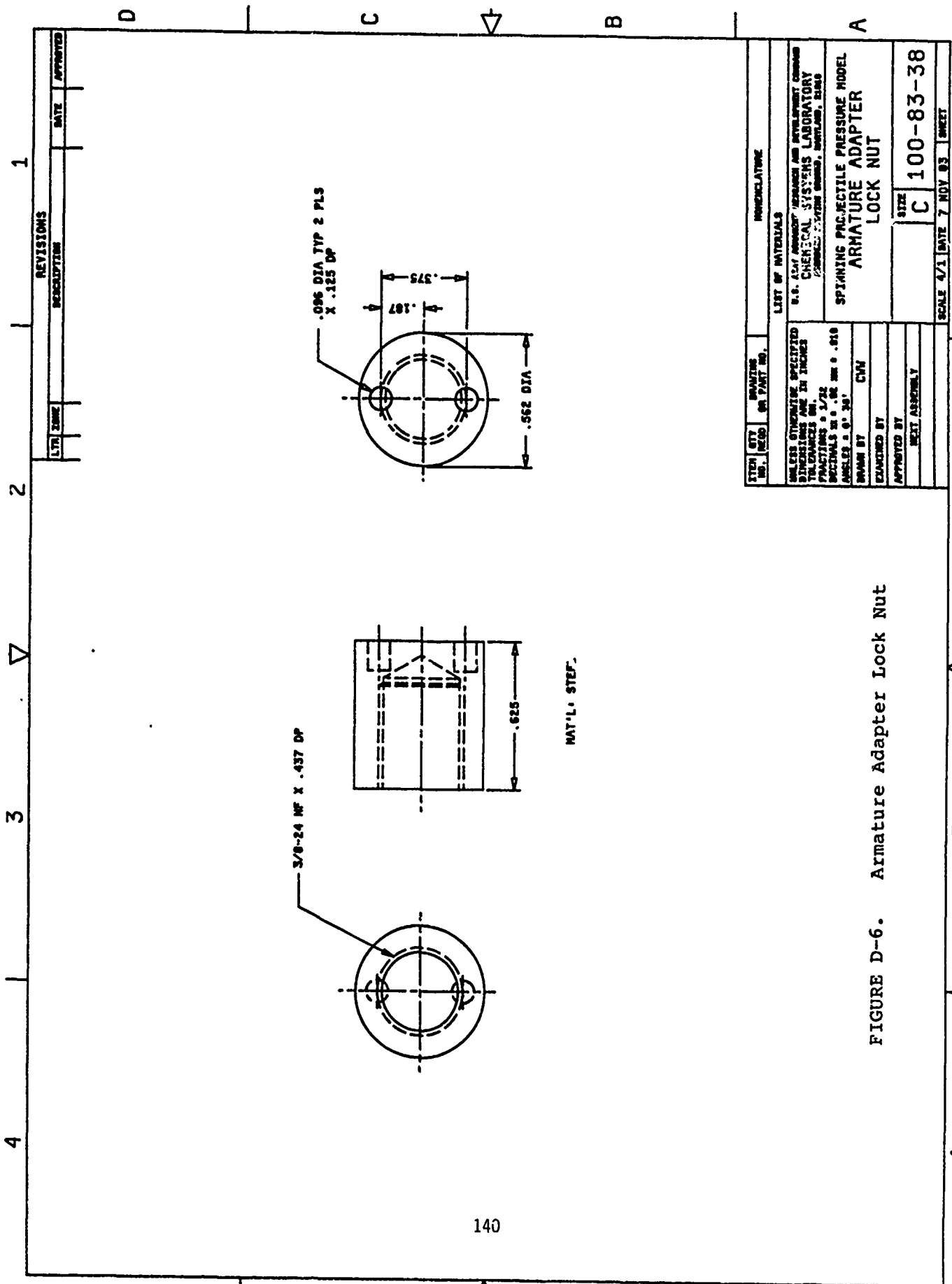


FIGURE D-6. Armature Adapter Lock Nut

LIT. ZONE		REVISIONS		DATE		APPROVED	
NO.	DESCRIPTION	NO.	DESCRIPTION	NO.	DESCRIPTION	NO.	DESCRIPTION
1		2		3		4	

ITEM NO.	QTY	REMARKS	OR PART NO.	SYMBOL	DESCRIPTION
1	1	ARMATURE ADAPTER LOCK NUT			

LIST OF MATERIALS	
UNLESS OTHERWISE SPECIFIED	U.S. ARMY AMMUNITION RESEARCH AND DEVELOPMENT COMMAND
DIMENSIONS ARE IN INCHES	CHEMICAL SYSTEMS LABORATORY
TOLERANCES ARE:	2200 ARMY AMMUNITION RESEARCH AND DEVELOPMENT COMMAND, WASHINGTON, D.C.
FRACTIONS ± 1/32	
DECIMALS ± 0.005	
ANGLES ± 0.1°	
DRAWN BY	CW
EXAMINED BY	
APPROVED BY	
TEST ASSEMBLY	

SIZE	DATE	BY	NO.
C	100-83-38		

SCALE	DATE	BY	NO.
1/1	7 NOV 83		

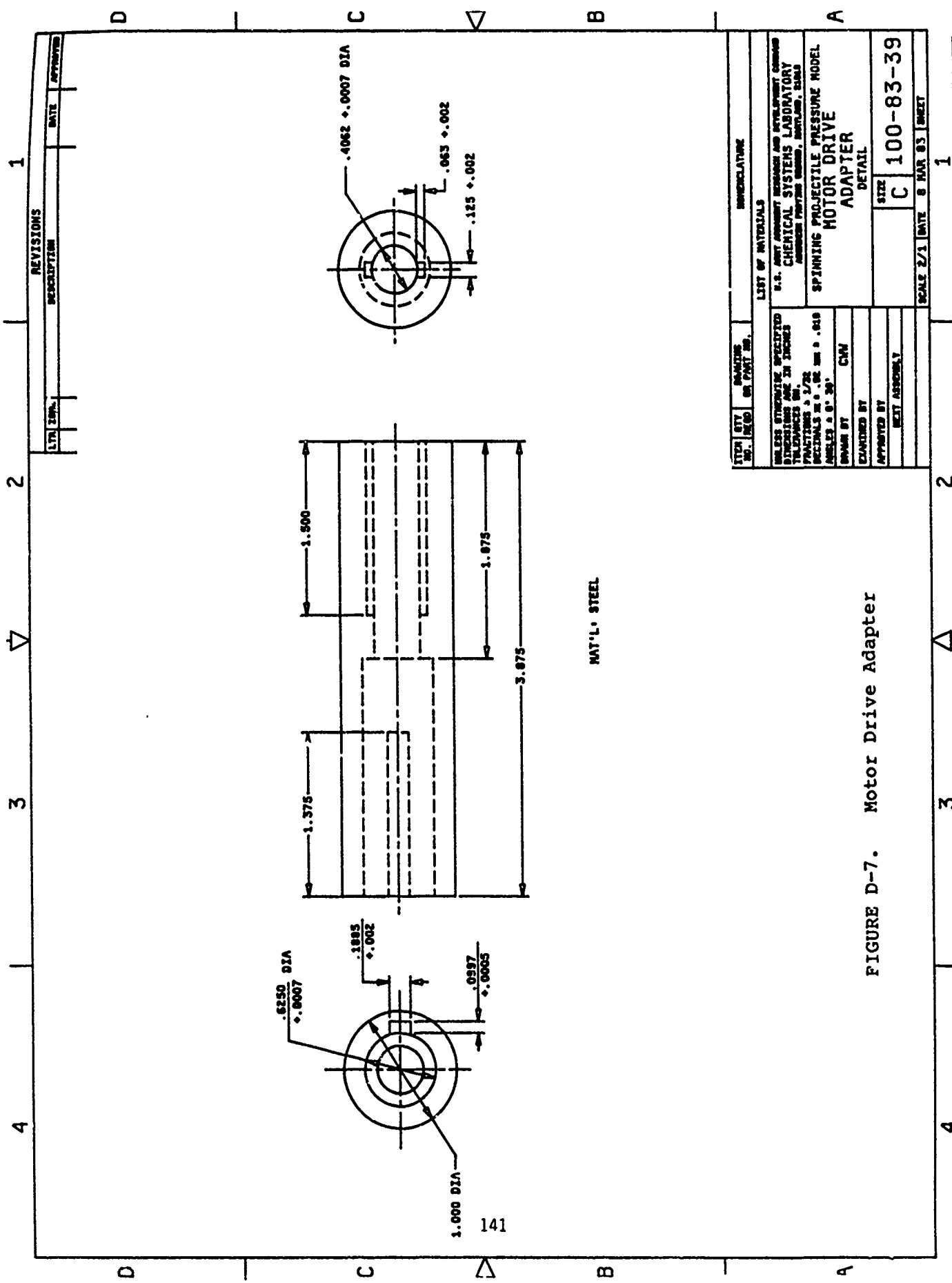
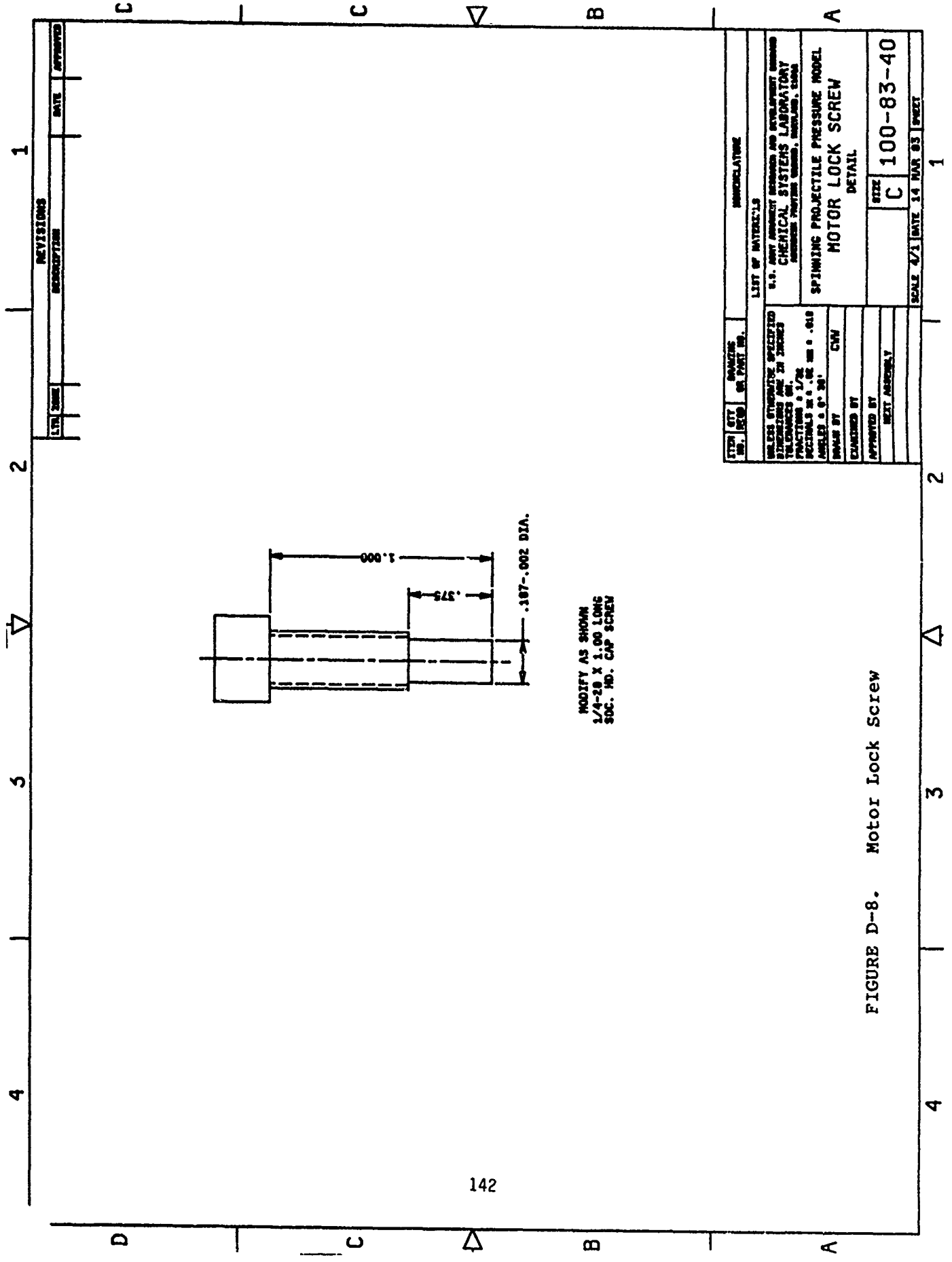


FIGURE D-7. Motor Drive Adapter

ITEM NO.	QTY REQD	DESCRIPTION	DATE	APPROVED
<p>UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ARE:</p> <p>FRACTIONS \pm .005</p> <p>DECIMALS \pm .001</p> <p>ANGLES \pm 1° 30'</p>				
<p>LIST OF MATERIALS</p> <p>U.S. ARMY ARMY RESEARCH AND DEVELOPMENT COMMAND</p> <p>CHEMICAL SYSTEMS LABORATORY</p> <p>AMERICAN PROJECTILE MODEL</p>				
<p>SPINNING PROJECTILE PRESSURE MODEL</p> <p>MOTOR DRIVE ADAPTER</p>				
<p>DETAIL</p>				
<p>EXAMINED BY</p>				
<p>APPROVED BY</p>				
<p>NEXT ASSEMBLY</p>				
<p>SCALE 2/1 DATE 8 MAR 83 SHEET</p>				



MODIFY AS SHOWN
1/4-28 X 1.00 LONG
SDC. NO. CAP SCREW

FIGURE D-8. Motor Lock Screw

ITEM NO.		QUANTITIES ON HAND		DATE	
LIST OF MATERIALS					
2.2. SPIN. PROJECTILE FORMER AND JET-LOCKER MOUNTED CHEMICAL SYSTEMS LABORATORY RESEARCH PROJECTS DIVISION, BIRMINGHAM, ALABAMA					
SPINNING PROJECTILE PRESSURE MODEL MOTOR LOCK SCREW DETAIL					
DRAWN BY CWH				SIZE C	100-83-40
EXAMINED BY					
APPROVED BY					
NEXT ASSEMBLY					
SCALE 4/1				DATE 14 MAR 63	SHEET

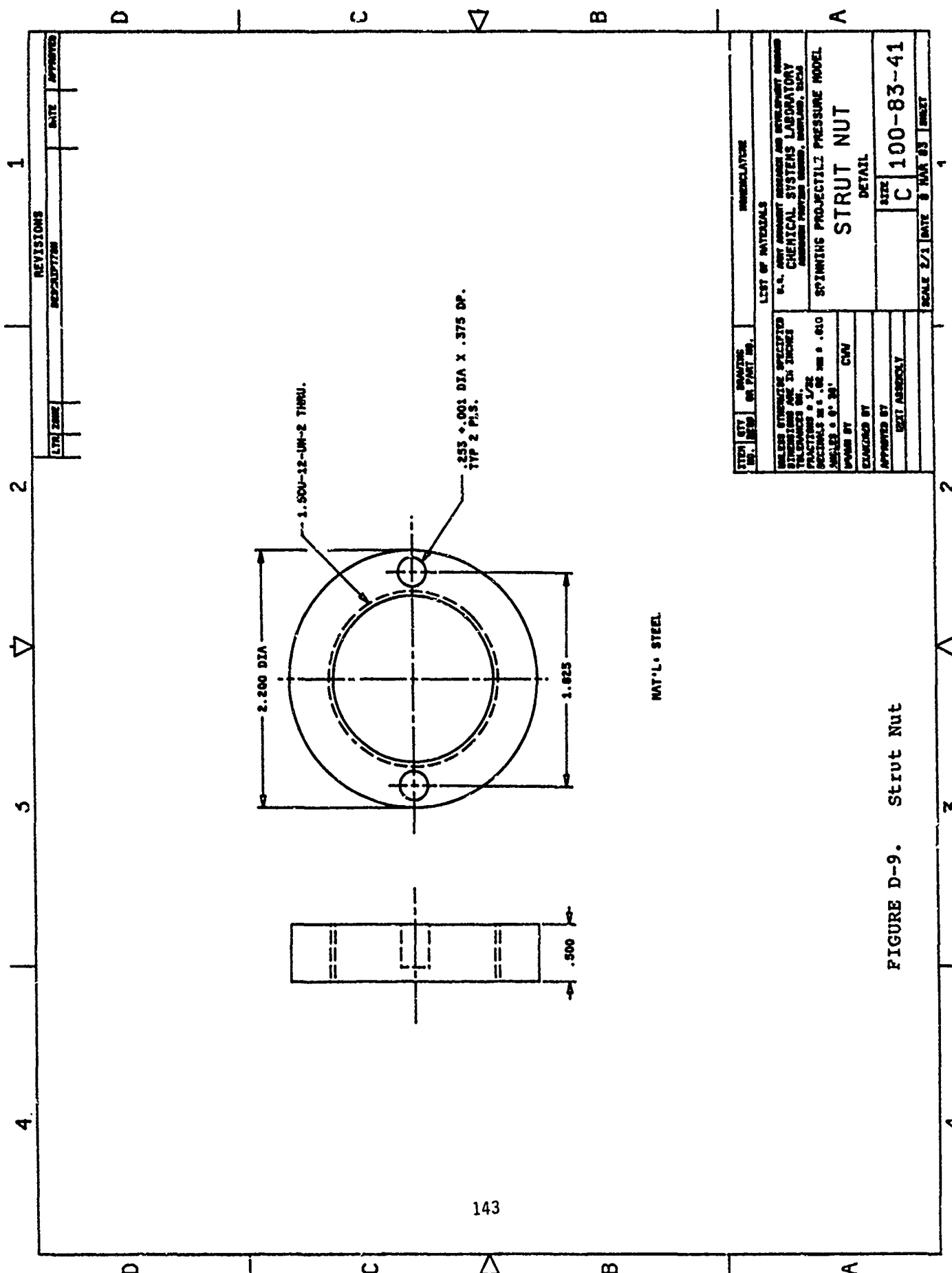


FIGURE D-9. Strut Nut

STEP	QTY	REMARKS	OR PART NO.
1	1	1	1
<p>LIST OF MATERIALS</p> <p>UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES ARE: FRACTIONS ± 1/32 DECIMALS ± .01 ANGLES ± 1° 30'</p> <p>WARRANTY BY C/W</p> <p>EXAMINED BY</p> <p>APPROVED BY</p> <p>DATE ASSEMBLY</p>			
<p>U.S. ARMY AMMUNITION RESEARCH AND DEVELOPMENT COMMAND CHEMICAL SYSTEMS LABORATORY AMMUNITION PRODUCTION DIVISION, BARCLAY, MD</p>			
<p>SPINNING PROJECTILE PRESSURE MODEL</p>			
<p>STRUT NUT</p>			
<p>DETAIL</p>			
<p>SIZE</p>			<p>C 100-83-41</p>
<p>SCALE 2/1 (DATE 8 MAR 83)</p>			<p>1</p>

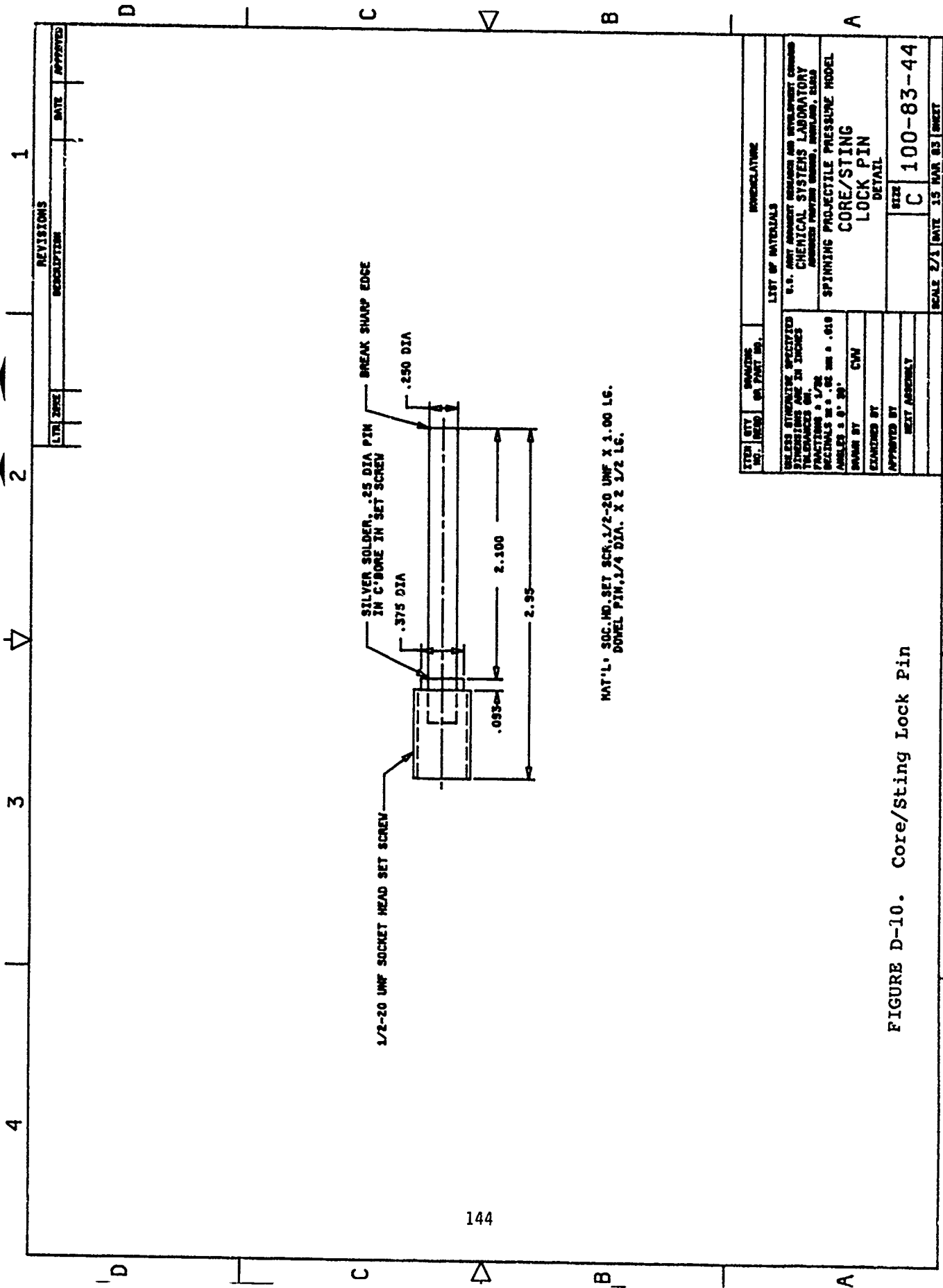
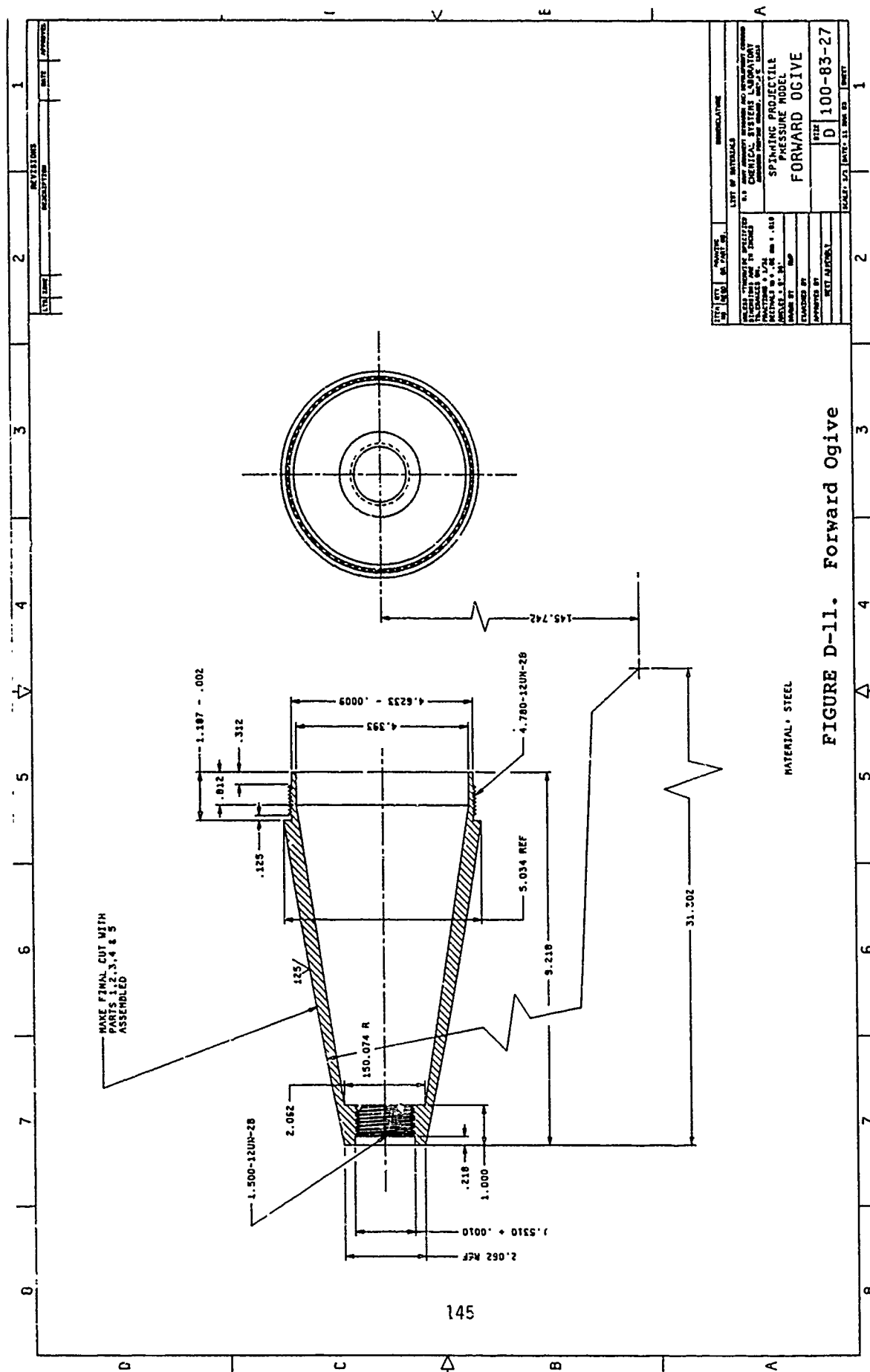
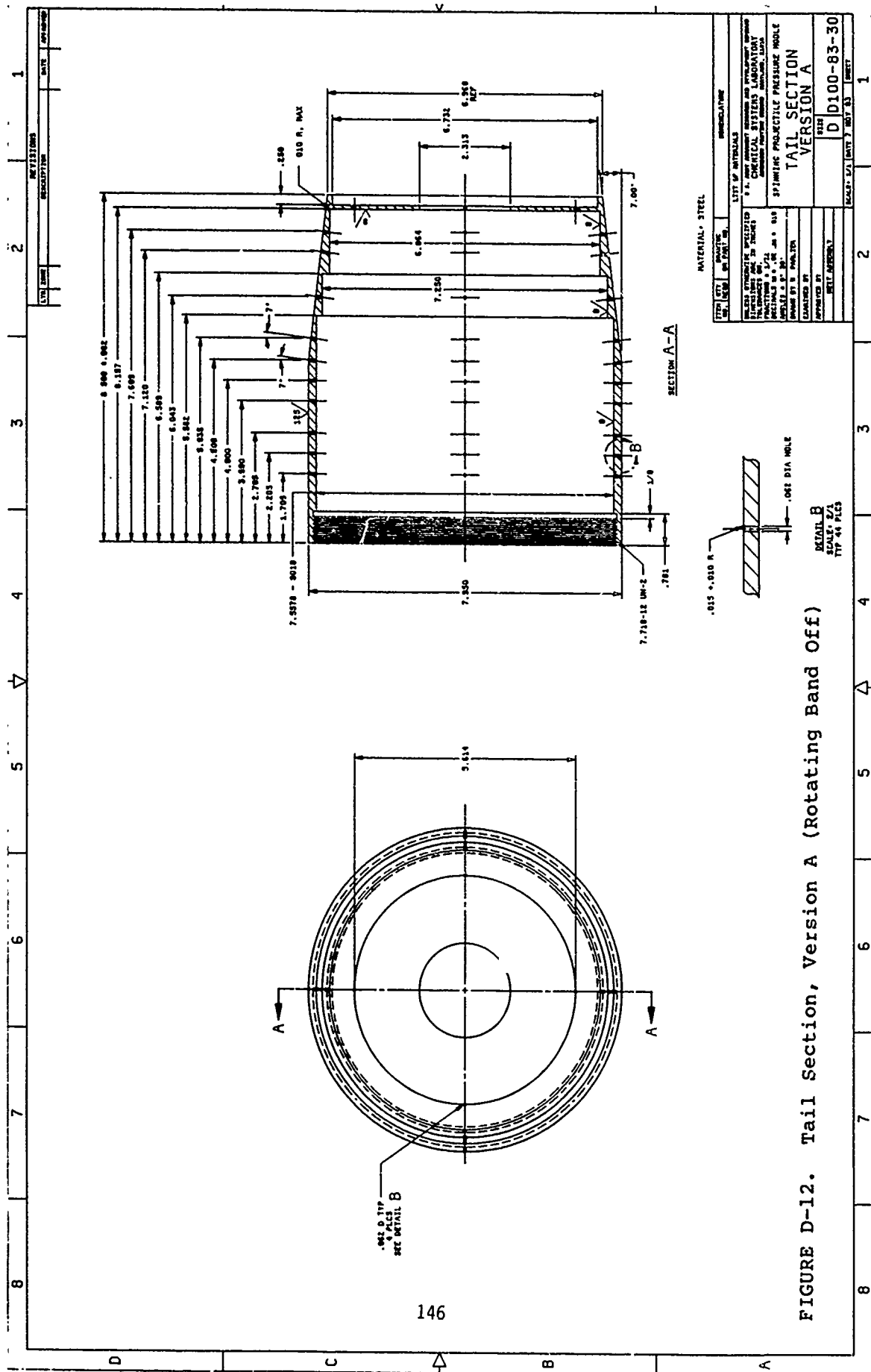
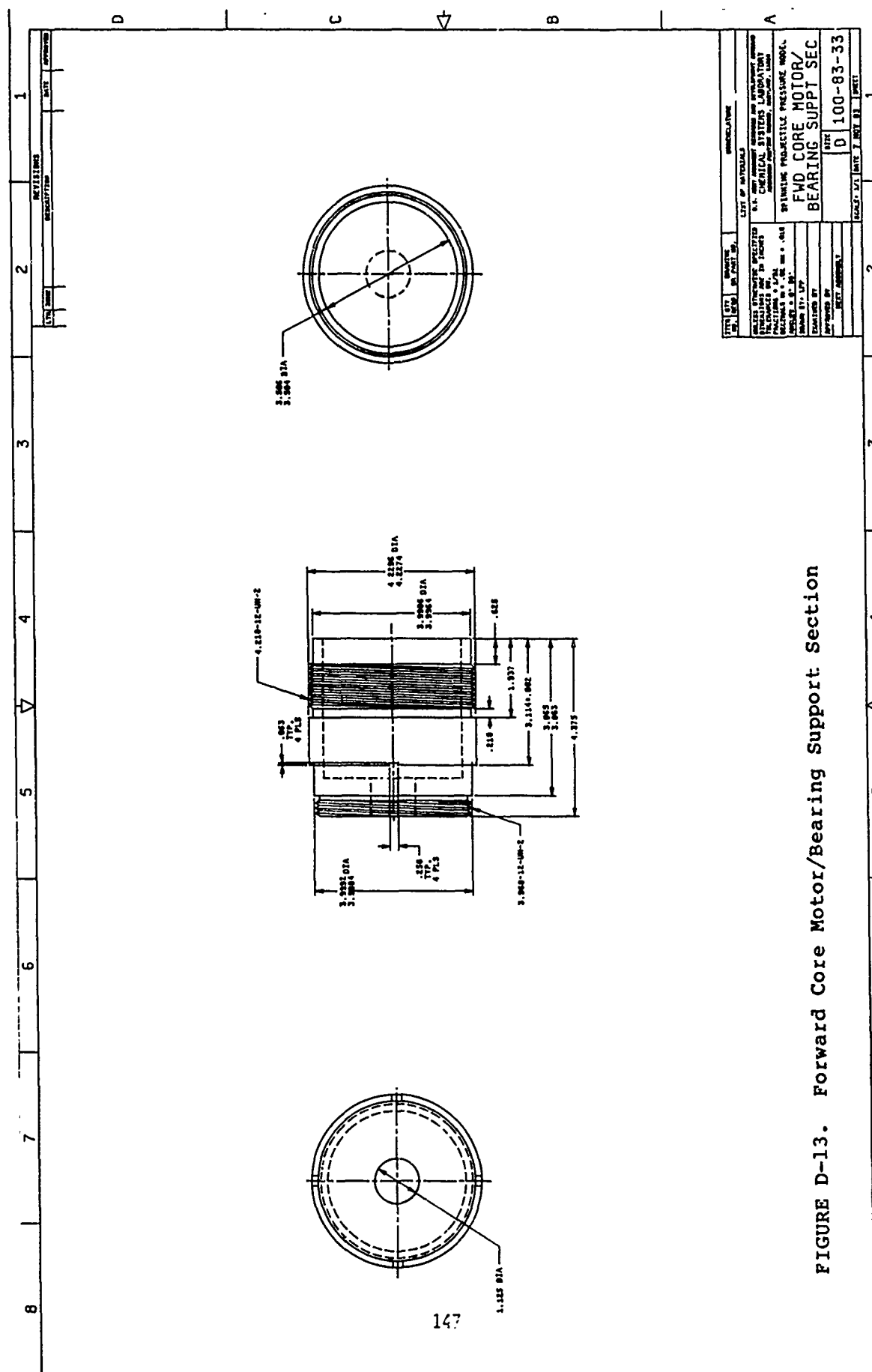
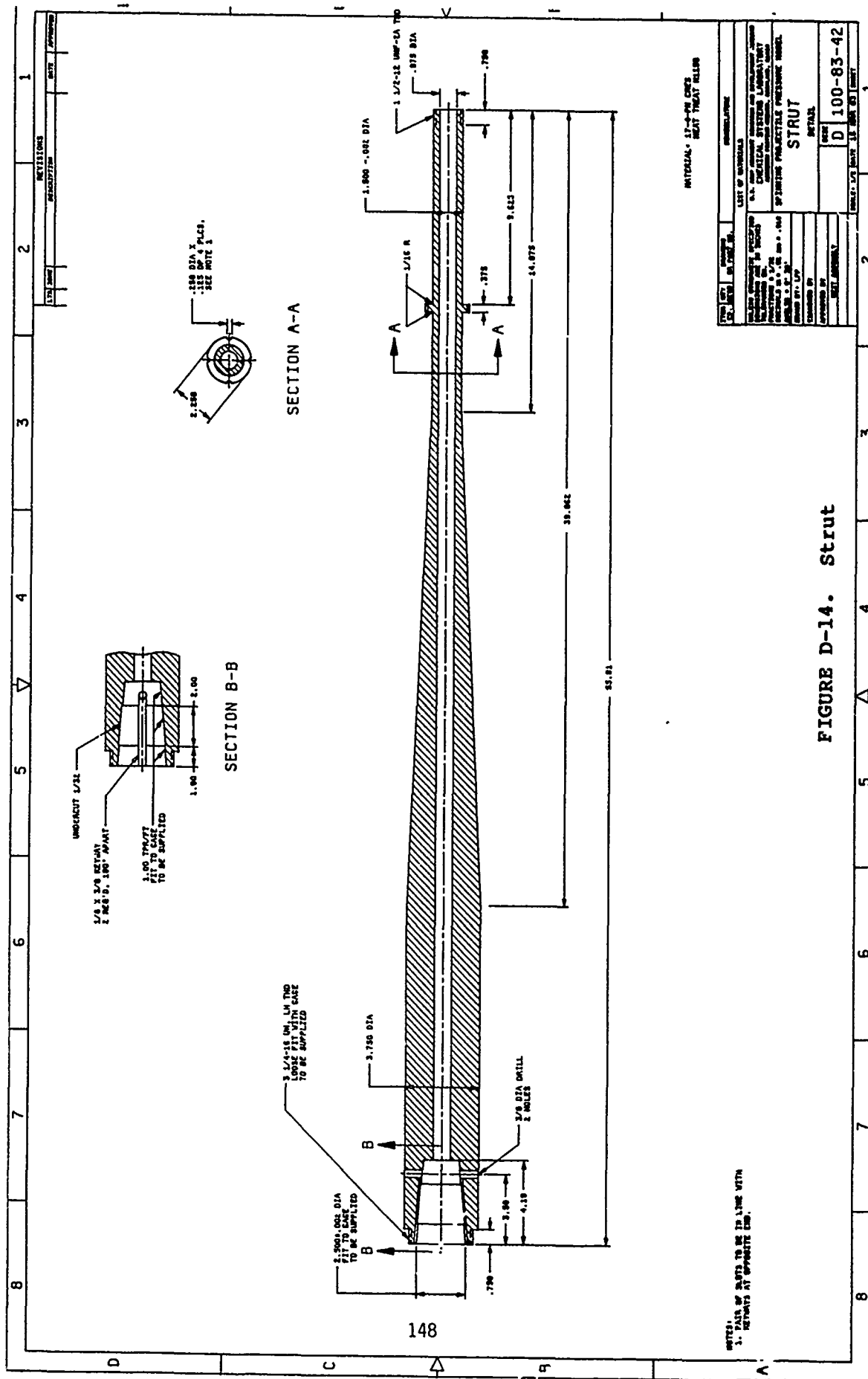


FIGURE D-10. Core/Sting Lock Pin









NOTES:
1. PARTS OF STRUTS TO BE IN LINE WITH
2. RETAINS AT OPPOSITE END.

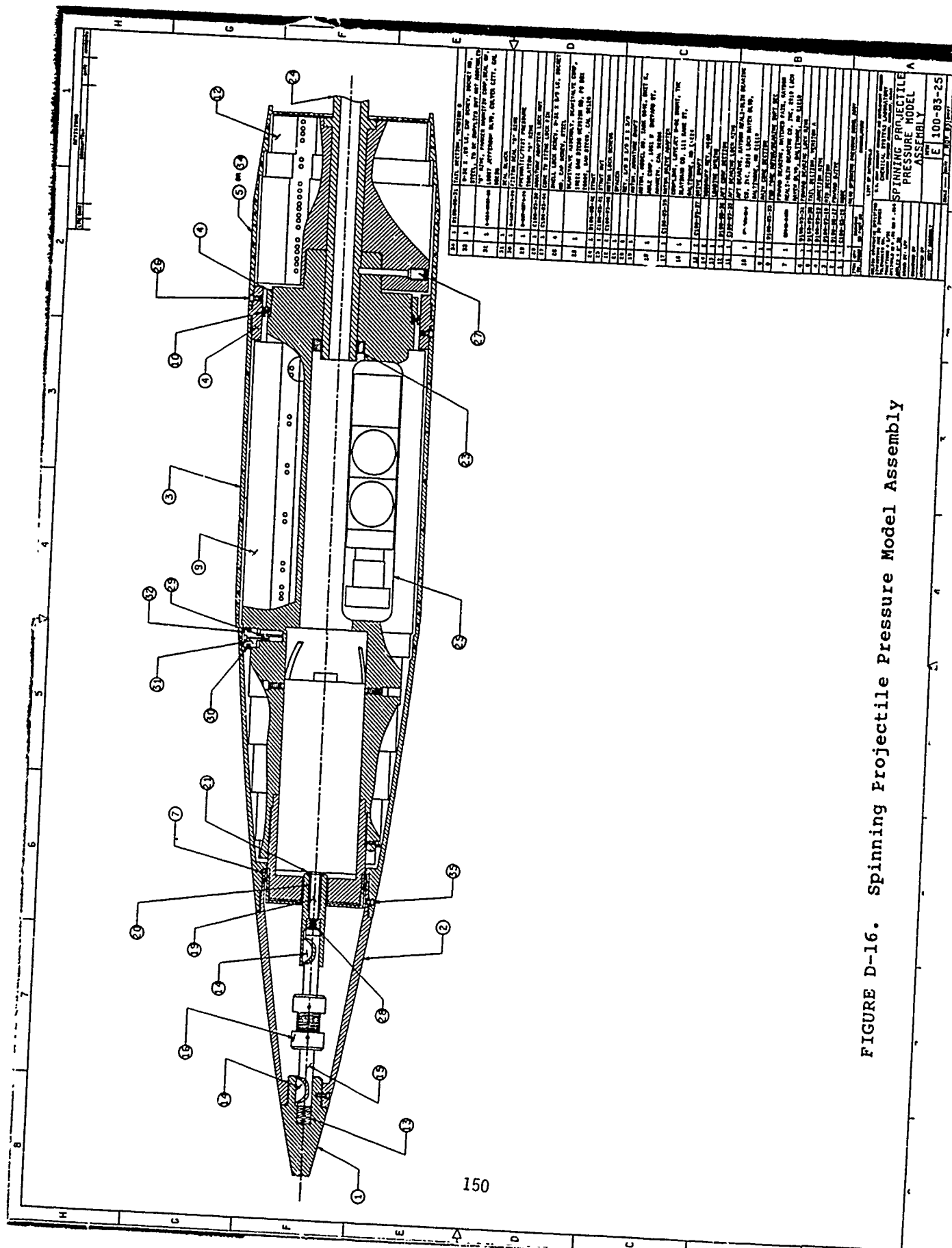


FIGURE D-16. Spinning Projectile Pressure Model Assembly

